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## **DAVENPORT SUBDIVISION**

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*Township of Georgian Bluffs (Sarawak)*  
*Project No. 06-D-3969*

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### **FUNCTIONAL PLANNING REPORT**

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### **STORMWATER MANAGEMENT COMPONENT**

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# TABLE OF CONTENTS

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	<b>Page No.</b>
1.0 INTRODUCTION	1
2.0 EXISTING CONDITIONS	1
3.0 POST-DEVELOPMENT CONDITIONS	4
4.0 STORMWATER QUANTITY AND QUALITY CONTROL	7
5.0 EROSION AND SEDIMENT CONTROL	11
6.0 CONCLUSIONS	12

## APPENDICES

APPENDIX I	Stormwater Management Supporting Information
APPENDIX II	Visual Otthymo Output Pre Development
APPENDIX III	Visual Otthymo Output Post Development Un-Controlled
APPENDIX IV	Visual Otthymo Output Post Development Controlled

## **1.0 INTRODUCTION**

The proposed Davenport Subdivision is located on part of Lot 27, Concession III in the geographic township of Sarawak, now in the Township of Georgian Bluffs. The owner is proposing to develop 6.625 hectares of land adjacent to Church Side Road East, and leave the remaining property undeveloped. The proposed development will result in the creation of 29 rural residential lots.

The site is located approximately ten kilometres north of the City of Owen Sound, in the area of East Linton on the west side of Owen Sound. The project site is south of Church Side Road East, east of Grey County Road No.1, and west of Balmy Beach Road. The site is bordered by residential lands on the west, east and south sides. The area north of the project site is still rural agricultural land. The entire project site is well vegetated as either inactive pasture/meadow or wooded areas.

The development of the project site requires a stormwater management plan which addresses the potential impacts of increased surfacewater runoff with consideration given to the quality of that runoff and erosion control. Given the relatively low imperviousness which will be associated with a rural residential development it is preferred to utilize source and conveyance controls to provide the stormwater controls required. Due to the relatively low slopes (0 - 5.0%), source and conveyance controls will be feasible in providing adequate stormwater controls for the project site.

The goal of the stormwater management controls will be to meet the quantity control requirements of the Township of Georgian Bluffs and the Grey Sauble Conservation Authority (GSCA) plus the quality control requirements of GSCA and the Ontario Ministry of the Environment (MOE) 2003 guidelines. Due to the close proximity to Georgian Bay, "Enhanced" water quality treatment will be provided. It is also the intention of the development to control post-development peak flow rates due to the increase in impervious areas to as close to pre-development levels as possible.

## **2.0 EXISTING CONDITIONS**

The existing project site has variable topography with good vegetation cover over the majority of the site. The topography of the site and external associated lands varies from quite flat on the project site to very steep in the east with slopes approaching 30% on the west side of Balmy Beach Road. The existing land use of the project site consists mainly of idle field and meadow with a single detached family dwelling with surrounding manicured lawn and some scrub brush in the center of the site. Runoff from the subdivision and adjacent lands crosses easterly under Balmy Beach Road

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through one of two existing culverts. A 800mm diameter corrugated steel pipe (C.S.P.) culvert underneath Balmy Beach Road or a 760mm diameter corrugated steel pipe culvert near the intersection of Balmy Beach Road and Church Side Road East. Both culverts drain into Georgian Bay (Owen Sound), with the 800mm culvert across privately owned lands and the 760mm within the municipal roadway.

Based on the Grey County soil mapping from the Ministry of Agriculture and Food there are two main types of surficial soils present within the study area; Morely Bouldery Clay and Donnybrook Sandy Loam. Morely Bouldery Clay accounts for 100% of the surficial soil within the project site and is considered a poorly drained calcareous stony loam till. This loam soil is classified as type 'C' within the Soil Conservation Service (SCS) hydrologic soil grouping. Donnybrook Sandy Loam is present as surficial soil to the west of the project site, within the watershed area that drains through the site. It is considered a well drained moderately gravelly sand loam and is classified as type 'AB' within the Soil Conservation Service (SCS) hydrologic soil grouping.

Under existing conditions, the project site is considered three watershed areas based on the natural topography of the land determined by contour data (1.0m interval) from Ontario Base Maps, a stormwater management report prepared by Crozier & Associates (April, 2008) for the adjacent property to the south and a topographical survey carried out by M.J. Davenport & Associates plus a visual field inspection. The existing subwatershed areas are illustrated on Pre-Development Subwatershed Areas Drawing No. 3969-SW1.

The existing subwatershed area includes:

Subwatershed Area No. 1 (8.195 hectares) consists of a small area of the north western portion of the project site and additional area west of the site that drains towards the subject property. This subwatershed area is comprised primarily of open meadow with patches of mature trees and several single family detached dwellings and manicured landscaped areas. Under pre-development conditions this area drains mostly as sheet flow towards the roadside ditches running north-south across the subject property.

Subwatershed Area No. 2 (2.313 hectares) consists of an area within the subject property on both the east and west side of the existing driveway. This subwatershed area is comprised primarily of open pasture/meadows with a portion of a small treed area and a single family detached dwelling and manicured landscaped areas. Under pre-development conditions this area drains as sheet flow towards the existing ditches on both the east and west sides of the existing driveway.

Subwatershed Area No. 3 (1.561 hectares) consists of the easterly area within the subject property. This subwatershed area is comprised primarily of open pasture/meadows with a portion of a small treed area and a single family detached dwelling and manicured landscaped areas. Under pre-development conditions this area drains as sheet flow easterly onto adjacent lands.

The parameters used in the Visual Otthymo computer program are shown in Table 1.

**Table 1**  
**Existing Subwatershed Area Information**

Sub-watershed	Area (ha)	Land use	Slope (%)	Length (m)	C	Time to Peak (hr)	CN*	Ia (mm)
1	8.195	Woods / Meadow	3.0	650	0.376	0.407	67	5.0
2	2.313	Meadow / Lawns	3.0	320	0.446	0.246	75	5.0
3	1.561	Meadow / Lawns	3.0	70	0.393	0.129	75	5.0

The weighted runoff coefficient, 'C' is based upon "Design Chart 1.07: Runoff Coefficients" of the MTO Drainage Management Manual (MTO, 1997). The 'C' value considers the land use and topography plus the hydrologic soil classification or soil texture then is used to calculate "Time to Peak." Figure 3 in Appendix I "Supporting Information" includes the calculation of "time to peak".

Curve Number (CN) is based upon "Design Chart 1.09: Soil/Land Use Curve Numbers" of the MTO Drainage Management Manual (MTO, 1997). The CN value considers the soil type and the Hydrologic condition. The Curve Number (CN\*) is the weighted value for the antecedent moisture condition of the soil (AMC II). The weighted Curve Number (CN\*) is calculated based on the weighted average of the imperviousness of the subwatershed area. For modelling purposes different CN\* values are used due to the existence of different quantities of impervious areas within the subwatershed area. An initial abstraction value (Ia) of 5.0mm or less was used. Figure 2 in Appendix I includes the conversion of CN value to CN\*.

The Visual OTTHYMO computer program was used to model the surface water runoff from the subject area under existing conditions. Peak flows for varying return periods were computed, and the results are shown in Table 5 on page 10. The detailed Visual OTTHYMO output for the existing conditions is attached in Appendix II.

### **3.0 POST DEVELOPMENT CONDITIONS**

The development will create 29 rural residential lots with three streets constructed as rural road cross sections consistent with standards specified by the Township of Georgian Bluffs. The existing ditching along the proposed Street 'B' will be widened to accommodate the design criteria for enhanced grass swales and an under drained infiltration trench will be installed under the proposed swale to promote infiltration and provide quality control. The current gravel roadway will be paved with hot mix asphalt complete with gravel shoulders. Streets 'A' and 'C' will be constructed as rural road cross sections with complete with under drained infiltration trench beneath the roadside ditches. This configuration will affect all three pre-development watershed areas and will require some minor lot grading in addition to construction of two new roads, roadside ditching and other swales around the property to control stormwater runoff unto adjacent properties.

The proposed subwatershed areas include:

Subwatershed Area No. 1 (4.823 hectares) consists of the area west of the project site that drains towards the site as well the majority of the impervious area and ditching of proposed Street 'A'. This subwatershed area will remain largely unchanged, with the exception being the construction of Street 'A' as a hot mix asphalt road and associated enhanced grass swale ditching. The majority of the ditching for Street 'A' will be directed toward the existing roadside ditch along Church Side Road East. This will divert westerly flowing water into the Church Side Road East roadside ditch after passing through the enhanced grass swale ditching of Street 'A', instead of flowing across the subject property. All area west of the subject property is assumed to remain unchanged. The low impervious area of this subwatershed allows the use of the NasHYD command in the Visual OTTHYMO model.

Subwatershed Area No. 2 (1.396 hectares) consists of the area west of the subject property, but east of proposed Street 'A' and is identified as the Greig property on the design drawings. This subwatershed area will remain largely unchanged, with the exception being the extension of the existing grassed swale that runs along the border of the project site and the Greig lands. This grassed swale will divert stormwater flowing westerly from the Greig property into the Church Side Road East ditch directly, rather than allowing it to flow across the subject property as it does under pre-development conditions. The proposed extension of the swale will be constructed as a enhanced grass swale without a proposed under drain. The low impervious area of this subwatershed allows the use of the NasHYD command in the Visual OTTHYMO model.

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Subwatershed Area No. 3 (3.628 hectares) consists of the majority of the area within the subject property. This area includes half of the area of Street 'B', the entirety of Street 'C' as well as the driveways, rooftop areas and grassed yards of lots 11-29. This subwatershed includes all of the area draining to the west side of the roadside ditch for Street 'B' within the project site. This subwatershed area will be developed into 19 rural residential lots complete with single family detached homes, driveways and manicured lawn areas. Under post-development conditions the frontages of lots 11-29 will now drain into the roadside ditches of Street 'B' and 'C'. The roadside ditches along Street 'B' will be constructed as low slope enhanced grass swales and will outlet into the existing Church Side Road East ditch. The higher impervious area of this subwatershed (28.58%) due to the proposed development allows the use of the StandHYD command in the Visual OTTHYMO model.

Subwatershed Area No. 4 (0.827 hectares) consists of the area within the subject property draining to the east side of the roadside ditch of Street 'B'. This area includes the remaining half of the Street 'B' as well as the driveways and some rooftop areas of lots 1-10. This subwatershed area will be developed into 10 rural residential lots complete with single family detached homes, driveways and manicured lawn areas. Under post-development conditions the frontages of lots 1-10 will now drain into the east side roadside ditch of Street 'B'. The roadside ditches along Street 'B' will be constructed as low slope enhanced grass swales and will outlet into the existing Church Side Road East ditch. The higher impervious area of this subwatershed (32.77%) due to the proposed development allows the use of the StandHYD command in the Visual OTTHYMO model.

Subwatershed Area No. 5 (1.394 hectares) consists of the easterly area within the subject property and includes the majority of the rooftop rainwater discharge and rear yards of lots 1-10. The drainage for this subwatershed area will remain largely unchanged and will be developed into manicured lawn areas and single family dwellings. Under post-development conditions this area drains in the existing direction, easterly as sheet flow into a low slope enhanced grass swale running along the rear lot lines of lots 1-10. This swale will treat and direct stormwater runoff into the existing Church Side Road East ditch. The lower impervious area of this subwatershed allows the use of the NasHYD command in the Visual OTTHYMO model.

All parameters used to model the post-development subwatershed areas in the Visual Otthymo program are shown in Table 2 and 3.

<b>Table 2</b> <b>Proposed StandHYD Subwatershed Areas Information</b>									
Sub-watershed Area	Area (ha)	Imperviousness (%)		Slope (%)		Length (m)		CN*	Ia (mm)
		Total	Connected	Imp.	Perv.	Imp.	Perv.		
3	3.628	29	19	2.0	3.0	155.5	440	86	3.0
4	0.827	33	19	2.0	3.0	74.3	275	88	2.0

<b>Table 3</b> <b>Proposed NasHYD Subwatershed Area Information</b>									
Sub-watershed	Area (ha)	Land use		Slope (%)	Length (m)	C	Time to Peak (hr)	CN*	Ia (mm)
1	4.823	Woods / Meadow		3.0	475	0.369	0.353	66	5.0
2	1.396	Woods / Meadow		2.5	230	0.410	0.240	75	5.0
5	1.394	Lawns		3.0	295	0.441	0.239	84	4.0

Curve Number (CN) is based upon "Design Chart 1.09: Soil/Land Use Curve Numbers" of the MTO Drainage Management Manual (MTO, 1997). The 'CN' value considers the hydrologic soil type of 'AB' and 'C'. The weighted CN values were used to calculate the modified CN values, CN\*, for use in the Visual Otthymo modelling. The calculation of the CN\* values can be found in Figure 4 of Appendix I.

Peak flows listed in this report were calculated using the Visual Otthymo (version 2.0) computer modeling program. Peak flows were calculated for each of the 2, 5, 10, 25, 50 and 100 year design storms. Calculations include consideration for the 6 hour SCS Type II and Chicago storm distribution and the 1 Hour AES storm distribution. Rainfall data for the site was taken from the Owen Sound gauging station and is included in Appendix I.

## 4.0 STORMWATER QUALITY AND QUANTITY CONTROL

The project site area requires Enhanced Protection as described in the Ministry of the Environment and Energy's "Stormwater Management Practices Planning and Design Manual, 2003".

Providing quality and quantity control for Streets 'A', 'B' and 'C' along with the rooftop rainwater from the proposed residences and associated driveways (Subwatershed Area No. 3 and No. 4) is critical. Stormwater quality and quantity control will be achieved on this site through source and conveyance controls using a treatment train approach incorporating aspects of low impact development techniques.

The opportunity for rainwater infiltration into the native soils is limited due to the fact that the percolation rate of the native loam till soils range from 3.6 to 36 millimetres per hour according to the hydrogeological report prepared by GHD (July, 2017) for the subject site. In order to promote infiltration and achieve a pre/post development water balance, we are proposing several different low impact development techniques. It is important to note that according to the low impact development stormwater management planning and design guide, low impact development techniques can work in any soil type despite low measured infiltration rates on the subject site.

Surface water runoff from the proposed right-of-way lands will be controlled, treated and conveyed using the roadside ditches constructed as enhanced grassed swales with infiltration under-drains. The proposed enhanced grassed swales will be located on either side of Streets 'A', 'B' and 'C', however, the Street 'C' swales will not be constructed with an under drain due to the higher swale slope which limits infiltration potential.

In order for enhanced grass swales to provide quality control benefits, several design criteria must be met. According to section 4.8 regarding enhanced grass swales from the Low Impact Development Stormwater Management Planning and Design Guide, pg 4-137 to 4-148, stormwater velocity and flow depth need to be minimised during the 25mm quality storm event in order to provide quality control. Due to the possible re-suspension of solids under larger storm events, infiltration is the primary desired treatment mechanism, rather than filtration. The target velocity for stormwater flow during the 4 hour, 25mm Chicago storm event is 0.5 m/s or less in order to allow suspended solids to be captured in the grass and to promote infiltration. Furthermore, flow depth during the 25mm storm should be a maximum of two-thirds of the height of the proposed vegetation. Using un-maintained grass with an approximate height of 150-200mm as the proposed vegetation, that corresponds to a

maximum flow depth of approximately 133mm.

In order to meet these design objectives, the enhanced grass swales have been designed with low longitudinal slopes, in the range of 0.33%-1.0%. The proposed swales have been designed with a trapezoidal shape with a 762mm wide bottom section and maximum 3:1 side slopes in order to encourage pre-treatment as the stormwater enters the swales as sheet flow. Rather than construct permanent rock check dams in the enhanced grass swales, which can make periodic maintenance difficult, the enhanced grass swales have been designed with triple-french under drains. These under drains will capture low flow storm events, promoting infiltration and treatment, while also preventing frequent ponding in the swale due to the low slopes and low permeability soils found on the project site. These under drains will outlet into the existing Church Side Road East roadside ditch in order prevent the underlying soils from becoming constantly saturated. These design factors combined provide a velocity of less than 0.5 m/s and a maximum flow depth of 0.13m or less during the 4 hour, 25mm Chicago quality storm event in the Visual Otthymo model. The resulting flow depth and velocity of stormwater in the various swales proposed on site from the Visual Otthymo model are summarized in Table 4 below.

**Table 4**  
**Post Development Enhanced Grass Swale Information**

Enhanced Grass Swale (# in VOH Model)	Area (ha)	Channel Length (m)	Channel Slope (%)	25mm Flow Depth (m)	Velocity (m/s)
Street 'A' Roadside Swale (113)	4.823	200.0	0.50	0.08	0.28
West Site/Greig Enhanced Grass Swale (109)	1.396	123.0	0.50	0.03	0.14
Street 'B' Left Roadside Swale (110)	3.628	350.0	0.52	0.12	0.41
Street 'B' Right Roadside Swale (116)	0.827	250.0	0.33	0.06	0.19
East Property Line Swale (111)	1.394	250.0	0.78	0.06	0.29

The under-drain will consist of three six (6) inch diameter perforated "Big O" pipes surrounded by 3/4" washed stone. Taking into account the 40% void ratio in the clear

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stone, the volume of water able to contained within the under-drain structure is approximately 0.14 cubic metres per lineal metre of under drain. Street 'A' has been designed with approximately 395.9 lineal metres of under drain between both sides of the road, resulting in a storage volume of 55.43 cubic metres of storage beneath the enhanced grass swale. Street 'B' has been designed with roughly 480 lineal metres of under drain, totaling approximately 67.20 cubic metres of storage within the under drain structure. The water captured within the under-drain will slowly percolate into the underlying native soils in-between storm events, helping to promote groundwater recharge and providing quality control within the development.

In order to reduce the stormwater runoff from rooftop rainwater from the proposed houses, we are proposing that all of the rooftop rain water be directed onto pervious landscaped areas that have a minimum pervious flow path of 5 metres. Known as a downspout disconnection, the pervious area should be graded between one to five percent and an energy dissipater should be placed at the location of the downspout in order to ensure a level spread of flow. Rooftop rainwater is considered clean, and therefore does not require quality control. The downspout disconnect detail can be found on Drawing No. 3969-SW2 prepared by M.J. Davenport & Associates.

We are also proposing to maximize pervious surfaces by planning the subdivision with single detached lots and large grassed lawns. The larger grassed areas on each individual lot will further promote attenuation and re-use of stormwater as well as work in conjunction with the rooftop rainwater leader disconnect feature to attenuate rooftop rainwater before reaching the roadside ditch.

Peak flows listed in this report were calculated using the Visual Otthymo (version 2.0) computer modeling program. Peak flows were calculated for each of the 2, 5, 10, 25, 50 and 100 year design storms. Calculations include consideration for the 1 hour AES, 6 hour Chicago and the 6 hour SCS Type II storm distribution.

The wide range of design storms were utilized in the Visual Otthymo Model to ensure that both peak flows and maximum runoff volumes are incorporated into the stormwater management facility design. Rainfall data for the site was taken from the Owen Sound gauging station and is included in Appendix I.

Table 5 summarizes the 100 year peak flows for the existing condition compared to the proposed uncontrolled condition for all design storms discharging off site.

**Table 5 – Existing and Proposed Uncontrolled 100 Year Peak Flows Draining Off-site**

Design Storm (yr)	Peak Flows ( $m^3/s$ )								
	6 Hour Chicago			6 Hour SCS			1 Hour AES		
	Pre	Post	Diff	Pre	Post	Diff	Pre	Post	Diff
2	0.155	0.247	0.092	0.194	0.309	0.115	0.107	0.208	0.101
5	0.283	0.378	0.095	0.341	0.492	0.151	0.210	0.324	0.114
10	0.402	0.498	0.096	0.455	0.629	0.174	0.293	0.413	0.120
25	0.529	0.666	0.137	0.610	0.824	0.214	0.412	0.538	0.126
50	0.672	0.837	0.165	0.736	0.968	0.232	0.507	0.642	0.135
100	0.774	0.989	0.215	0.867	1.140	0.273	0.611	0.747	0.136

Table 5 indicates that off site flows will increase to a maximum peak flow of 1.140 cubic metres per second during the 100 year, 6 hour SCS Type II storm event under post development conditions. Quantity control measures are required to reduce the post development peak flows to be closer to pre-development levels. To achieve this, conveyance controls incorporating low impact development methods will be employed. The series of proposed enhanced grass swales capturing and conveying flow on site will reduce the peak flow off site when compared to the uncontrolled condition.

The peak flows discharging off-site for the pre-development and post-development controlled condition are summarized in Table 6.

**Table 6 – Existing and Proposed 100 Year Peak Flows Draining Off-site**

Design Storm (yr)	Peak Flows ( $m^3/s$ )								
	6 Hour Chicago			6 Hour SCS			1 Hour AES		
	Pre	Post	Diff	Pre	Post	Diff	Pre	Post	Diff
2	0.155	0.190	0.035	0.194	0.232	0.038	0.107	0.137	0.030
5	0.283	0.343	0.060	0.341	0.404	0.063	0.210	0.248	0.038
10	0.402	0.488	0.086	0.455	0.534	0.079	0.293	0.347	0.054
25	0.529	0.652	0.123	0.610	0.723	0.113	0.412	0.491	0.079
50	0.672	0.819	0.147	0.736	0.861	0.125	0.507	0.616	0.109
100	0.774	0.964	0.190	0.867	1.030	0.163	0.611	0.741	0.130

Table 6 indicates that off-site stormwater peak flows will see a net increase in all storm events under post development conditions. It is important to note that the simulated conditions do not include consideration for the storage capacity of the proposed roadside ditch under-drain and therefore do not take into account the

reduced peak flow and flow depth resulting from the under drain. Proposed municipal roadside ditch upgrades downstream of the subject property will expand the conveyance capacity in order to safely direct the increase in post development peak stormwater flows to Owen Sound Bay.

The supporting calculations for the stormwater management simulation are included in Appendix I. The summary and detailed Visual Otthymo output files for all three (3) scenarios are included in Appendix I.

## **5.0 EROSION AND SEDIMENTATION CONTROL**

Erosion and sedimentation control measures will be installed within the development during every step of construction, to minimize the effects on lands external to the development as well as to protect the infiltration techniques within the development.

Infiltration underdrains are susceptible to clogging during the construction stage of development. As a result, we are recommending that the municipal infrastructure be constructed within the Right-of-Way before the underdrain is installed. Two rows of silt fence will be installed in the Street 'A' and 'B' ditches before they outlet into Church Side Road East to capture any sedimentation that enters the road side ditches. After paving is complete on the proposed road way, the underdrain shall be installed under the road side ditches and the silt fencing can be removed. After the under-drains are installed, terrifix erosion control blankets (or approved equivalent) will be placed in all roadside ditches in order to accelerate the rate of re-vegetation, while also preventing excessive erosion of the channel until vegetation can be established. Furthermore, the erosion control blanket will capture any sedimentation coming from earth moving operations on the individual lots.

During construction of homes on the individual lots, the municipal road side ditches shall be protected from silt entering the ditch by installing silt fence between the proposed residence and the road side ditches.

The erosion and sedimentation control measures shall be inspected after every major rainfall event, and sediment buildup shall be cleaned and removed from the ditches as required. The proposed erosion controls shall be constructed according to drawing No. 3969-EC1 prepared by M.J. Davenport & Associates.

## **6.0 CONCLUSIONS AND RECOMMENDATIONS**

In our professional opinion, the combination of source and conveyance controls proposed, along with downstream municipal ditch upgrades, will provide adequate quality and quantity control for the proposed development preventing adverse negative impacts on adjacent and downstream land owners.

Prepared by:

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Jacob Clark, EIT

January 23, 2019



Michael M. Davenport, P. Eng.

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**APPENDIX I**

**STORMWATER MANAGEMENT**

**SUPPORTING INFORMATION**

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**FIGURE 1**  
**DAVENPORT SUBDIVISION**  
**WEIGHTED VALUES FOR CN & C - PRE-DEVELOPMENT**  
**UNCALIBRATED PARAMETERS**

**FIGURE 2**  
**DAVENPORT SUBDIVISION**  
**CONVERSION OF CN TO CN\* - PRE-DEVELOPMENT.**

UNCALIBRATED PARAMETERS										CN for Condition I										CN for Condition II										CN for Condition III																					
Subwatershed	Command	CN (AMC II)	CN (AMC III)	S (mm)	Calculated la	P	Q	Standard la	S*	CN* (AMC III)	CN* (AMC II)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0											
1	101	69.4	84	48.38	7.26	126.8	85.10	5	52.52	83	67	2	5	13	5	10	22	10	15	30	15	20	37	20	25	48	25	30	50	31	32	52	33	35	55	36	38	58	39	40											
2	102	74.8	88	34.64	5.20	151.3	118.11	5	34.92	88	75	6	15	30	15	20	37	20	25	48	25	30	50	31	32	52	33	35	55	36	38	58	39	40	60	61	62	63	64	65	66	67	68	69	70						
3	103	74.3	88	34.64	5.20	151.3	118.11	5	34.92	88	75	9	20	37	20	25	48	25	30	50	31	32	52	33	35	55	36	38	58	39	40	60	61	62	63	64	65	66	67	68	69	70									
<b>Post-Development Conditions</b>										0										0										0																					
1	101	69.4	84	48.38	7.26	126.8	85.10	5	52.52	83	67	2	5	13	5	10	22	10	15	30	15	20	37	20	25	48	25	30	50	31	32	52	33	35	55	36	38	58	39	40	60	61	62	63	64	65	66	67	68	69	70
2	102	74.8	88	34.64	5.20	151.3	118.11	5	34.92	88	75	6	15	30	15	20	37	20	25	48	25	30	50	31	32	52	33	35	55	36	38	58	39	40	60	61	62	63	64	65	66	67	68	69	70						
3	103	74.3	88	34.64	5.20	151.3	118.11	5	34.92	88	75	9	20	37	20	25	48	25	30	50	31	32	52	33	35	55	36	38	58	39	40	60	61	62	63	64	65	66	67	68	69	70									

The CN values used for each subcatchment are the weighted values calculated based upon the different soils and land use.

**FIGURE 3**  
**DAVENPORT SUBDIVISION**  
**TIME TO PEAK (Tp) FOR DIFFERENT RETURN PERIODS**

Subwatershed	Area (ha)	Average Slope (%)	Travel Length (m)	Runoff Coefficient - 'C'				25 Year	100 Year	2/5/10 Year	50 Year	100 Year	Time to Peak (hr)
				25 Year	50 Year	100 Year							
<b>Pre-Development</b>													
1	8.195	3.00	650	0.376	0.414	0.451	0.470	0.467	0.443	0.419	0.407		
2	2.313	3.00	320	0.446	0.491	0.535	0.558	0.296	0.276	0.256	0.246		
3	1.561	3.00	70	0.392	0.431	0.470	0.490	0.150	0.142	0.133	0.129		

**Bransby-Williams Method**  
**Post-Development Urban Watersheds**

Subwatershed	Average Slope (%)	Travel Length (m)	Velocity (m/s)	Time to Peak (hr)		
				2/5/10 Year	25 Year	50 Year

**FIGURE 4**  
**DAVENPORT SUBDIVISION**  
**WEIGHTED VALUES FOR CN & C - POST-DEVELOPMENT**  
**UNCALIBRATED PARAMETERS**

Soil Type from Mapping	Hydrologic Soil Group for Modelling	Land Use	CN Value	Runoff Coeff. C	Subwatershed No. 1			Subwatershed No. 2			Subwatershed No. 3			Subwatershed No. 4			Subwatershed No. 5		
					Area (ha.)	Weighted CN Portion	C Portion	Area (ha.)	Weighted CN Portion	C Portion	Area (ha.)	Weighted CN Portion	C Portion	Area (ha.)	Weighted CN Portion	C Portion	Area (ha.)	Weighted CN Portion	C Portion
Morely Bouldery Clay	C	Woodland	77	0.35	1.206	92.852	0.422	0.476	36.652	0.167	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Morely Bouldery Clay	C	Meadow	71	0.40	1.080	76.680	0.432	0.822	58.352	0.329	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Morely Bouldery Clay	C	Lawns	82	0.35	0.069	5.658	0.024	0.020	1.540	0.007	2.591	212.462	0.907	0.556	45.552	0.195	1.164	95.448	0.407
Morely Bouldery Clay	C	Impervious	98	0.90	0.264	25.872	0.238	0.078	7.644	0.070	1.037	101.626	0.933	0.271	26.558	0.244	0.230	22.540	0.207
Donnybrook Sandy Loam	AB	Woodland	54	0.25	2.032	109.728	0.508	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Donnybrook Sandy Loam	AB	Impervious	98	0.90	0.172	16.856	0.155	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Total Area :					4.323		1.396		3.628		0.827					1.394			
Weighted CN :					67.956		0.369		74.712		0.410					87.243			
Weighted C :																0.530			
																34.640			
																0.441			

**FIGURE 5**  
**DAVENPORT SUBDIVISION**  
**CONVERSION OF CN TO CN\* POST-DEVELOPMENT**

UNCALIBRATED PARAMETERS									
Subwatershed	Command	CN (AMC II)	CN (AMC III)	S (mm)	Calculated la	P	Q	Standard la	S*
<b>Post-Development Conditions</b>									
1	101	67.9	83	52.02	7.80	126.8	82.80	5	57.37
2	102	74.7	88	34.64	5.20	102.9	72.13	5	34.97
3	103	86.6	94	16.21	3.24	126.8	109.23	3	16.52
4	104	87.2	95	13.37	2.67	126.8	112.06	2	14.19
5	105	84.6	93	19.12	3.82	126.8	106.43	4	18.89
									84

The CN values used for each subcatchment are the weighted values calculated based upon the different soils and land use.

Post-Development Condition	CN for Condition I	CN for Condition II	CN for Condition III	CN for Condition II	CN for Condition III	CN for Condition II	CN for Condition III	CN for Condition II	CN for Condition III	CN for Condition II	CN for Condition III	CN for Condition II	CN for Condition III	CN for Condition II	CN for Condition III	CN for Condition II	CN for Condition III	CN for Condition II	CN for Condition III	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	2	5	13	5	13	5	13	4	10	22	10	22	10	22	15	30	15	30	15	30
2	4	6	15	6	15	6	15	5	10	20	5	10	20	5	10	20	5	10	20	5
3	75	88	99	75	88	99	75	88	99	75	88	99	75	88	99	75	88	99	75	88
4	9	20	37	9	20	37	9	20	37	9	20	37	9	20	37	9	20	37	9	20
5	12	25	43	12	25	43	12	25	43	12	25	43	12	25	43	12	25	43	12	25
6	15	30	50	15	30	50	15	30	50	15	30	50	15	30	50	15	30	50	15	30
7	16	32	52	16	32	52	16	32	52	16	32	52	16	32	52	16	32	52	16	32
8	17	33	53	17	33	53	17	33	53	17	33	53	17	33	53	17	33	53	17	33
9	19	35	55	19	35	55	19	35	55	19	35	55	19	35	55	19	35	55	19	35
10	20	37	57	20	37	57	20	37	57	20	37	57	20	37	57	20	37	57	20	37
11	21	38	58	21	38	58	21	38	58	21	38	58	21	38	58	21	38	58	21	38
12	22	40	60	22	40	60	22	40	60	22	40	60	22	40	60	22	40	60	22	40
13	23	41	61	23	41	61	23	41	61	23	41	61	23	41	61	23	41	61	23	41
14	24	42	62	24	42	62	24	42	62	24	42	62	24	42	62	24	42	62	24	42
15	25	43	63	25	43	63	25	43	63	25	43	63	25	43	63	25	43	63	25	43
16	26	45	65	26	45	65	26	45	65	26	45	65	26	45	65	26	45	65	26	45
17	27	46	66	27	46	66	27	46	66	27	46	66	27	46	66	27	46	66	27	46
18	28	47	67	28	47	67	28	47	67	28	47	67	28	47	67	28	47	67	28	47
19	29	48	68	29	48	68	29	48	68	29	48	68	29	48	68	29	48	68	29	48
20	30	49	69	30	49	69	30	49	69	30	49	69	30	49	69	30	49	69	30	49
21	31	50	70	31	50	70	31	50	70	31	50	70	31	50	70	31	50	70	31	50
22	32	51	71	32	51	71	32	51	71	32	51	71	32	51	71	32	51	71	32	51
23	33	52	72	33	52	72	33	52	72	33	52	72	33	52	72	33	52	72	33	52
24	34	53	73	34	53	73	34	53	73	34	53	73	34	53	73	34	53	73	34	53
25	35	54	74	35	54	74	35	54	74	35	54	74	35	54	74	35	54	74	35	54
26	36	55	75	36	55	75	36	55	75	36	55	75	36	55	75	36	55	75	36	55
27	37	56	76	37	56	76	37	56	76	37	56	76	37	56	76	37	56	76	37	56
28	38	57	77	38	57	77	38	57	77	38	57	77	38	57	77	38	57	77	38	57
29	39	58	78	39	58	78	39	58	78	39	58	78	39	58	78	39	58	78	39	58
30	40	59	79	40	59	79	40	59	79	40	59	79	40	59	79	40	59	79	40	59
31	41	60	80	41	60	80	41	60	80	41	60	80	41	60	80	41	60	80	41	60
32	42	61	81	42	61	81	42	61	81	42	61	81	42	61	81	42	61	81	42	61
33	43	62	82	43	62	82	43	62	82	43	62	82	43	62	82	43	62	82	43	62
34	44	63	83	44	63	83	44	63	83	44	63	83	44	63	83	44	63	83	44	63
35	45	64	84	45	64	84	45	64	84	45	64	84	45	64	84	45	64	84	45	64
36	46	65	85	46	65	85	46	65	85	46	65	85	46	65	85	46	65	85	46	65
37	47	66	86	47	66	86	47	66	86	47	66	86	47	66	86	47	66	86	47	66
38	48	67	87	48	67	87	48	67	87	48	67	87	48	67	87	48	67	87	48	67
39	49	68	88	49	68	88	49	68	88	49	68	88	49	68	88	49	68	88	49	68
40	50	69	89	50	69	89	50	69	89	50	69	89	50	69	89	50	69	89	50	69
41	51	70	90	51	70	90	51	70	90	51	70	90	51	70	90	51	70	90	51	70
42	52	71	91	52	71	91	52	71	91	52	71	91	52	71	91	52	71	91	52	71
43	53	72	92	53	72	92	53	72	92	53	72	92	53	72	92	53	72	92	53	72
44	54	73	93	54	73	93	54	73	93	54	73	93	54	73	93	54	73	93	54	73
45	55	74	94	55	74	94	55	74	94	55	74	94	55	74	94	55	74	94	55	74
46	56	75	95	56	75	95	56	75	95	56	75	95	56	75	95	56	75	95	56	75
47	57	76	96	57	76	96	57	76	96	57	76	96	57	76	96	57	76	96	57	76
48	58	77	97	58	77	97	58	77	97	58	77	97	58	77	97	58	77	97	58	77
49	59	78	98	59	78	98	59	78	98	59	78	98	59	78	98	59	78	98	59	78
50	60	79	99	60	79	99	60	79	99	60	79	99	60	79	99	60	79	99	60	79
51	61	80	100	61	80	100	61	80	100	61	80	100	61	80	100	61	80	100	61	80
52	62	81	100	62	81	100	62	81	100	62	81	100	62	81	100	62	81	100	62	81
53	63	82	100	63	82	100	63	82	100	63	82	100	63	82	100	63	82	100	63	82
54	64	83	100	64	83	100	64	83	100	64	83	100	64	83	100	64	83	100	64	83
55	65	84	100	65	84	100	65	84	100	65	84	100	65	84	100	65	84	100	65	84
56	66	85	100	66	85	100	66	85	100	66	85	100	66	85	100	66	85	100	66	85
57	67	86	100	67	86	100	67	86	100	67	86	100	67	86	100	67	86	100	67	86
58	68	87	100	68	87	100	68	87	100	68	87	100	68	87	100	68	87	100	68	87
59	69	88	100	69	88	10														

**FIGURE 6**  
**DAVENPORT SUBDIVISION**

Subwatershed	Area (ha)	Average Slope (%)	Travel Length (m)	Runoff Coefficient - 'C'				Time to Peak (hr)		
				2/5/10 Year	25 Year	50 Year	100 Year	2/5/10 Year	25 Year	50 Year
<b>Post-Development</b>										
1	4.823	3.00	475	0.369	0.406	0.443	0.461	0.404	0.383	0.363
2	1.396	2.50	230	0.410	0.451	0.492	0.513	0.281	0.265	0.248
5	1.394	3.00	295	0.441	0.485	0.529	0.551	0.287	0.268	0.248

**Bransby-Williams Method**  
**Post-Development Urban Watersheds**

Subwatershed	Average Slope (%)	Travel Length (m)	Velocity (m/s)	Time to Peak (hr)	
				3	4
3	2.0	440.0	0.477		
4	2.0	275.0	0.346		

### Design Chart 1.07: Runoff Coefficients

#### - Urban for 5 to 10-Year Storms

Land Use	Runoff Coefficient	
	Min.	Max.
Pavement - asphalt or concrete	0.80	0.95
- brick	0.70	0.85
Gravel roads and shoulders	0.40	0.60
Roofs	0.70	0.95
Business - downtown	0.70	0.95
- neighbourhood	0.50	0.70
- light	0.50	0.80
- heavy	0.60	0.90
Residential - single family urban	0.30	0.50
- multiple, detached	0.40	0.60
- multiple, attached	0.60	0.75
- suburban	0.25	0.40
Industrial - light	0.50	0.80
- heavy	0.60	0.90
Apartments	0.50	0.70
Parks, cemeteries	0.10	0.25
Playgrounds (unpaved)	0.20	0.35
Railroad yards	0.20	0.35
Unimproved areas	0.10	0.30
Lawns - Sandy soil		
- flat, to 2%	0.05	0.10
- average, 2 to 7%	0.10	0.15
- steep, over 7%	0.15	0.20
- Clayey soil		
- flat, to 2%	0.13	0.17
- average, 2 to 7%	0.18	0.22
- steep, over 7%	0.25	0.35

For flat or permeable surfaces, use the lower values. For steeper or more impervious surfaces, use the higher values. For return period of more than 10 years, increase above values as 25-year - add 10%, 50-year - add 20%, 100-year - add 25%.

The coefficients listed above are for unfrozen ground.

**Design Chart 1.07: Runoff Coefficients (Continued)****- Rural**

Land Use & Topography <sup>3</sup>	Soil Texture		
	Open Sand Loam	Loam or Silt Loam	Clay Loam or Clay
CULTIVATED			
Flat 0 - 5% Slopes	0.22	0.35	0.55
Rolling 5 - 10% Slopes	0.30	0.45	0.60
Hilly 10- 30% Slopes	0.40	0.65	0.70
PASTURE			
Flat 0 - 5% Slopes	0.10	0.28	0.40
Rolling 5 - 10% Slopes	0.15	0.35	0.45
Hilly 10- 30% Slopes	0.22	0.40	0.55
WOODLAND OR CUTOVER			
Flat 0 - 5% Slopes	0.08	0.25	0.35
Rolling 5 - 10% Slopes	0.12	0.30	0.42
Hilly 10- 30% Slopes	0.18	0.35	0.52
BARE ROCK	COVERAGE <sup>3</sup>		
	30%	50%	70%
Flat 0 - 5% Slopes	0.40	0.55	0.75
Rolling 5 - 10% Slopes	0.50	0.65	0.80
Hilly 10- 30% Slopes	0.55	0.70	0.85
LAKES AND WETLANDS	0.05		

<sup>2</sup> Terrain Slopes

<sup>3</sup> Interpolate for other values of % imperviousness

Sources: American Society of Civil Engineers - ASCE (1960)  
U.S. Department of Agriculture (1972)

## Design Chart 1.08: Hydrologic Soil Groups

### - Based on Surficial Geology Maps

Map Ref.No.	Soil Type or Texture	Hydrologic Soil Group (Tentative)
1a	<u>Ground Moraine</u> Usually sandy till, stony, varying depth. (Most widespread type in Shield).	Usually B (shallow); may be A or AB
1b	Clayey till, varying depth.	BC-C
2a	<u>End or Interlobate Moraine</u>	A
2b	Sand & stones, deep. (May be rough topography). Sand & stones capped by till, deep.	A-C depending on type of till.
2c	Sand & stones, deep. (Smoothen topography).	A
3a	<u>Kames &amp; Eskers</u>	A
3b	Sand & stones, deep. (May be rough topography). Sand & stones capped by till, deep.	A-C depending on type of till.
3c	Sand & stones, deep. (Smoothen topography).	A
4a	<u>Lacustrine</u> Clay & silt, in lowlands.	BC-C
4b	Fine sand, in lowlands.	AB-B
4c	Sand, in lowlands.	AB
4d	Sand (deltas & valley trains).	A-AB
5	<u>Outwash</u> Sand, some gravel, deep.	A
6	<u>Aeolian</u> Very fine sand & silt, shallow. (Loess)	B
7	<u>Bedrock</u> Bare bedrock (normally negligible areas).	Varies according to rock type.

Source: Ministry of Natural Resources - MNR

**Design Chart 1.08: Hydrologic Soil Groups (Continued)****- Based on Soil Texture**

<u>Sands, Sandy Loams and Gravels</u>	
- overlying sand, gravel or limestone bedrock, very well drained	A
- ditto, imperfectly drained	AB
- shallow, overlying Precambrian bedrock or clay subsoil	B
<u>Medium to Coarse Loams</u>	
- overlying sand, gravel or limestone, well drained	AB
- shallow, overlying Precambrian bedrock or clay subsoil	B
<u>Medium Textured Loams</u>	
- shallow, overlying limestone bedrock	B
- overlying medium textured subsoil	BC
<u>Silt Loams, Some Loams</u>	
- with good internal drainage	BC
- with slow internal drainage and good external drainage	C
<u>Clays, Clay Loams, Silty Clay Loams</u>	
- with good internal drainage	C
- with imperfect or poor external drainage	C
- with slow internal drainage and good external drainage	D

Source: U.S. Department of Agriculture (1972)

### Design Chart 1.09: Soil/Land Use Curve Numbers

Land Use	Treatment or Practice	Hydrologic Condition <sup>4</sup>	Hydrologic Soil Group			
			A	B	C	D
Fallow	Straight row	---	77	86	91	94
Row crops	"	Poor	72	81	88	91
	"	Good	67	78	85	89
	Contoured	Poor	70	79	84	88
	"	Good	65	75	82	86
	" and terraced	Poor	66	74	8	82
	" " "	Good	62	71	78	81
Small grain	Straight row	Poor	65	76	84	88
		Good	63	75	83	87
	Contoured	Poor	63	74	82	85
		Good	61	73	81	84
	" and terraced	Poor	61	72	79	82
		Good	59	70	78	81
Close-seeded legumes <sup>2</sup> or rotation meadow	Straight row	Poor	66	77	85	89
	" "	Good	58	72	81	85
	Contoured	Poor	64	75	83	85
	"	Good	55	69	78	83
	" and terraced	Poor	63	73	80	83
	" and terraced	Good	51	67	76	80
Pasture or range		Poor	68	79	86	89
		Fair	49	69	79	84
	Contoured	Good	39	61	74	80
	"	Poor	47	67	81	88
	"	Fair	25	59	75	83
		Good	6	35	70	79
Meadow		Good	30	58	71	78
Woods		Poor	45	66	77	83
		Fair	36	60	73	79
		Good	25	55	70	77
Farmsteads	---	---	59	74	82	86
		---	72	82	87	89
		---	74	84	90	92

For average antecedent soil moisture condition (AMC II)

<sup>2</sup> Close-drilled or broadcast.

<sup>4</sup> The hydrologic condition of cropland is good if a good crop rotation practice is used; it is poor if one crop is grown continuously.

Source: U.S. Department of Agriculture (1972)

**Design Chart 1.09: Soil Conservation Service Curve Numbers (Continued)**

Land Use or Surface	Hydrologic Soil Group						
	A	AB	B	BC	C	CD	D
Fallow (special cases only)	77	82	86	89	91	93	94
Crop and other improved land	66** (62)	70** (68)	74	78	82	84	86 AMC I
Pasture & other unimproved land	58* (38)	62* (51)	65	71	76	79	81
Woodlots and forest	50* (30)	54* (44)	58	65	71	74	77
Impervious areas (paved)							98
Bare bedrock draining directly to stream by surface flow							98
Bare bedrock draining indirectly to stream as groundwater (usual case)							70
Lakes and wetlands							50

Notes

- (i) All values are based on AMC II except those marked by \* (AMC III) or \*\* (mean of AMC II and AMC III).
- (ii) Values in brackets are AMC II and are to be used only for special cases.
- (iii) Table is not applicable to frozen soils or to periods in which snowmelt contributes to runoff.

idf\_v2-3\_2014\_12\_21\_611\_ON\_6116132\_OWEN\_SOUND\_MOE  
 Environment Canada/Environnement Canada

Short Duration Rainfall Intensity-Duration-Frequency Data  
 Données sur l'intensité, la durée et la fréquence des chutes  
 de pluie de courte durée

Gumbel - Method of moments/Méthode des moments

2014/12/21

=====

OWEN SOUND MOE ON 6116132

Latitude: 44 35'N Longitude: 80 56'W Elevation/Altitude: 178 m

Years/Années : 1965 - 2006 # Years/Années : 37

\*\*\*\*\*

Table 1 : Annual Maximum (mm)/Maximum annuel (mm)

\*\*\*\*\*

Year Année	5 min	10 min	15 min	30 min	1 h	2 h	6 h	12 h	24 h
1965	12.7	16.0	23.9	28.7	32.3	35.1	35.1	35.1	35.1
1966	6.9	8.9	13.2	18.8	21.8	22.1	30.5	32.0	32.3
1967	11.4	15.7	21.3	38.1	43.9	43.9	43.9	46.5	52.6
1968	14.7	19.6	24.4	31.2	43.9	56.4	63.8	68.1	75.9
1969	6.6	13.0	17.0	22.9	30.2	39.4	49.3	71.9	71.9
1970	10.2	18.8	25.4	32.5	41.4	42.7	42.7	55.6	55.6
1971	7.6	12.2	17.3	26.9	36.1	39.1	55.6	55.6	55.9
1972	7.4	13.2	18.3	19.3	20.1	23.6	36.8	42.7	42.7
1973	5.8	10.2	12.4	16.3	16.5	16.5	18.3	29.7	33.5
1974	6.6	10.4	11.7	16.3	18.8	23.9	43.9	43.9	45.0
1975	6.9	9.4	9.4	11.2	17.0	17.0	24.6	25.4	25.4
1976	7.1	13.2	17.3	22.4	22.6	22.6	29.2	31.7	34.8
1977	13.0	14.7	18.0	22.9	22.9	25.1	26.9	37.3	37.3
1979	18.4	26.0	26.4	30.4	32.1	32.2	41.1	47.1	48.3
1980	9.4	16.1	19.8	30.8	32.0	41.3	45.7	45.7	72.4
1981	-99.9	-99.9	-99.9	-99.9	14.5	19.7	29.4	40.6	41.4
1982	11.8	11.8	12.0	12.0	12.6	23.0	52.6	56.6	56.8
1983	5.6	7.8	8.2	15.7	27.3	38.2	46.8	50.0	53.4
1984	6.9	11.4	15.6	22.3	36.4	45.1	47.0	47.0	47.0
1985	10.1	16.0	18.0	22.4	25.9	32.1	44.8	62.4	73.0
1986	4.6	8.4	11.2	12.4	16.2	16.3	39.2	43.3	60.9
1987	9.0	13.5	15.1	15.1	15.5	15.8	17.0	28.0	28.0
1988	11.4	14.2	18.0	21.0	24.8	27.7	35.9	45.0	54.0
1989	6.9	12.1	12.7	13.5	13.9	14.0	-99.9	-99.9	47.2
1990	10.6	15.0	18.7	27.4	34.1	35.9	40.0	45.4	45.4
1991	5.6	7.0	8.1	8.3	10.5	18.0	27.3	28.6	38.9
1992	4.8	7.4	8.4	8.9	14.1	18.2	27.9	43.3	47.5
1993	7.7	15.4	23.1	25.9	27.9	28.6	33.1	39.0	49.9
1994	5.2	10.4	15.4	27.4	32.4	32.6	35.7	35.7	48.0
1995	7.6	12.0	12.5	12.5	16.4	21.6	30.5	33.2	38.7
1996	10.8	15.3	18.1	27.8	32.5	41.7	47.0	55.9	55.9
1999	7.2	11.1	15.2	20.6	21.7	21.7	36.5	40.8	42.4
2000	7.2	14.1	18.0	33.0	53.0	70.3	79.3	79.5	80.5
2001	5.2	9.0	11.6	14.6	21.4	24.4	30.8	35.6	42.0
2002	8.2	11.0	12.8	15.8	16.4	25.8	53.0	54.8	65.2

	idf_v2-3_2014_12_21_611_ON_6116132_Owen_Sound_MOE									
2003	11.2	16.3	20.6	24.5	30.5	32.2	32.4	32.4	48.1	
2004	6.5	9.7	11.3	16.9	27.8	35.4	54.6	70.8	76.2	
2006	12.2	17.4	20.0	30.6	53.1	74.8	74.8	76.6	85.8	
# Yrs. Années	37	37	37	37	38	38	37	37	38	
Mean Moyenne	8.7	13.1	16.2	21.5	26.6	31.4	40.6	46.3	51.2	
Std. Dev. Écart-type	3.1	3.9	4.9	7.6	10.9	14.0	13.8	14.1	15.1	
Skew. Dissymétrie	1.08	0.96	0.23	0.13	0.73	1.39	0.89	0.76	0.58	
Kurtosis	4.39	5.17	2.55	2.32	3.23	5.37	4.30	3.09	2.87	

\*-99.9 Indicates Missing Data/Données manquantes

Warning: annual maximum amount greater than 100-yr return period amount

Avertissement : la quantité maximale annuelle excède la quantité pour une période de retour de 100 ans

Year/Année	Duration/Durée	Data/Données	100-yr/ans
1979	5 min	18.4	18.4
1979	10 min	26.0	25.2

\*\*\*\*\*

Table 2a : Return Period Rainfall Amounts (mm)  
Quantité de pluie (mm) par période de retour

\*\*\*\*\*

Duration/Durée	2 yr/ans	5 yr/ans	10 yr/ans	25 yr/ans	50 yr/ans	100 yr/ans	#Years Années
5 min	8.2	10.9	12.7	15.0	16.7	18.4	37
10 min	12.4	15.9	18.1	21.0	23.1	25.2	37
15 min	15.4	19.8	22.7	26.3	29.0	31.7	37
30 min	20.3	27.0	31.5	37.1	41.3	45.5	37
1 h	24.8	34.5	40.8	48.9	54.9	60.9	38
2 h	29.1	41.5	49.7	60.1	67.8	75.5	38
6 h	38.4	50.5	58.6	68.7	76.3	83.8	37
12 h	44.0	56.5	64.7	75.2	83.0	90.7	37
24 h	48.7	62.0	70.9	82.0	90.3	98.5	38

\*\*\*\*\*

Table 2b :

Return Period Rainfall Rates (mm/h) - 95% Confidence limits  
Intensité de la pluie (mm/h) par période de retour - Limites de confiance de 95%

\*\*\*\*\*

Duration/Durée	2 yr/ans	5 yr/ans	10 yr/ans	25 yr/ans	50 yr/ans	100 yr/ans	#Years Années
5 min	98.0	130.8	152.4	179.8	200.2	220.3	37
	+/- 11.0	+/- 18.5	+/- 24.9	+/- 33.6	+/- 40.2	+/- 46.9	37
10 min	74.6	95.2	108.7	125.9	138.7	151.3	37
	+/- 6.9	+/- 11.6	+/- 15.6	+/- 21.1	+/- 25.2	+/- 29.4	37
15 min	61.7	79.1	90.6	105.2	116.0	126.8	37
	+/- 5.8	+/- 9.8	+/- 13.3	+/- 17.9	+/- 21.4	+/- 24.9	37
30 min	40.6	54.1	63.0	74.3	82.7	91.0	37
	+/- 4.5	+/- 7.6	+/- 10.3	+/- 13.8	+/- 16.6	+/- 19.3	37
1 h	24.8	34.5	40.8	48.9	54.9	60.9	38
	+/- 3.2	+/- 5.4	+/- 7.3	+/- 9.8	+/- 11.7	+/- 13.6	38

	idf_v2-3_2014_12_21_611_ON_6116132_Owen_SOUND_MOE							
2 h	14.6 +/-	20.8 +/-	24.9 +/-	30.1 +/-	33.9 +/-	37.7 +/-	8.8 +/-	38
6 h	6.4 +/-	8.4 +/-	9.8 +/-	11.5 +/-	12.7 +/-	14.0 +/-	2.9 +/-	37
12 h	3.7 +/-	4.7 +/-	5.4 +/-	6.3 +/-	6.9 +/-	7.6 +/-	1.5 +/-	37
24 h	2.0 +/-	2.6 +/-	3.0 +/-	3.4 +/-	3.8 +/-	4.1 +/-	0.8 +/-	38
	0.2 +/-	0.3 +/-	0.4 +/-	0.6 +/-	0.7 +/-	0.8 +/-		

\*\*\*\*\*

Table 3 : Interpolation Equation / Équation d'interpolation:  $R = A \cdot T^B$

$R$  = Interpolated Rainfall rate (mm/h) / Intensité interpolée de la pluie (mm/h)

$RR$  = Rainfall rate (mm/h) / Intensité de la pluie (mm/h)

$T$  = Rainfall duration (h) / Durée de la pluie (h)

\*\*\*\*\*

Statistics/Statistiques	2 yr/ans	5 yr/ans	10 yr/ans	25 yr/ans	50 yr/ans	100 yr/ans
Mean of RR/Moyenne de RR	36.3	47.8	55.4	65.0	72.2	79.3
Std. Dev. /Écart-type (RR)	34.8	45.4	52.5	61.4	68.1	74.7
Std. Error/Erreur-type	10.4	13.9	16.3	19.4	21.7	24.0
Coefficient (A)	21.8	28.8	33.5	39.3	43.7	48.0
Exponent/Exposant (B)	-0.701	-0.703	-0.704	-0.705	-0.706	-0.706
Mean % Error/% erreur moyenne	10.2	12.2	13.1	13.8	14.3	14.8

## 4.8 Enhanced Grass Swale

### 4.8.1 Overview

#### Description

Enhanced grass swales are vegetated open channels designed to convey, treat and attenuate stormwater runoff (also referred to as enhanced vegetated swales). Check dams and vegetation in the swale slows the water to allow sedimentation, filtration through the root zone and soil matrix, evapotranspiration, and infiltration into the underlying native soil. Simple grass channels or ditches have long been used for stormwater conveyance, particularly for roadway drainage. Enhanced grass swales incorporate design features such as modified geometry and check dams that improve the contaminant removal and runoff reduction functions of simple grass channel and roadside ditch designs (Figure 4.8.1). A dry swale is a design variation that incorporates an engineered soil media bed and optional perforated pipe underdrain system (see Section 4.9 – Dry Swale). Enhanced grass swales are not capable of providing the same water balance and water quality benefits as dry swales, as they lack the engineered soil media and storage capacity of that best management practice.

Where development density, topography and depth to water table permit, enhanced grass swales are a preferred alternative to both curb and gutter and storm drains as a stormwater conveyance system. When incorporated into a site design, they can reduce impervious cover, accent the natural landscape, and provide aesthetic benefits.

**Figure 4.8.1 Enhanced grass swales can be applied in road rights-of-way or along parking lots**



Source: Seattle Public Utilities (left); Sue Donaldson (right)

**Figure 4.8.2 Enhanced grass swales feature check dams that temporarily pond runoff to increase pollutant retention and infiltration and decrease flow velocity**



Source: Delaware Department of Transportation (left); Center for Watershed Protection (right)

### Common Concerns

If they are properly designed and maintained, enhanced grass swales can provide stormwater treatment and improved site aesthetics. However, there are some common concerns associated with their use:

- *Risk of Groundwater Contamination:* Most pollutants in urban runoff are well retained by infiltration practices and soils and therefore, have a low to moderate potential for groundwater contamination (Pitt *et al.*, 1999). Chloride and sodium from de-icing salts applied to roads and parking areas during winter are not well attenuated in soil and can easily travel to shallow groundwater. Infiltration of de-icing salt constituents is also known to increase the mobility of certain heavy metals in soil (e.g., lead, copper and cadmium), thereby raising the potential for elevated concentrations in underlying groundwater (Amrhein *et al.*, 1992; Bauske and Goetz, 1993). However, very few studies that have sampled groundwater below infiltration facilities or roadside ditches receiving de-icing salt laden runoff have found concentrations of heavy metals that exceed drinking water standards (e.g., Howard and Beck, 1993; Granato *et al.*, 1995). To minimize risk of groundwater contamination the following management approaches are recommended (Pitt *et al.*, 1999; TRCA, 2009b):
  - stormwater infiltration practices should not receive runoff from high traffic areas where large amounts of de-icing salts are applied (e.g., busy highways), nor from pollution hot spots (e.g., source areas where land uses or activities have the potential to generate highly contaminated runoff such as vehicle fuelling, servicing or demolition areas, outdoor storage or handling areas for hazardous materials and some heavy industry sites);
  - prioritize infiltration of runoff from source areas that are comparatively less contaminated such as roofs, low traffic roads and parking areas; and,
  - apply sedimentation pretreatment practices (e.g., oil and grit separators) before infiltration of road or parking area runoff.

- *Risk of Soil Contamination:* Available evidence from monitoring studies indicates that small distributed stormwater infiltration practices do not contaminate underlying soils, even after more than 10 years of operation (TRCA, 2008).
- *On Private Property:* If enhanced grass swales are installed on private lots, property owners or managers will need to be educated on their routine maintenance needs, understand the long-term maintenance plan, and may be subject to a legally binding maintenance agreement. An incentive program such as a storm sewer user fee based on the area of impervious cover on a property that is directly connected to a storm sewer (*i.e.*, does not first drain to a pervious area or LID practice) could be used to encourage property owners or managers to maintain existing practices. Alternatively, swales could be located in an expanded road right-of-way or “stormwater easement” so that municipal staff can access the facility in the event it fails to function properly.
- *Maintenance:* The major maintenance requirement associated with grass swales is mowing. Occasionally, sediment will need to be removed, although this can be minimized by ensuring that upstream areas are stabilized and incorporating pretreatment devices (*e.g.*, vegetated filter strips, sedimentation forebays, gravel diaphragms). If grass swales are installed on private lots, homeowners need to be educated on routine maintenance requirements.
- *Erosion:* Erosion can be prevented by limiting the allowable longitudinal slope and incorporating check dams. Additionally, designers can use permanent reinforcement matting on swales designed for high velocity flows and temporary matting during the vegetation establishment period.
- *Standing Water and Mosquitoes:* Properly designed grass swales will not pond water for longer than 24 hours following a storm event. However, poor design, installation, or maintenance can lead to nuisance conditions.

### **Physical Suitability and Constraints**

Enhanced grass swales are suitable on sites where development density, topography and water table depth permit their implementation. Some key constraints to their application include:

- *Available Space:* Grass swales usually consume about 5 to 15 percent of their contributing drainage area. A width of at least 2 metres is needed.
- *Site Topography:* Site topography constrains the application of grass swales. Longitudinal slopes between 0.5 and 6% are allowable. This prevents ponding while providing residence time and preventing erosion. On slopes steeper than 3%, check dams should be used.

- *Water Table:* Designers should ensure that the bottom of the swale is separated from the seasonally high water table or top of bedrock elevation by at least one (1) metre.
- *Soils:* Grass swales can be applied on sites with any type of soils.
- *Drainage Area and Runoff Volume:* The conveyance capacity should match the drainage area. Sheet flow to the grass swale is preferable. If drainage areas are greater than 2 hectares, high discharge through the swale may not allow for filtering and infiltration, and may create erosive conditions. Typical ratios of impervious drainage area to swale area range from 5:1 to 10:1.
- *Pollution Hot Spot Runoff:* To protect groundwater from possible contamination, source areas where land uses or human activities have the potential to generate highly contaminated runoff (e.g., vehicle fueling, servicing and demolition areas, outdoor storage and handling areas for hazardous materials and some heavy industry sites) should not be treated by grass swales.
- *Setbacks from Buildings:* Enhanced grass swales should be located a minimum of four (4) metres from building foundations to prevent water damage.
- *Proximity to Underground Utilities:* Utilities running parallel to the grass swale should be offset from the centerline of the swale. Underground utilities below the bottom of the swale are not a problem.

### Typical Performance

The ability of enhanced grass swales to help meet stormwater management objectives is summarized in Table 4.8.1.

**Table 4.8.1 Ability of enhanced grass swales to meet SWM objectives**

BMP	Water Balance Benefit	Water Quality Improvement	Stream Channel Erosion Control Benefit
Enhanced Grass Swale	Partial – depends on soil infiltration rate	Yes, if design velocity is 0.5 m/s or less for a 4 hour, 25 mm Chicago storm	Partial – depends on soil infiltration rate

### Water Balance

Runoff reduction by grass swales is generally low, but is strongly influenced by soil type, slope, vegetative cover and the length of the swale. Recent research indicates that a conservative runoff reduction rate of 20 to 10% can be used depending on whether soils fall in hydrologic soil groups A/B or C/D, respectively. The runoff reduction rates can be doubled if the native soils on which the swale is located have been tilled to a depth of 300 mm and amended with compost to achieve an organic content of between 8 and 15% by weight or 30 to 40% by volume.

**Table 4.8.2 Volumetric runoff reduction achieved by enhanced grass swales**

LID Practice	Location	% Runoff Reduction	Reference
Grass Swale	Virginia	0%	Schueler (1983)
Grass Swale	Various	40%	Strecker <i>et al.</i> (2004)
Grass Swale	California	27 to 41%	Barrett <i>et al.</i> (2004)
<b>Runoff Reduction Estimate<sup>1</sup></b>		<b>20% on HSG A or B soils; 10% on HSG C or D soils</b>	

## Notes:

1. This estimate is provided only for the purpose of initial screening of LID practices suitable for achieving stormwater management objectives and targets. Performance of individual facilities will vary depending on site specific contexts and facility design parameters and should be estimated as part of the design process and submitted with other documentation for review by the approval authority.

**Water Quality – Pollutant Removal Capacity**

Research has shown the pollutant mass removal rates of grass swales are variable, depending on influent pollutant concentrations (Bäckström *et al.*, 2006), but generally moderate for most pollutants (Barrett *et al.*, 1998; Deletic and Fletcher, 2006). Median pollutant mass removal rates of swales from available performance studies are 76% for total suspended solids, 55% for total phosphorus, and 50% for total nitrogen (Deletic and Fletcher, 2006). Significant reductions in total zinc and copper event mean concentrations have been observed in performance studies with a median value of 60%, but results have varied widely (Barrett, 2008). Site specific factors such as slope, soil type, infiltration rate, swale length and vegetative cover also affect pollutant mass removal rates. In general, the dominant pollutant removal mechanism operating in grass swales is infiltration, rather than filtration, because pollutants trapped on the surface of the swale by vegetation or check dams are not permanently bound (Bäckström *et al.*, 2006). Designers should maximize the degree of infiltration achieved within a grass swale by incorporating check dams and ensuring the native soils have infiltration rates of 15 mm/hr or greater or specifying that the soils be tilled and amended with compost prior to planting.

Several of the factors that can significantly increase or decrease the pollutant removal capacity of grass channels are provided in Table 4.8.3.

**Table 4.8.3 Factors that influence the pollutant removal capacity of grass swales**

Factors that Reduce Removal Rates	Factors that Enhance Removal Rates
Longitudinal slope > 1%	Longitudinal slope < 1%
Measured soil infiltration rate < 15 mm/hr	Measured soil infiltration rate is 15 mm/hr or greater
Flow velocity within channel > 0.5 m/s during a 4 hour, 25 mm Chicago storm event	Flow velocity within channel is 0.5 m/s or less during a 4 hour, 25 mm Chicago storm event
No pretreatment	Pretreatment with vegetated filter strips, gravel diaphragms and/or sedimentation forebays
Side slopes steeper than 3:1 (H:V)	Side slopes 3:1 (H:V) or less

## 4.8.2 Design Template

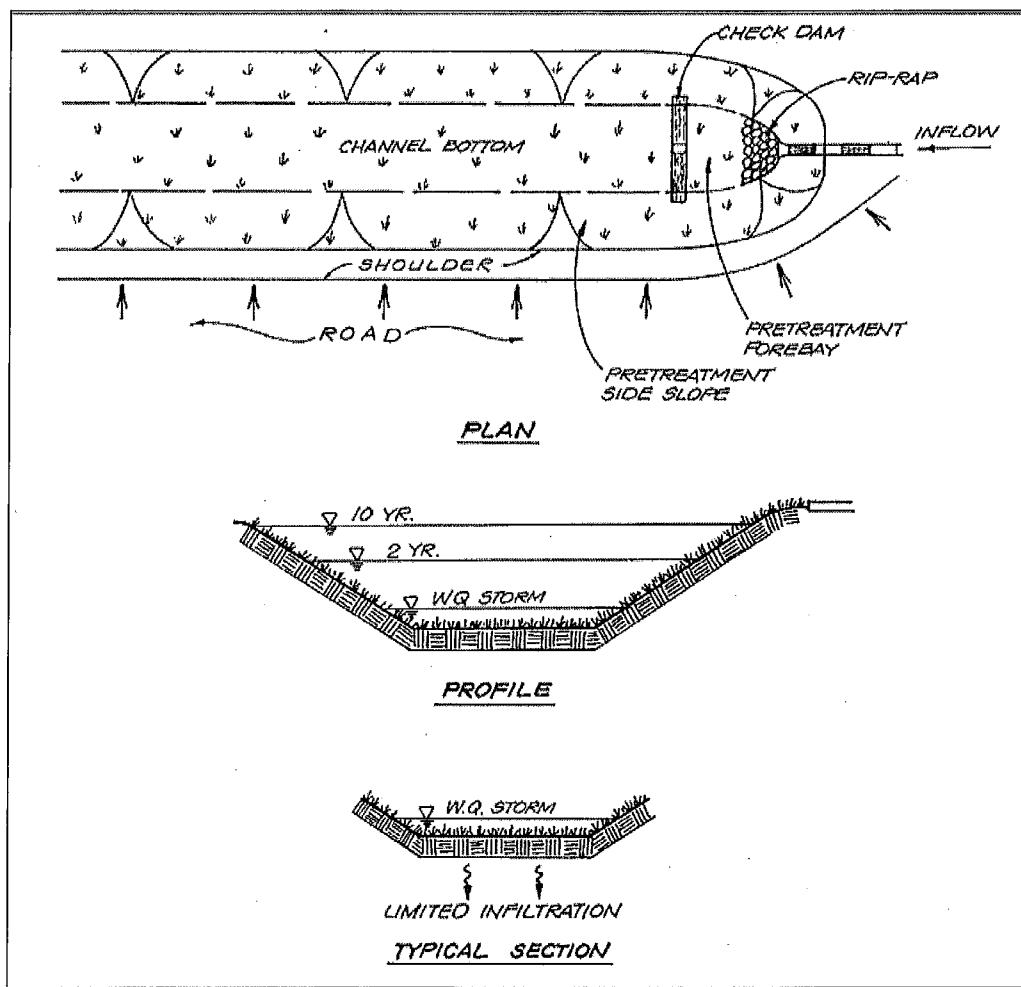
### Applications

Enhanced grass swales are well suited for conveying and treating runoff from highways and other roads because they are a linear practice and easily incorporated into road rights-of-way. They are also a suitable practice for managing runoff from parking lots, roofs and pervious surfaces, such as yards, parks and landscaped areas. Grass swales can be used as snow storage areas.

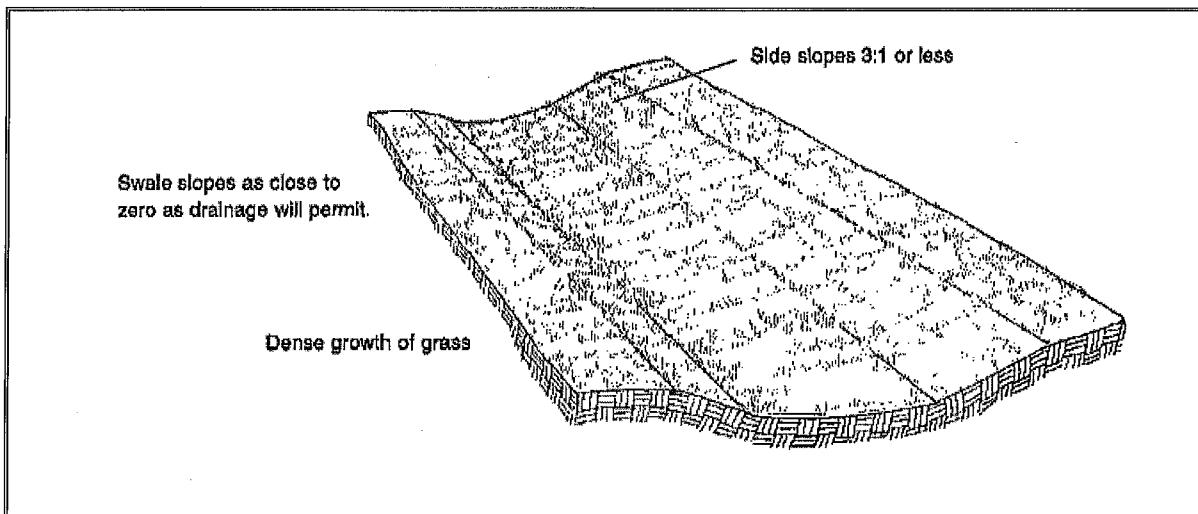
Grass swales can also provide pretreatment for other stormwater best management practices, such as bioretention areas, soakaways and perforated pipe systems or be designed in series with other practices as part of a treatment train approach. They are often impractical in densely developed urban areas because they consume a large amount of space. Where development density and topography permit, grass swales can be used in place of conventional curb and gutter and storm drain systems.

### Typical Details

**Figure 4.8.3 Plan, profile, and section views of a grass swale**



Source: ARC, 2001

**Figure 4.8.4 Plan view of a grass swale**

Source: ARC, 2001

## Design Guidance

### **Geometry and Site Layout**

Design guidance regarding the geometry and layout of grass swales is provided below.

- **Shape:** Grass swales should be designed with a trapezoidal or parabolic cross section. Trapezoidal swales will generally evolve into parabolic swales over time, so the initial trapezoidal cross section design should be checked for capacity and conveyance assuming it is a parabolic cross section. Swale length between culverts should be 5 metres or greater.
- **Bottom Width:** Grass swales should be designed with a bottom width between 0.75 and 3.0 metres. The design width should allow for shallow flows and adequate water quality treatment, while preventing flows from concentrating and creating gullies.
- **Longitudinal Slope:** Slopes should be between 0.5% and 4%. Check dams should be incorporated on slopes greater than 3% (PDEP, 2006).
- **Length:** When used to convey and treat road runoff, the length simply parallels the road, and therefore should be equal to, or greater than the contributing roadway length.
- **Flow Depth:** The maximum flow depth should correspond to two-thirds the height of the vegetation. Vegetation in some grass swales may reach heights of 150 millimetres; therefore a maximum flow depth of 100 millimetres is recommended during a 4 hour, 25 mm Chicago storm event.

- **Side Slopes:** The side slopes should be as flat as possible to aid in providing pretreatment for lateral incoming flows and to maximize the swale filtering surface. Steeper side slopes are likely to have erosion gulling from incoming lateral flows. A maximum slope of 2.5:1 (H:V) is recommended and a 4:1 slope is preferred where space permits.

### **Pretreatment**

A pea gravel diaphragm located along the top of each bank can be used to provide pretreatment of any stormwater runoff that may be entering the swale laterally along its length. Vegetated filter strips or mild side slopes (3:1) also provide pretreatment for any lateral sheet flow entering the swale. Sedimentation forebays at inlets to the swale are also a pretreatment option.

### **Conveyance and Overflow**

Grass swales must be designed for a maximum velocity of 0.5 m/s or less for the 4 hour 25 mm Chicago storm. The swale should also convey the locally required design storm (usually the 10 year storm) at non-erosive velocities.

### **Soil Amendments**

If soils along the location of the swale are highly compacted, or of such low fertility that vegetation cannot become established, they should be tilled to a depth of 300 mm and amended with compost to achieve an organic content of 8 to 15% by weight or 30 to 40% by volume.

### **Landscaping**

Designers should choose grasses that can withstand both wet and dry periods as well as relatively high velocity flows within the swale. For applications along roads and parking lots, where snow will be plowed and stored, non woody and salt tolerant species should be chosen. Taller and denser grasses are preferable, though the species of grass is less important than percent coverage (Barrett *et al.*, 2004). Appendix B provides further guidance regarding suitable species and planting.

### **Other Design Resources**

Section 4.9.8 of the OMOE *Stormwater Management Planning and Design Manual* (2003) provides further guidance regarding design and modelling performance of enhanced grass swales. Several other stormwater manuals that provide useful design guidance for grass swales include:

Minnesota Stormwater Manual

<http://www.pca.state.mn.us/water/stormwater/stormwater-manual.html>

Virginia Stormwater Management Handbook

[http://www.dcr.virginia.gov/soil & water/stormwat.shtml](http://www.dcr.virginia.gov/soil_water/stormwat.shtml)

Georgia Stormwater Management Manual

<http://www.georgiastormwater.com/>

## BMP Sizing

Enhanced grass swale designs are flow rate based. The swale should be designed for a maximum flow velocity of 0.5 m/s and flow depth of 100 mm during a 4 hour 25 mm Chicago storm event. The suggested Manning's n for use in Manning's equation is 0.027 (grass swale) to 0.050 (shrub vegetated or cobble lined swale). Given typical urban swale dimensions (0.75 m bottom width, 2.5:1 side slopes and 0.5 m depth), the contributing drainage area is generally limited to  $\leq$  2 hectares to maintain flow  $\leq$  0.15 m<sup>3</sup>/s and velocity  $\leq$  0.5 m/s. Table 4.8.4 describes the relationship between imperviousness of the development and maximum drainage area that can be treated by a grass swale.

**Table 4.8.4 Grassed swale drainage area guidelines**

Percent Imperviousness	Maximum Drainage Area (hectares)
35	2.0
75	1.5
90	1.0

Source: OMOE, 2003.

For further guidance regarding BMP sizing, refer to the *OMOE Stormwater Management Planning and Design Manual* (OMOE, 2003).

## Design Specifications

Recommended design specifications for enhanced grass swales are provided in Table 4.8.5

**Table 4.8.5 Design specifications for enhanced grass swales**

Component	Specification	Quantity
Check Dams	<p>Check dams should be constructed of a non-erosive material such as suitably sized aggregate, wood, gabions, riprap, or concrete. All check dams should be underlain with filter fabric conforming to local design standards.</p> <p>Wood used for check dams should consist of pressure treated logs or timbers, or water-resistant tree species such as cedar, hemlock, swamp oak or locust.</p>	Spacing should be based on the longitudinal slope and desired ponding volume
Pea Gravel Diaphragm	Washed stone between 3 and 10 mm in diameter.	Minimum of 300 mm wide and 600 mm deep

## Construction Considerations

Grass swales should be clearly marked before site work begins to avoid disturbance during construction. No vehicular traffic, except that specifically used to construct the facility, should be allowed within the swale site. Any accumulation of sediment that does occur within the swale must be removed during the final stages of grading to achieve the design cross section. Final grading and planting should not occur until the adjoining

areas draining into the swale are stabilized. Flow should not be diverted into the swale until the banks are stabilized.

Preferably, the swale should be planted in the spring so that the vegetation can become established with minimal irrigation. Installation of erosion control matting or blanketing to stabilize soil during establishment of vegetation is highly recommended. If sod is used, it should be placed with staggered ends and secured by rolling the sod. This helps to prevent gullies.

#### 4.8.3 Maintenance and Construction Costs

##### Inspection and Maintenance

Maintenance requirements for enhanced grass swales is similar to vegetated filter strips and typically involve a low level of activity after vegetation becomes established. Grass channel maintenance procedures are already in place at many municipal public works and transportation departments. These procedures should be compared to the recommendations below (Table 4.8.6) to assure that the infiltration and water quality benefits of enhanced grass swales are preserved. Routine roadside ditch maintenance practices such as scraping and re-grading should be avoided at swale locations. Vehicles should not be parked or driven on grass swales. For routine mowing, the lightest possible mowing equipment should be used to prevent soil compaction.

For swales located on private property, the property owner or manager is responsible for maintenance as outlined in a legally binding maintenance agreement. Roadside swales in residential areas generally receive routine maintenance from homeowners who should be advised regarding recommended maintenance activities.

**Table 4.8.6 Typical inspection and maintenance activities for enhanced grass swales**

Activity	Schedule
▪ Inspect for vegetation density (at least 80% coverage), damage by foot or vehicular traffic, channelization, accumulation of debris, trash and sediment, and structural damage to pretreatment devices.	After every major storm event (>25 mm), quarterly for the first two years, and twice annually thereafter.
▪ Regular watering may be required during the first two years while vegetation is becoming established; ▪ Mow grass to maintain height between 75 to 150 mm; ▪ Remove trash and debris from pretreatment devices, the swale surface and inlet and outlets.	At least twice annually. More frequently if desired for aesthetic reasons.
▪ Remove accumulated sediment from pretreatment devices, inlets and outlets; ▪ Replace dead vegetation, remove invasive growth, dethatch, remove thatching and aerate (PDEP, 2006); ▪ Repair eroded or sparsely vegetated areas; ▪ Remove accumulated sediment on the swale surface when dry and exceeds 25 mm depth (PDEP, 2006); ▪ If gullies are observed along the swale, regrading and revegetating may be required.	Annually or as needed

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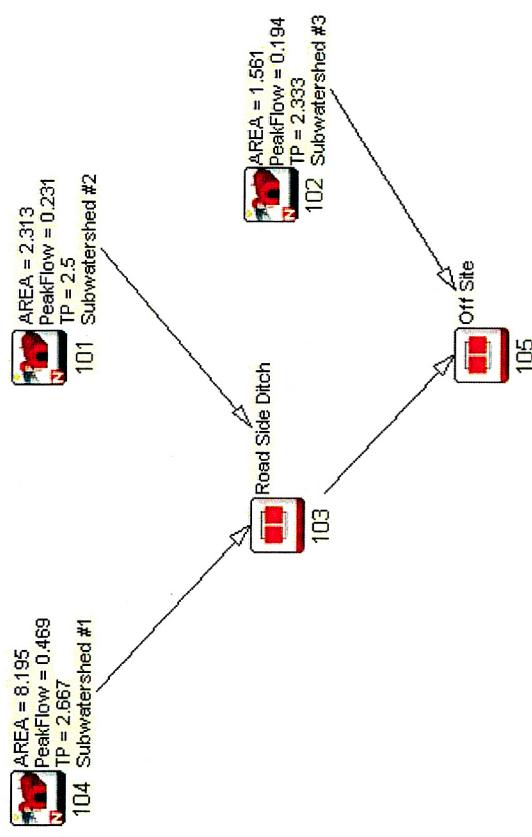
**APPENDIX II**

**VISUAL OTTHYMO OUTPUT**

**PRE DEVELOPMENT**

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**2 Pre-Development**



## Existing-25mm

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=====
V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLL
000 TTTTT H H Y Y M M 000 TM, Version 2.0
0 0 T T H H Y Y M M O O Licensed To: MJ Davenport
000 T T H H Y M M 000 vo2-0057

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

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output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Pre-Development.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Pre-Development.sum

DATE: 1/23/2019 TIME: 1:48:43 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 9 \*\*  
\*\*\*\*\*

CHICAGO STORM	IDF curve parameters: A= 486.300
Ptotal= 25.00 mm	B= 7.500
	C= .790

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs  
Storm time step = 10.00 min  
Time to peak ratio = .38

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.17	1.66	1.17	6.41	2.17	4.73	3.17	2.05
.33	1.87	1.33	14.61	2.33	3.84	3.33	1.89
.50	2.16	1.50	50.69	2.50	3.25	3.50	1.75
.67	2.35	1.67	17.59	2.67	2.82	3.67	1.63
.83	3.16	1.83	9.15	2.83	2.50	3.83	1.53
1.00	4.20	2.00	6.21	3.00	2.25	4.00	1.44

Page 1

## Existing-25mm

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .13	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .016 (i)  
TIME TO PEAK (hrs)= 1.500  
RUNOFF VOLUME (mm)= 3.385  
TOTAL RAINFALL (mm)= 24.995  
RUNOFF COEFFICIENT = .135

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .020 (i)  
TIME TO PEAK (hrs)= 1.667  
RUNOFF VOLUME (mm)= 3.773  
TOTAL RAINFALL (mm)= 24.995  
RUNOFF COEFFICIENT = .151

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .41	

Unit Hyd Qpeak (cms)= .769

PEAK FLOW (cms)= .040 (i)  
TIME TO PEAK (hrs)= 2.000  
RUNOFF VOLUME (mm)= 2.750  
TOTAL RAINFALL (mm)= 24.995  
RUNOFF COEFFICIENT = .110

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3	2.31	.020	1.67	3.77
+ ID1= 1 (0101):	2.31			
+ ID2= 2 (0104):	8.19	.040	2.00	2.75
ID = 3 (0103):	10.51	.057	1.83	2.98

Page 2

## Existing-25mm

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3	1.56	.016	1.50	3.38
+ ID1= 1 (0102):	10.51	.057	1.83	2.98
ID = 3 (0105):	12.07	.068	1.83	3.03

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

**Existing-6hr-Chicago**

```

V   V   I   SSSSS U   U   A   L
V   V   I   SS    U   U   A   A   L
V   V   I   SS    U   U   AAAAAA L
V   V   I   SS    U   U   A   A   L
VV   I   SSSSS UUUUU A   A   LLLL
000   TTTT TTTT H   H   Y   Y   M   M   000   TM, Version 2.0
0   0   T   T   H   H   Y   Y   M   M   0   0   Licensed To: MJ Davenport
000   T   T   H   H   Y   M   M   000   vo2-0057

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual OTTHYMO v2.0\voin.dat  
output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Pre-Development.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Pre-Development.sum

DATE: 1/23/2019 TIME: 1:43:11 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 1 \*\*  
\*\*\*\*\*

CHICAGO STORM	IDF curve parameters: A= 662.000
Ptotal= 37.36 mm	B= 7.500
	C= .790

used in: INTENSITY = A / (t + b)<sup>c</sup>

Duration of storm = 6.00 hrs  
Storm time step = 10.00 min  
Time to peak ratio = .38

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	1.48	1.67	4.30	3.17	5.23	4.67	2.08
.33	1.59	1.83	5.71	3.33	4.42	4.83	1.96
.50	1.71	2.00	8.73	3.50	3.84	5.00	1.86
.67	1.86	2.17	19.94	3.67	3.41	5.17	1.76
.83	2.04	2.33	69.00	3.83	3.07	5.33	1.68
1.00	2.26	2.50	23.94	4.00	2.79	5.50	1.61

Page 1

Existing-6hr-chicago

```

+ ID2= 2 (0104): 8.19   .092   2.83   6.64
ID = 3 (0103): 10.51   .134   2.67   7.12

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0102):	1.56	.041	2.33	7.93	
+ ID2= 2 (0103):	10.51	.134	2.67	7.12	
ID = 3 (0105):	12.07	.155	2.67	7.23	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 2 \*\*  
\*\*\*\*\*

CHICAGO STORM	IDF curve parameters: A=1098.000
Ptotal= 48.64 mm	B= 10.100
	C= .830

used in: INTENSITY = A / (t + b)<sup>c</sup>

Duration of storm = 6.00 hrs  
Storm time step = 10.00 min  
Time to peak ratio = .38

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	1.65	1.67	5.38	3.17	6.69	4.67	2.40
.33	1.78	1.83	7.38	3.33	5.55	4.83	2.25
.50	1.93	2.00	11.78	3.50	4.74	5.00	2.12
.67	2.12	2.17	28.11	3.67	4.15	5.17	2.00
.83	2.35	2.33	90.98	3.83	3.69	5.33	1.90
1.00	2.63	2.50	33.98	4.00	3.33	5.50	1.80
1.17	3.01	2.67	17.30	4.47	3.08	5.67	1.72
1.33	3.51	2.83	11.37	4.33	2.79	5.83	1.64
1.50	4.24	3.00	8.43	4.50	2.58	6.00	1.58

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .13	

Unit Hyd Qpeak (cms)= .462  
PEAK FLOW (cms)= .074 (i)  
TIME TO PEAK (hrs)= 2.333  
RUNOFF VOLUME (mm)= 13.154  
TOTAL RAINFALL (mm)= 48.645  
RUNOFF COEFFICIENT = .270

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.  
Page 3

Existing-6hr-Chicago	1.17	2.55	2.67	12.46	4.17	2.57	5.67	1.54
	1.33	2.94	2.83	8.46	4.33	2.38	5.83	1.48
	1.50	3.48	3.00	6.44	4.50	2.22	6.00	1.42

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .13	

Unit Hyd Qpeak (cms)= .462  
PEAK FLOW (cms)= .041 (i)  
TIME TO PEAK (hrs)= 2.333  
RUNOFF VOLUME (mm)= 7.930  
TOTAL RAINFALL (mm)= 37.363  
RUNOFF COEFFICIENT = .212

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .25	

Unit Hyd Qpeak (cms)= .359  
PEAK FLOW (cms)= .048 (i)  
TIME TO PEAK (hrs)= 2.500  
RUNOFF VOLUME (mm)= 8.840  
TOTAL RAINFALL (mm)= 37.363  
RUNOFF COEFFICIENT = .237

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .41	

Unit Hyd Qpeak (cms)= .769  
PEAK FLOW (cms)= .092 (i)  
TIME TO PEAK (hrs)= 2.833  
RUNOFF VOLUME (mm)= 6.639  
TOTAL RAINFALL (mm)= 37.363  
RUNOFF COEFFICIENT = .178

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0101):	2.31	.048	2.50	8.84	

Page 2

**Existing-6hr-Chicago**

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .25	

Unit Hyd Qpeak (cms)= .359  
PEAK FLOW (cms)= .087 (i)  
TIME TO PEAK (hrs)= 2.500  
RUNOFF VOLUME (mm)= 14.665  
TOTAL RAINFALL (mm)= 48.645  
RUNOFF COEFFICIENT = .301

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .41	

Unit Hyd Qpeak (cms)= .769  
PEAK FLOW (cms)= .168 (i)  
TIME TO PEAK (hrs)= 2.833  
RUNOFF VOLUME (mm)= 11.268  
TOTAL RAINFALL (mm)= 48.645  
RUNOFF COEFFICIENT = .232

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0101):	2.31	.087	2.50	14.66	
+ ID2= 2 (0104):	8.19	.168	2.83	11.27	
ID = 3 (0103):	10.51	.245	2.67	12.02	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0102):	1.56	.074	2.33	13.15	
+ ID2= 2 (0103):	10.51	.245	2.67	12.02	
ID = 3 (0105):	12.07	.283	2.67	12.16	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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Page 4



Existing-6hr-chicago

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .2000 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 32.079

TOTAL RAINFALL (mm)= 76.131

RUNOFF COEFFICIENT = .421

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .41	

Unit Hyd Qpeak (cms)= .769

PEAK FLOW (cms)= .406 (i)

TIME TO PEAK (hrs)= 2.833

RUNOFF VOLUME (mm)= 25.737

TOTAL RAINFALL (mm)= 76.131

RUNOFF COEFFICIENT = .338

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		2.31	.200	2.50	32.08
+ ID1= 1 (0101):		2.31	.200	2.50	32.08
+ ID2= 2 (0104):		8.19	.406	2.83	25.74
	ID = 3 (0103):	10.51	.586	2.67	27.13

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		2.31	.168	2.33	28.78
+ ID1= 1 (0102):		1.56	.168	2.33	28.78
+ ID2= 2 (0103):		10.51	.586	2.67	27.13
	ID = 3 (0105):	12.07	.672	2.67	27.35

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Existing-6hr-Chicago

\*\*\*\*\*

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .13	

IDF curve parameters: A=2507.000

B= 14.800

C= .880

used in: INTENSITY = A / (t + B)<sup>C</sup>

Duration of storm = 6.00 hrs

Storm time step = 10.00 min

Time to peak ratio = .38

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.13	2.25	1.67	8.85	3.17	11.36
.33	2.47	1.83	9.00	3.37	11.52
.50	2.70	2.00	21.34	3.50	7.66
.67	3.00	2.17	52.05	3.67	6.56
.83	3.38	2.33	148.61	3.83	5.72
1.00	3.86	2.50	62.77	4.00	5.07
1.17	4.51	2.67	32.11	4.17	4.55
1.33	5.41	2.83	20.54	4.33	4.12
1.50	6.73	3.00	14.75	4.50	3.77

TIME hrs

RAIN mm/hr

TIME hrs

RAIN mm hr

TIME hrs

RAIN mm hr

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .25	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .194 (i)

TIME TO PEAK (hrs)= 2.333

RUNOFF VOLUME (mm)= 32.319

TOTAL RAINFALL (mm)= 81.724

RUNOFF COEFFICIENT = .395

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .231 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 36.030

TOTAL RAINFALL (mm)= 81.724

RUNOFF COEFFICIENT = .441

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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| CALIB |

Page 10

NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hr)= .41	

Unit Hyd Qpeak (cms)= .769

PEAK FLOW (cms)= .469 (i)

TIME TO PEAK (hrs)= 2.667

RUNOFF VOLUME (mm)= 29.144

TOTAL RAINFALL (mm)= 81.724

RUNOFF COEFFICIENT = .356

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		2.31	.231	2.50	36.03
+ ID1= 1 (0101):		2.31	.231	2.50	36.03
+ ID2= 2 (0104):		8.19	.469	2.67	29.11
	ID = 3 (0103):	10.51	.676	2.67	30.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		2.31	.194	2.33	32.32
+ ID1= 1 (0102):		1.56	.194	2.33	32.32
+ ID2= 2 (0103):		10.51	.676	2.67	30.64
	ID = 3 (0105):	12.07	.774	2.67	30.85

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

**Existing-AES**

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V   V   I   SSSSS U   U   A   L
V   V   I   SS   U   U   A   A   L
V   V   I   SS   U   U   AAAAAA L
V   V   I   SS   U   U   A   A   L
V   V   I   SSSSS UUUUUU A   A   LLLL
000   TTTT   TTTT   H   H   Y   Y   M   M   M   000   TM, Version 2.0
0   0   T   T   H   H   Y   Y   M   M   M   0   Licensed To: MJ Davenport
000   T   T   H   H   Y   M   M   000   vo2-0057

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual otthymo v2.0\voin.dat  
output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Pre-Development.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Pre-Development.sum

DATE: 1/23/2019 TIME: 1:36:05 PM

USER:

COMMENTS: \_\_\_\_\_

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*****
** SIMULATION NUMBER: 1 **
*****

MASS STORM | Filename: C:\visual otthymo files\4456\AES 1-hr.mst
Ptotal= 22.50 mm | Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=
Duration of storm = 1.00 hrs
Mass curve time step = 5.00 min

TIME   RAIN | TIME   RAIN | TIME   RAIN | TIME   RAIN
hrs   mm/hr | hrs   mm/hr | hrs   mm/hr | hrs   mm/hr
.08   10.02 | .33   69.93 | .58   11.10 | .83   .81
.17   30.00 | .42   64.29 | .67   4.62 | .92   .30
.25   49.98 | .50   27.03 | .75   1.92 | 1.00   .03

CALIB | NASHYD (0101) | Area (ha)= 2.31 Curve Number (CN)= 75.0
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00

```

Page 1

**Existing-AES**

U.H. Tp(hr)= .13

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TIME		RAIN		TIME		RAIN		TIME		RAIN	
hrs	mm/hr										
.167	20.01	.500	45.66	.833	1.36	.333	59.95	.667	7.86	1.000	.16

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .034 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 2.656  
TOTAL RAINFALL (mm)= 22.500  
RUNOFF COEFFICIENT = .118

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		NASHYD (0101)		Area		(ha)		Curve Number		(CN)= 75.0	
ID=	1	DT=	10.0	min	Ia	(mm)=	5.00	# of Linear Res.(N)=	3.00	U.H. Tp(hr)=	.25

Unit Hyd Qpeak (cms)= .359  
PEAK FLOW (cms)= .033 (i)  
TIME TO PEAK (hrs)= .667  
RUNOFF VOLUME (mm)= 2.961  
TOTAL RAINFALL (mm)= 22.500  
RUNOFF COEFFICIENT = .132

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		NASHYD (0104)		Area		(ha)		Curve Number		(CN)= 67.0	
ID=	1	DT=	10.0	min	Ia	(mm)=	5.00	# of Linear Res.(N)=	3.00	U.H. Tp(hr)=	.41

Unit Hyd Qpeak (cms)= .769  
PEAK FLOW (cms)= .058 (i)  
TIME TO PEAK (hrs)= .833  
RUNOFF VOLUME (mm)= 2.144  
TOTAL RAINFALL (mm)= 22.500  
RUNOFF COEFFICIENT = .095

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)				AREA		QPEAK		TPEAK		R.V.	
1 +	2 =	3		(ha)	(cms)	(hrs)	(mm)				
ID1=	1 (0101):			2.31	.033	.67	2.96	+ ID2=	2 (0104):		
				8.19	.058	.83	2.14				

Page 2

**Existing-AES**

ID = 3 (0103): 10.51 .090 .67 2.32

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)				AREA		QPEAK		TPEAK		R.V.	
1 +	2 =	3		(ha)	(cms)	(hrs)	(mm)				
ID1=	1 (0102):			1.56	.034	.50	2.66	+ ID2=	2 (0103):		
	10.51	.090	.67	2.32							

ID = 3 (0105): 12.07 .107 .67 2.37

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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*****
** SIMULATION NUMBER: 2 **
*****
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MASS STORM		Filename: C:\visual otthymo files\4456\AES 1-hr.mst		Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=	
Ptotal=	30.50 mm				
Duration of storm =	1.00 hrs				
Mass curve time step =	5.00 min				
TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr

.08	13.58	.33	94.79	.58	15.04	.83	1.10
.17	40.66	.42	87.14	.67	6.26	.92	.40
.25	67.75	.50	36.64	.75	2.60	1.00	.04

CALIB		NASHYD (0102)		Area		(ha)		Curve Number		(CN)= 75.0	
ID=	1 DT=10.0 min	Ia	(mm)=	5.00	# of Linear Res.(N)=	3.00	U.H. Tp(hr)=	.13			

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TIME		RAIN		TIME		RAIN		TIME		RAIN	
hrs	mm/hr										

.167	27.12	.500	61.89	.833	1.85	.333	81.27	.667	10.65	1.000	.22
------	-------	------	-------	------	------	------	-------	------	-------	-------	-----

Unit Hyd Qpeak (cms)= .462  
PEAK FLOW (cms)= .065 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 5.230  
TOTAL RAINFALL (mm)= 30.500  
RUNOFF COEFFICIENT = .171

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 3

**Existing-AES**

CALIB		NASHYD (0101)		Area		(ha)		Curve Number		(CN)= 75.0	
ID=	1	DT=	10.0	min	Ia	(mm)=	5.00	# of Linear Res.(N)=	3.00	U.H. Tp(hr)=	.25

Unit Hyd Qpeak (cms)= .359  
PEAK FLOW (cms)= .064 (i)  
TIME TO PEAK (hrs)= .667  
RUNOFF VOLUME (mm)= 5.830  
TOTAL RAINFALL (mm)= 30.500  
RUNOFF COEFFICIENT = .191

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		NASHYD (0104)		Area		(ha)		Curve Number		(CN)= 67.0	
ID=	1	DT=	10.0	min	Ia	(mm)=	5.00	# of Linear Res.(N)=	3.00	U.H. Tp(hr)=	.41

Unit Hyd Qpeak (cms)= .769  
PEAK FLOW (cms)= .116 (i)  
TIME TO PEAK (hrs)= .667  
RUNOFF VOLUME (mm)= 4.310  
TOTAL RAINFALL (mm)= 30.500  
RUNOFF COEFFICIENT = .141

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)				AREA		QPEAK		TPEAK		R.V.	
1 +	2 =	3		(ha)	(cms)	(hrs)	(mm)				
ID1=	1 (0101):			2.31	.064	.67	5.83	+ ID2=	2 (0104):		
	10.51	.180	.67	4.31							

ID = 3 (0103): 10.51 .180 .67 4.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)				AREA		QPEAK		TPEAK		R.V.	
1 +	2 =	3		(ha)	(cms)	(hrs)	(mm)				
ID1=	1 (0102):			1.56	.065	.50	5.23	+ ID2=	2 (0103):		
	10.51	.180	.67	4.64							

ID = 3 (0105): 12.07 .210 .67 4.72

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

*****
** SIMULATION NUMBER: 3 **
*****
```

Page 4

Existing-AES

MASS STORM	Filename: C:\visual otthymo files\4456\AES 1-hr.mst						
Ptotal= 35.80 mm	Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=						
Duration of storm = 1.00 hrs Mass curve time step = 5.00 min							
TIME	RAIN	TIME	RAIN	TIME	RAIN		
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr		
.08	15.94	.33	111.27	.58	17.66	.83	1.29
.17	47.73	.42	102.29	.67	7.35	.92	.47
.25	79.52	.50	43.00	.75	3.05	1.00	.04

CALIB	NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .13			

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----					
TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.167	31.83	.500	72.65	.833	2.17
.333	95.39	.667	12.50	1.000	.26

Unit Hyd Qpeak (cms)= .462  
PEAK FLOW (cms)= .089 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 7.279  
TOTAL RAINFALL (mm)= 35.800  
RUNOFF COEFFICIENT = .203

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .25			

Unit Hyd Qpeak (cms)= .359  
PEAK FLOW (cms)= .089 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 8.115  
TOTAL RAINFALL (mm)= 35.800  
RUNOFF COEFFICIENT = .227

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .41			

Page 5

Existing-AES

Unit Hyd Qpeak (cms)= .769
PEAK FLOW (cms)= .164 (i)
TIME TO PEAK (hrs)= .667
RUNOFF VOLUME (mm)= 6.774
TOTAL RAINFALL (mm)= 35.800
RUNOFF COEFFICIENT = .170

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0101):		2.31	.089	.50	8.12
+ ID2= 2 (0104):		8.19	.164	.67	6.07
ID = 3 (0103):		10.51	.252	.67	6.52

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0102):		1.56	.089	.50	7.28
+ ID2= 2 (0103):		10.51	.252	.67	6.52
ID = 3 (0105):		12.07	.293	.67	6.62

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 4 \*\*  
\*\*\*\*\*

MASS STORM	Filename: C:\visual otthymo files\4456\AES 1-hr.mst				
Ptotal= 42.50 mm	Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=				
Duration of storm = 1.00 hrs Mass curve time step = 5.00 min					
TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	18.92	.33	132.09	.58	20.96
.17	56.66	.42	121.43	.67	8.72
.25	94.40	.50	51.05	.75	3.62
					1.00 .05

CALIB	NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .13			

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.  
Page 6

Existing-AES

TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.167	37.79	.500	86.24	.833	2.58
.333	113.25	.667	14.84	1.000	.31

Unit Hyd Qpeak (cms)= .462  
PEAK FLOW (cms)= .124 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 10.199  
TOTAL RAINFALL (mm)= 42.500  
RUNOFF COEFFICIENT = .240

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .25			

Unit Hyd Qpeak (cms)= .359  
PEAK FLOW (cms)= .125 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 11.370  
TOTAL RAINFALL (mm)= 42.500  
RUNOFF COEFFICIENT = .268

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .41			

Unit Hyd Qpeak (cms)= .769  
PEAK FLOW (cms)= .233 (i)  
TIME TO PEAK (hrs)= .667  
RUNOFF VOLUME (mm)= 8.633  
TOTAL RAINFALL (mm)= 42.500  
RUNOFF COEFFICIENT = .203

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0101):		2.31	.125	.50	11.37
+ ID2= 2 (0104):		8.19	.233	.67	8.63
ID = 3 (0103):		10.51	.356	.67	9.24

Page 7

Existing-AES  
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0102):		1.56	.124	.50	10.20
+ ID2= 2 (0103):		10.51	.356	.67	9.24
ID = 3 (0105):		12.07	.412	.67	9.36

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 5 \*\*  
\*\*\*\*\*

MASS STORM	Filename: C:\visual otthymo files\4456\AES 1-hr.mst				
Ptotal= 47.40 mm	Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=				
Duration of storm = 1.00 hrs Mass curve time step = 5.00 min					
TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	21.11	.33	147.32	.58	23.38
.17	63.19	.42	135.43	.67	9.73
.25	105.28	.50	36.94	.75	4.04
					1.00 .06

CALIB	NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .13			

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.167	42.15	.500	96.18	.833	2.87
.333	126.30	.667	16.55	1.000	.34

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .151 (i)
TIME TO PEAK (hrs)= .500
RUNOFF VOLUME (mm)= 12.536
TOTAL RAINFALL (mm)= 47.400
RUNOFF COEFFICIENT = .264

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
Page 8			

| ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hr)= .25

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .155 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 13.976  
TOTAL RAINFALL (mm)= 47.400  
RUNOFF COEFFICIENT = .295

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB NASHYD (0104) | Area (ha)= 8.19 Curve Number (CN)= 67.0  
-----  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hr)= .41

Unit Hyd Qpeak (cms)= .769

PEAK FLOW (cms)= .290 (i)  
TIME TO PEAK (hrs)= .667  
RUNOFF VOLUME (mm)= 10.713  
TOTAL RAINFALL (mm)= 47.400  
RUNOFF COEFFICIENT = .226

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD (0103) |  
1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
-----  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0101): 2.31 .155 .50 13.98  
+ ID2= 2 (0104): 8.19 .290 .67 10.71  
-----  
ID = 3 (0103): 10.51 .440 .67 11.43

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| ADD HYD (0105) |  
1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
-----  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0102): 1.56 .151 .50 12.54  
+ ID2= 2 (0103): 10.51 .440 .67 11.43  
-----  
ID = 3 (0105): 12.07 .507 .67 11.57

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 6 \*\*  
\*\*\*\*\*

| MASS STORM | Filename: C:\visual otthymo files\4456\AES 1-hr.mst  
Page 9

| Ptotal= 52.40 mm | Existing-AES  
Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=

Duration of storm = 1.00 hrs  
Mass curve time step = 5.00 min

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.08	23.33	.33	162.86	.58	25.84
.17	69.86	.42	149.72	.67	10.75
.25	116.39	.50	62.94	.75	4.46

| CALIB NASHYD (0102) | Area (ha)= 1.56 Curve Number (CN)= 75.0  
-----  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hr)= .13

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.167	46.59	.500	106.33	.833	3.18
.333	139.63	.667	18.30	1.000	.38

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .180 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 15.074  
TOTAL RAINFALL (mm)= 52.400  
RUNOFF COEFFICIENT = .288

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB NASHYD (0101) | Area (ha)= 2.31 Curve Number (CN)= 75.0  
-----  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hr)= .25

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .186 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 16.805  
TOTAL RAINFALL (mm)= 52.400  
RUNOFF COEFFICIENT = .321

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB NASHYD (0104) | Area (ha)= 8.19 Curve Number (CN)= 67.0  
-----  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hr)= .41

Unit Hyd Qpeak (cms)= .769

Page 10

### Existing-AES

PEAK FLOW (cms)= .353 (i)  
TIME TO PEAK (hrs)= .667  
RUNOFF VOLUME (mm)= 13.001  
TOTAL RAINFALL (mm)= 52.400  
RUNOFF COEFFICIENT = .248

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD (0103) |  
1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
-----  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0101): 2.31 .186 .50 16.80  
+ ID2= 2 (0104): 8.19 .353 .67 13.00  
-----  
ID = 3 (0103): 10.51 .531 .67 13.84

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| ADD HYD (0105) |  
1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
-----  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0102): 1.56 .180 .50 15.07  
+ ID2= 2 (0103): 10.51 .531 .67 13.84  
-----  
ID = 3 (0105): 12.07 .611 .67 14.00

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

## Existing-SCS

```

V   V   I   SSSSS U   U   A   L
V   V   I   SS   U   U   A   A   L
V   V   I   SS   U   U   AAAAAA L
V   V   I   SS   U   U   A   A   L
V   V   I   SSSSS UUUUUU A   A   LLLL

000   TTTTT TTTTT H   H   Y   Y   M   M   M   000   TM, Version 2.0
0   0   T   T   H   H   Y   Y   M   M   O   O   Licensed To: MJ Davenport
000   T   T   H   H   Y   M   M   000   vo2-0057

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual otthymo v2.0\voin.dat  
output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Pre-Development.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Pre-Development.sum

DATE: 1/23/2019 TIME: 1:32:44 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 1 \*\*  
\*\*\*\*\*

MASS STORM	Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst
Ptotal= 38.40 mm	Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Duration of storm = 6.00 hrs  
Mass curve time step = 10.00 min

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	1.61	1.67	3.92	3.17	8.52	4.67	2.30
.33	1.38	1.83	3.69	3.33	8.29	4.83	2.30
.50	1.61	2.00	3.92	3.50	8.52	5.00	2.30
.67	2.30	2.17	4.61	3.67	3.92	5.17	1.61
.83	2.30	2.33	4.61	3.83	3.69	5.33	1.38
1.00	2.30	2.50	4.61	4.00	3.92	5.50	1.61
1.17	2.30	2.67	23.04	4.17	3.00	5.67	1.61
1.33	2.30	2.83	41.47	4.33	3.23	5.83	1.38
1.50	2.30	3.00	59.90	4.50	3.00	6.00	1.61

Page 1

## Existing-SCS

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hr)= .13		

Unit Hyd Qpeak (cms)= .462  
PEAK FLOW (cms)= .103 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 14.093  
TOTAL RAINFALL (mm)= 50.500  
RUNOFF COEFFICIENT = .279

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hr)= .25		

Unit Hyd Qpeak (cms)= .359  
PEAK FLOW (cms)= .059 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 8.372  
TOTAL RAINFALL (mm)= 38.400  
RUNOFF COEFFICIENT = .243

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hr)= .41		

Unit Hyd Qpeak (cms)= .769  
PEAK FLOW (cms)= .113 (i)  
TIME TO PEAK (hrs)= 3.333  
RUNOFF VOLUME (mm)= 7.025  
TOTAL RAINFALL (mm)= 38.400  
RUNOFF COEFFICIENT = .183

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0102):	2.31	.059	3.00	9.33
+ ID2= 2 (0104):	8.19	.113	3.33	7.03
ID = 3 (0103):	10.51	.167	3.17	7.53

Page 2

## Existing-SCS

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0102):	1.56	.061	3.00	8.37
+ ID2= 2 (0103):	10.51	.167	3.17	7.53
ID = 3 (0105):	12.07	.194	3.00	7.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 2 \*\*  
\*\*\*\*\*

MASS STORM	Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst
Ptotal= 50.50 mm	Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Duration of storm = 6.00 hrs  
Mass curve time step = 10.00 min

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	2.12	1.67	5.15	3.17	11.21	4.67	3.03
.33	1.82	1.83	4.85	3.33	10.91	4.83	3.03
.50	2.00	1.60	5.15	3.60	11.21	5.00	3.03
.67	3.03	2.17	6.06	3.67	5.15	5.17	2.12
.83	3.03	2.33	6.06	3.83	4.85	5.33	1.82
1.00	3.03	2.50	6.06	4.00	5.15	5.50	2.12
1.17	3.03	2.67	30.30	4.17	3.94	5.67	2.12
1.33	3.03	2.83	54.54	4.33	4.24	5.83	1.82
1.50	3.03	3.00	78.78	4.50	3.94	6.00	2.12

## Existing-SCS

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .103 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 15.711  
TOTAL RAINFALL (mm)= 50.500  
RUNOFF COEFFICIENT = .311

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hr)= .41		

Unit Hyd Qpeak (cms)= .769  
PEAK FLOW (cms)= .113 (i)  
TIME TO PEAK (hrs)= 3.333  
RUNOFF VOLUME (mm)= 12.113  
TOTAL RAINFALL (mm)= 50.500  
RUNOFF COEFFICIENT = .240

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0101):	2.31	.103	3.00	15.71
+ ID2= 2 (0104):	8.19	.197	3.33	12.11
ID = 3 (0103):	10.51	.293	3.17	12.91

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hr)= .13		

Unit Hyd Qpeak (cms)= .462  
PEAK FLOW (cms)= .103 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 14.093  
TOTAL RAINFALL (mm)= 50.500  
RUNOFF COEFFICIENT = .279

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hr)= .25		

Page 3

CALIB NASHYD (0105)	Area (ha)= 1.56	Curve Number (CN)= 75.0		
ID1= 1 (0102):	.103	3.00	14.09	
+ ID2= 2 (0103):	10.51	.293	3.17	12.91
ID = 3 (0105):	12.07	.341	3.00	13.06

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 3 \*\*  
\*\*\*\*\*

MASS STORM	Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst
Ptotal= 58.60 mm	Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

duration of storm = 6.00 hrs

Page 4

Existing-SCS  
Mass curve time step = 10.00 min

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.73	2.46	1.67	5.98	3.17	13.01	4.67	3.52
.50	2.46	2.00	5.98	3.33	13.06	5.83	3.52
.67	3.52	2.17	7.03	3.67	5.63	5.17	2.46
.83	3.52	2.33	7.03	3.83	5.63	5.33	2.11
1.00	3.52	2.50	7.03	4.00	5.98	5.50	2.46
1.17	3.52	2.67	35.16	4.17	4.57	5.67	2.46
1.33	3.52	2.83	63.29	4.33	4.92	5.83	2.11
1.50	3.52	3.00	91.42	4.50	4.57	6.00	2.46

Note: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Existing-SCS  
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 +	2 = 3	ID1= 1 (0101):	2.31	.135	3.00
+ ID2= 2 (0104):		Ia	.176	3.00	20.53
ID = 3 (0103):		TP(hrs)=	.263	3.33	16.05
				ID = 3 (0103):	10.51 .390 3.17 17.03

Note: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .13	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .135 (i)

TIME TO PEAK (hrs)= 3.000

RUNOFF VOLUME (mm)= 18.411

TOTAL RAINFALL (mm)= 58.600

RUNOFF COEFFICIENT = .314

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .136 (i)

TIME TO PEAK (hrs)= 3.000

RUNOFF VOLUME (mm)= 20.525

TOTAL RAINFALL (mm)= 58.600

RUNOFF COEFFICIENT = .350

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .41	

Unit Hyd Qpeak (cms)= .769

PEAK FLOW (cms)= .263 (i)

TIME TO PEAK (hrs)= 3.333

RUNOFF VOLUME (mm)= 16.048

TOTAL RAINFALL (mm)= 58.600

RUNOFF COEFFICIENT = .274

Page 5

Existing-SCS							
RUNOFF VOLUME (mm)= 24.233							
TOTAL RAINFALL (mm)= 68.700							
RUNOFF COEFFICIENT = .353							

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .181 (i)

TIME TO PEAK (hrs)= 3.000

RUNOFF VOLUME (mm)= 27.016

TOTAL RAINFALL (mm)= 68.700

RUNOFF COEFFICIENT = .393

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .41	

Unit Hyd Qpeak (cms)= .769

PEAK FLOW (cms)= .354 (i)

TIME TO PEAK (hrs)= 3.333

RUNOFF VOLUME (mm)= 21.453

TOTAL RAINFALL (mm)= 68.700

RUNOFF COEFFICIENT = .312

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0101):	2.31	.181	3.00	27.02	
+ ID2= 2 (0104):	8.19	.354	3.33	21.45	
ID = 3 (0103):	10.51	.523	3.17	22.68	

Note: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0102):	1.56	.177	3.00	24.23	
+ ID2= 2 (0103):	10.51	.523	3.17	22.68	
ID = 3 (0105):	12.07	.610	3.00	22.88	

Page 7

Existing-SCS  
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0105)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 +	2 = 3	ID1= 1 (0101):	2.31	.136	3.00
+ ID2= 2 (0104):		Ia	.19	.263	3.33
ID = 3 (0105):		TP(hrs)=	.390	3.17	17.03
				ID = 3 (0105):	10.51 .390 3.17 17.03

Note: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .13	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .135 (i)

TIME TO PEAK (hrs)= 3.000

RUNOFF VOLUME (mm)= 18.411

TOTAL RAINFALL (mm)= 58.600

RUNOFF COEFFICIENT = .314

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .136 (i)

TIME TO PEAK (hrs)= 3.000

RUNOFF VOLUME (mm)= 20.525

TOTAL RAINFALL (mm)= 58.600

RUNOFF COEFFICIENT = .350

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .41	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .177 (i)

TIME TO PEAK (hrs)= 3.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\* SIMULATION NUMBER: 4 \*\*

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .13	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .177 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .217 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .41	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .211 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .13	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .217 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .217 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .41	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .211 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .13	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .217 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .217 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .41	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .211 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .13	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .217 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .217 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .41	

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .211 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .13	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .217 (i)

TIME TO PEAK (hrs)= 3.000

CALIB NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .25	

Unit Hyd Qpeak (cms)= .359

PEAK FLOW (cms)= .217 (i)

Existing-SCS

CALIB	NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	U.H. Tp(hr)= .41

Unit Hyd Qpeak (cms)= .769  
 PEAK FLOW (cms)= .428 (i)  
 TIME TO PEAK (hrs)= 3.333  
 RUNOFF VOLUME (mm)= 25.838  
 TOTAL RAINFALL (mm)= 76.300  
 RUNOFF COEFFICIENT = .339  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)  
 1 + 2 = 3  

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
2.31	.217	3.00	32.20
8.19	.428	3.33	25.84
10.51	.632	3.17	27.24

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)  
 1 + 2 = 3  

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1.56	.211	3.00	28.88
10.51	.632	3.17	27.24
12.07	.736	3.00	27.45

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
 \*\* SIMULATION NUMBER: 6 \*\*  
 \*\*\*\*\*

MASS STORM  
 Ptotal= 83.80 mm |  
 Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst  
 Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Duration of storm = 6.00 hrs  
 MASS curve time step = 10.00 min  

TIME hrs	RAIN mm/hr						
.17	3.52	1.67	8.55	3.17	18.60	4.67	5.03
.33	3.02	1.83	8.04	3.33	18.10	4.83	5.03
.50	3.52	2.00	8.55	3.50	18.60	5.00	5.03
.67	5.03	2.17	10.06	3.67	8.55	5.17	3.52
.83	5.03	2.33	10.06	3.83	8.04	5.33	3.02
1.00	5.03	2.50	10.06	4.00	8.55	5.50	3.52
1.17	5.03	2.67	10.28	4.17	6.54	5.67	3.52
1.33	5.03	2.83	90.30	4.33	7.04	5.83	3.02

Page 9

Existing-SCS

1.50	5.03	3.00	130.73	4.50	6.54	6.00	3.52
------	------	------	--------	------	------	------	------

CALIB	NASHYD (0102)	Area (ha)= 1.56	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	U.H. Tp(hr)= .13

Unit Hyd Qpeak (cms)= .462  
 PEAK FLOW (cms)= .246 (i)  
 TIME TO PEAK (hrs)= 3.000  
 RUNOFF VOLUME (mm)= 33.658  
 TOTAL RAINFALL (mm)= 83.800  
 RUNOFF COEFFICIENT = .402

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0101)	Area (ha)= 2.31	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	U.H. Tp(hr)= .25

Unit Hyd Qpeak (cms)= .359  
 PEAK FLOW (cms)= .254 (i)  
 TIME TO PEAK (hrs)= 3.000  
 RUNOFF VOLUME (mm)= 37.523  
 TOTAL RAINFALL (mm)= 83.800  
 RUNOFF COEFFICIENT = .448

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0104)	Area (ha)= 8.19	Curve Number (CN)= 67.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	U.H. Tp(hr)= .41

Unit Hyd Qpeak (cms)= .769  
 PEAK FLOW (cms)= .505 (i)  
 TIME TO PEAK (hrs)= 3.333  
 RUNOFF VOLUME (mm)= 30.398  
 TOTAL RAINFALL (mm)= 83.800  
 RUNOFF COEFFICIENT = .363

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0101):		2.31	.254	3.00	37.52
+ ID2= 2 (0104):		8.19	.505	3.33	30.40
ID = 3 (0103):		10.51	.744	3.17	31.97

Page 10

Existing-SCS

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0105)  
 1 + 2 = 3  

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1.56	.246	3.00	33.66
10.51	.744	3.17	31.97
12.07	.867	3.00	32.19

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

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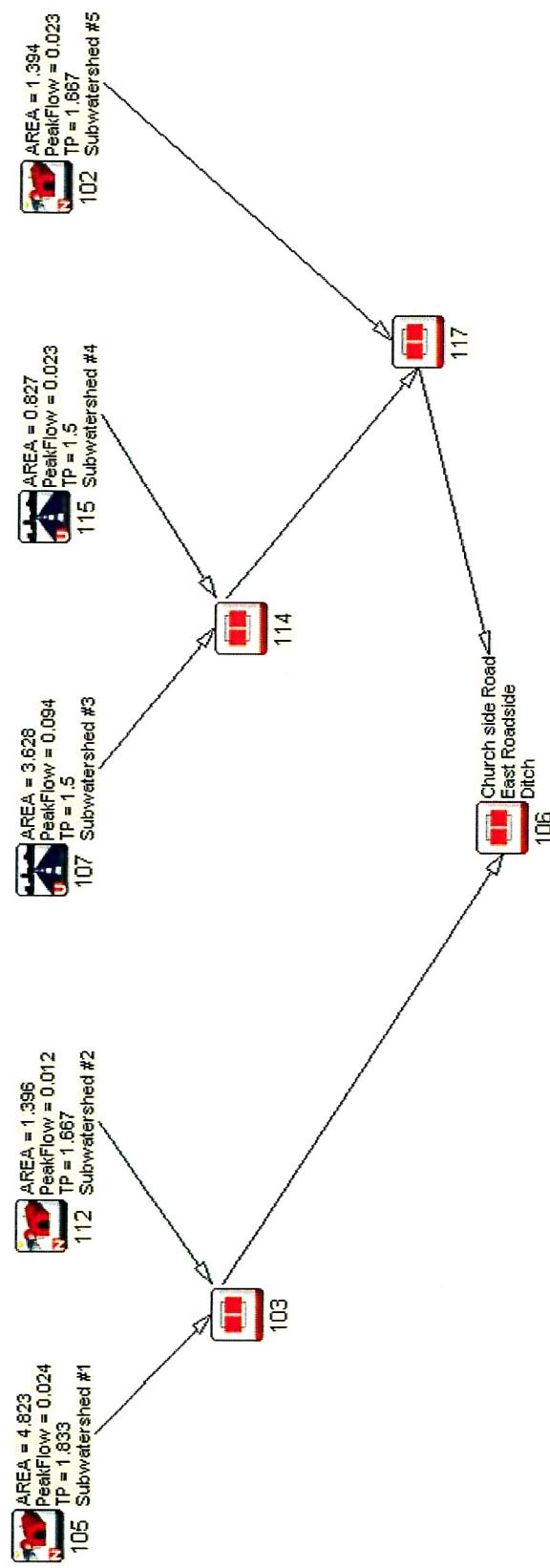
**APPENDIX III**

**VISUAL OTTHYMO OUTPUT**

**POST DEVELOPMENT UN-CONTROLLED**

---

2 Post-Dev Uncontrolled



## Pre-Dev-Uncon-25mm

```

V   V   I   SSSSS U   U   A   L
V   V   I   SS   U   U   A   A   L
V   V   I   SS   U   U   AAAAAA L
V   V   I   SS   U   U   A   A   L
V   V   I   SSSSS UUUUU A   A   LLLL L

000   TTTTT TTTTT H   H   Y   Y   M   M   000   TM, Version 2.0
0   0   T   T   H   H   Y   M   M   0   0   Licensed To: MJ Davenport
000   T   T   H   H   Y   M   M   000   vo2-0057

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual otthymo v2.0\voin.dat  
output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Uncontrolled.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Uncontrolled.sum

DATE: 1/23/2019 TIME: 1:55:59 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 9 \*\*  
\*\*\*\*\*

CHICAGO STORM	IDF curve parameters: A= 486.300				
Ptotal= 25.00 mm	B= 7.500				
	C= .790				
used in: INTENSITY = A / (t + B)^C					
Duration of storm = 4.00 hrs					
Storm time step = 10.00 min					
Time to peak ratio = .38					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.17	1.66	1.17	6.41	2.17	4.73
.33	1.87	1.33	14.61	2.33	3.84
.50	2.16	1.50	50.69	2.50	3.25
.67	2.35	1.67	17.59	2.67	2.82
.83	2.56	1.83	9.15	2.83	2.50
1.00	4.20	2.00	6.21	3.00	2.25

Page 1

## Pre-Dev-Uncon-25mm

CALIB NASHYD (0105)	Area (ha)= 4.82	Curve Number (CN)= 66.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .35	

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .024 (i)

TIME TO PEAK (hrs)= 1.833

RUNOFF VOLUME (mm)= 2.642

TOTAL RAINFALL (mm)= 24.995

RUNOFF COEFFICIENT = .106

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0112)	Area (ha)= 1.40	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .24	

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .012 (i)

TIME TO PEAK (hrs)= 1.667

RUNOFF VOLUME (mm)= 3.769

TOTAL RAINFALL (mm)= 24.995

RUNOFF COEFFICIENT = .151

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3	4.82	.024	1.83	2.64
+ ID2= 2 (0112):	1.40	.012	1.67	3.77
=====				
ID = 3 (0103):	6.22	.036	1.83	2.90

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .24	

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .023 (i)

TIME TO PEAK (hrs)= 1.667

RUNOFF VOLUME (mm)= 6.267

TOTAL RAINFALL (mm)= 24.995

RUNOFF COEFFICIENT = .251

Page 2

## Pre-Dev-Uncon-25mm

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115)	Area (ha)= .83	
ID= 1 DT= 5.0 min	Total Imp(%)= 33.00	Dir. Conn. (%)= 19.00
IMPERVIOUS PERVIOUS (i)		
Surface Area (ha)= .27	.55	
Dep. Storage (mm)= 1.00	2.00	
Average Slope (%)= 2.00	3.00	
Length (m)= 74.30	275.00	
Mannings n = .013	.250	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm hr
.083	1.66	1.083	6.41	2.083	4.73
.167	1.66	1.167	6.41	2.167	4.73
.250	1.87	1.250	14.61	2.250	3.84
.333	1.87	1.333	14.61	2.333	3.84
.417	2.16	1.417	50.69	2.417	3.25
.500	2.16	1.500	50.69	2.500	3.25
.583	2.55	1.583	17.59	2.583	2.82
.667	2.55	1.667	17.59	2.667	2.82
.750	3.16	1.750	9.15	2.750	3.75
.833	3.16	1.833	9.15	2.833	2.30
.917	4.20	1.917	6.21	2.917	2.25
1.000	4.20	2.000	6.21	3.000	2.25

Max.Eff.Inten.(mm/hr)= 50.69	10.32
over (min)= 5.00	55.00
Storage Coeff. (min)= 2.28 (ii)	51.57 (ii)
Unit Hyd. Tpeak (min)= 5.00	55.00
Unit Hyd. peak (cms)= .30	.02
*TOTALS*	
PEAK FLOW (cms)= .02	.01
TIME TO PEAK (hrs)= 1.50	2.42
RUNOFF VOLUME (mm)= 24.00	10.48
TOTAL RAINFALL (mm)= 25.00	25.00
RUNOFF COEFFICIENT = .96	.42

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN= 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0107)	Area (ha)= 3.63	
ID= 1 DT= 5.0 min	Total Imp(%)= 29.40	Dir. Conn. (%)= 19.00

Page 3

## Pre-Dev-Uncon-25mm (i)

Surface Area (ha)= 1.07	2.56
Dep. Storage (mm)= 1.00	3.00
Average Slope (%)= 2.00	3.00
Length (m)= 155.50	440.00
Mannings n = .013	.250

Max.Eff.Inten.(mm/hr)= 50.69	7.08
over (min)= 5.00	80.00

Storage Coeff. (min)= 3.55 (ii)

Unit Hyd. Tpeak (min)= 5.00

Unit Hyd. peak (cms)= .26

\*TOTALS\*

PEAK FLOW (cms)= .09

TIME TO PEAK (hrs)= 1.50

RUNOFF VOLUME (mm)= 24.00

TOTAL RAINFALL (mm)= 25.00

RUNOFF COEFFICIENT = .96

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN= 86.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114)	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3	.83	.023	1.50	13.01
+ ID2= 2 (0107):	3.63	.094	1.50	11.49
=====				
ID = 3 (0114):	4.45	.117	1.50	11.77

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3	1.39	.023	1.67	6.27
+ ID2= 2 (0114):	4.45	.117	1.50	11.77
=====				
ID = 3 (0117):	5.85	.132	1.50	10.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3	6.22	.036	1.83	2.90
+ ID2= 2 (0117):	5.85	.132	1.50	10.46
=====				

Page 4

Pre-Dev-Uncon-25mm  
=====  
ID = 3 (0106): 12.07 .148 1.50 6.56  
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
FINISH  
=====

Pre-Dev-Uncon-6hr-Chicago

```

V   V   I   SSSSS U   U   A   L
V   V   I   SS  U   U   A   A   L
V   V   I   SS  U   U   AAAAAA L
V   V   I   SS  U   U   A   A   L
VV   I   SSSSS UUUUU A   A   LLLL
000   TTTT  TTTT H   H   Y   Y   M   M   000   TM, Version 2.0
0   0   T   T   H   H   Y   Y   M   M   0   0   Licensed To: MJ Davenport
000   T   T   H   H   Y   M   M   000   vo2-0057

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual otthymo v2.0\voin.dat  
output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Uncontrolled.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Uncontrolled.sum

DATE: 1/23/2019 TIME: 1:54:35 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 1 \*\*  
\*\*\*\*\*

CHICAGO STORM	IDF curve parameters: A= 662.000
Ptotal= 37.36 mm	B= 7.500
	C= .790

used in: INTENSITY = A / (t + B)^C

Duration of storm = 6.00 hrs  
Storm time step = 10.00 min  
Time to peak ratio = .38

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	1.48	1.67	4.30	3.17	5.23	4.67	2.08
.33	1.59	1.83	5.71	3.33	4.42	4.83	1.96
.50	1.71	2.00	8.73	3.50	3.84	5.00	1.86
.67	1.86	2.17	19.94	3.67	3.41	5.17	1.76
.83	2.04	2.33	69.00	3.83	3.07	5.33	1.68
1.00	2.26	2.50	23.94	4.00	2.79	5.50	1.61

Page 1

Pre-Dev-Uncon-6hr-Chicago  
RUNOFF VOLUME (mm)= 13.432  
TOTAL RAINFALL (mm)= 37.363  
RUNOFF COEFFICIENT = .359

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	STANDHYD (0115)	Area (ha)= .83	Total Imp(%)= 33.00	Dir. Conn.(%)= 19.00
		IMPERVIOUS PERVIOUS (i)		
Surface Area (ha)=	.27	.55		
Dep. Storage (mm)=	1.00	2.00		
Average Slope (%)=	2.00	3.00		
Length (m)=	74.30	275.00		
Mannings n =	.013	.250		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

===== TRANSFORMED HYETOGRAPH =====							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	1.48	1.583	4.30	3.083	5.23	4.58	2.08
.167	1.48	1.667	4.30	3.167	5.23	4.67	2.08
.250	1.59	1.750	5.71	3.250	4.42	4.75	1.96
.333	1.59	1.833	5.71	3.333	4.42	4.83	1.96
.417	1.71	1.917	8.73	3.417	3.84	4.92	1.86
.500	1.00	2.000	8.73	3.500	3.84	5.00	1.86
.583	1.86	1.983	19.90	3.583	3.11	5.08	1.86
.667	1.86	2.167	19.90	3.667	3.41	5.17	1.76
.750	2.04	2.250	69.00	3.750	3.07	5.25	1.68
.833	2.04	2.333	69.00	3.833	3.07	5.33	1.68
.917	2.26	2.417	23.94	3.917	2.79	5.42	1.61
1.000	2.26	2.500	23.94	4.000	2.79	5.50	1.61
1.083	2.55	2.583	12.46	4.083	2.57	5.58	1.54
1.167	2.55	2.667	12.46	4.167	2.57	5.67	1.54
1.250	2.94	2.750	8.46	4.250	2.38	5.75	1.48
1.333	2.94	2.833	8.46	4.333	2.38	5.83	1.48
1.417	3.48	2.917	6.44	4.417	2.22	5.92	1.42
1.500	3.48	3.000	6.44	4.500	2.22	6.00	1.42

Max.Eff.Inten.(mm/hr)= 69.00 20.78  
over (min)= 5.00 40.00  
Storage Coeff. (min)= 2.01 (ii) 39.27 (ii)  
Unit Hyd. Tpeak (min)= 5.00 40.00  
Unit Hyd. peak (cms)= .31 .03

\*TOTALS\*

PEAK FLOW (cms)= .03 .02 .034 (iii)  
TIME TO PEAK (hrs)= 2.33 2.92 2.33  
RUNOFF VOLUME (mm)= 36.36 19.81 22.93  
TOTAL RAINFALL (mm)= 37.36 37.36 37.36  
RUNOFF COEFFICIENT = .97 .53

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN\* = 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
Page 3

Pre-Dev-Uncon-6hr-Chicago

1.17	2.55	2.67	12.46	4.17	2.57	5.67	1.54
1.33	2.94	2.83	8.46	4.33	2.38	5.83	1.48
1.50	3.48	3.00	6.44	4.50	2.22	6.00	1.42

CALIB	NASHYD (0105)	Area (ha)= 4.82	Curve Number (CN)= 66.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .35		

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .057 (i)  
TIME TO PEAK (hrs)= 2.667  
RUNOFF VOLUME (mm)= 6.397  
TOTAL RAINFALL (mm)= 37.363  
RUNOFF COEFFICIENT = .171

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0112)	Area (ha)= 1.40	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .24		

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .029 (i)  
TIME TO PEAK (hrs)= 2.500  
RUNOFF VOLUME (mm)= 8.830  
TOTAL RAINFALL (mm)= 37.363  
RUNOFF COEFFICIENT = .236

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0105):		4.82	.057	2.67	6.40
+ ID2= 2 (0112):		1.40	.029	2.50	8.83
ID = 3 (0103):		6.22	.084	2.67	6.94

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	NASHYD (0102)	Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .24		

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .048 (i)  
TIME TO PEAK (hrs)= 2.500

Page 2

Pre-Dev-Uncon-6hr-Chicago

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	STANDHYD (0107)	Area (ha)= 3.63	Total Imp(%)= 29.40	Dir. Conn.(%)= 19.00
		IMPERVIOUS	PERVIOUS (i)	

Surface Area (ha)=	1.07	2.56
Dep. Storage (mm)=	1.00	3.00
Average Slope (%)=	2.00	3.00
Length (m)=	155.50	440.00
Mannings n =	.013	.250

Max.Eff.Inten.(mm/hr)=	69.00	13.00
over (min)=	5.00	65.00
Storage Coeff. (min)=	3.14 (ii)	62.72 (ii)
Unit Hyd. Tpeak (min)=	5.00	65.00
Unit Hyd. peak (cms)=	.27	.02

\*TOTALS\*

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%

YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:

CN\* = 86.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114)	1 + 2 = 3	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0115):		.83	.034	2.33	22.93
+ ID2= 2 (0107):		3.63	.133	2.33	20.72
ID = 3 (0114):		4.45	.167	2.33	21.13

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)	1 + 2 = 3	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0102):		1.39	.048	2.50	13.43
+ ID2= 2 (0114):		4.45	.167	2.33	21.13
ID = 3 (0117):		5.85	.202	2.33	19.29

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 4

Pre-Dev-Uncon-6hr-Chicago

ADD HYD (0106)			AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1	+ 2	= 3				
ID1= 1 (0103):	6.22	.084	2.67	6.94		
+ ID2= 2 (0117):	5.85	.202	2.33	19.29		
ID = 3 (0106):	12.07	.247	2.33	12.93		

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 2 \*\*  
\*\*\*\*\*

CHICAGO STORM	IDF curve parameters:	A=1098.000
Ptotal= 48.64 mm	B= 10.100	C= .830
used in: INTENSITY = A / (t + B) <sup>AC</sup>		

Duration of storm = 6.00 hrs  
Storm time step = 10.00 min  
Time to peak ratio = .38

TIME hrs	RAIN mm/hr						
.17	1.65	1.67	5.38	3.17	6.69	4.67	2.40
.33	1.78	1.83	7.38	3.33	5.55	4.83	2.25
.50	1.93	2.00	11.78	3.50	4.74	5.00	2.12
.67	2.12	2.17	28.11	3.67	4.15	5.17	2.00
.83	2.35	2.33	90.98	3.83	3.69	5.33	1.90
1.00	2.63	2.50	33.98	4.00	3.33	5.50	1.80
1.17	3.01	2.67	17.30	4.17	3.03	5.67	1.72
1.33	3.51	2.83	11.37	4.33	2.79	5.83	1.64
1.50	4.24	3.00	8.43	4.50	2.58	6.00	1.58

CALIB NASHYD (0105)	Area (ha)=	4.82	Curve Number (CN)=	66.0
ID= 1 DT=10.0 min	Ia (mm)=	5.00	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.35		

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .106 (i)  
TIME TO PEAK (hrs)= 2.667  
RUNOFF VOLUME (mm)= 10.883  
TOTAL RAINFALL (mm)= 48.645  
RUNOFF COEFFICIENT = .224

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0112)	Area (ha)=	1.40	Curve Number (CN)=	75.0
				Page 5

Pre-Dev-Uncon-6hr-Chicago

ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .24

unit Hyd Qpeak (cms)= .222  
PEAK FLOW (cms)= .053 (i)  
TIME TO PEAK (hrs)= 2.500  
RUNOFF VOLUME (mm)= 14.647  
TOTAL RAINFALL (mm)= 48.645  
RUNOFF COEFFICIENT = .301

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1	+ 2	= 3		
ID1= 1 (0103):	4.82	.106	2.67	10.88
+ ID2= 2 (0112):	1.40	.053	2.50	14.65
ID = 3 (0103):	6.22	.153	2.67	11.73

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha)=	1.39	Curve Number (CN)=	84.0
ID= 1 DT=10.0 min	Ia (mm)=	4.00	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.24		

unit Hyd Qpeak (cms)= .223  
PEAK FLOW (cms)= .081 (i)  
TIME TO PEAK (hrs)= 2.500  
RUNOFF VOLUME (mm)= 21.135  
TOTAL RAINFALL (mm)= 48.645  
RUNOFF COEFFICIENT = .434

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115)	Area (ha)=	.83
ID= 1 DT= 5.0 min	Total Imp(%)=	33.00
	Dir. Conn. (%)=	19.00

IMPERVIOUS Surface Area (ha)= .27  
Dep. Storage (mm)= 1.00  
Average Slope (%)= 2.00  
Length (m)= 74.30  
Mannings n = .013

PERVIOUS (.i) 5.55  
2.00  
3.00  
275.00  
.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.083	1.65	1.583	5.38	3.083	6.69

Page 6

Pre-Dev-Uncon-6hr-Chicago							
.167	1.65	1.667	5.38	3.167	6.69	4.67	2.40
.250	1.78	1.750	7.38	3.250	5.55	4.75	2.25
.333	1.78	1.833	7.38	3.333	5.55	4.83	2.25
.417	1.93	1.917	11.78	3.417	4.74	4.92	2.12
.500	1.93	2.000	11.78	3.500	4.74	5.00	2.12
.583	2.12	2.083	28.11	3.583	4.15	5.08	2.00
.667	2.12	2.167	28.11	3.667	4.15	5.17	2.00
.750	2.35	2.250	90.98	3.750	3.69	5.25	1.90
.833	2.35	2.333	90.98	3.833	3.69	5.33	1.80
.917	2.63	2.417	33.98	3.917	3.33	5.42	1.80
1.000	2.63	2.500	33.98	4.000	3.33	5.50	1.80
1.083	3.01	2.583	17.30	4.083	3.03	5.58	1.72
1.167	3.01	2.667	17.30	4.167	3.03	5.67	1.72
1.250	3.51	2.750	11.37	4.250	2.79	5.75	1.64
1.333	3.51	2.833	11.37	4.333	2.79	5.83	1.64
1.417	4.24	2.917	8.43	4.417	2.58	5.92	1.58
1.500	4.24	3.000	8.43	4.500	2.58	6.00	1.58

Max.Eff.Inten.(mm/hr)= 90.98  
Over (min)= 5.00  
Storage Coeff(%)= 1.80 (ii) 30.88 (iii)  
Unit Hyd. Tpeak (min)= 5.00  
Unit Hyd. peak (cms)= .32 .04

\*TOTALS\*

PEAK FLOW (cms)= .04 .04 .048 (iii)  
TIME TO PEAK (hrs)= 2.33 2.83 2.33  
RUNOFF VOLUME (mm)= 47.64 29.19 32.68  
TOTAL RAINFALL (mm)= 48.64 48.64 48.64  
RUNOFF COEFFICIENT = .98 .60 .67

\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN<sup>o</sup> = 86.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0107)	Area (ha)=	3.63
ID= 1 DT= 5.0 min	Total Imp(%)=	29.40
	Dir. Conn. (%)=	19.00

IMPERVIOUS Surface Area (ha)= 1.07  
Dep. Storage (mm)= 1.00  
Average Slope (%)= 2.00  
Length (m)= 155.50  
Mannings n = .013

2.56  
3.00  
3.00  
440.00  
.250

Max.Eff.Inten.(mm/hr)= 90.98  
Over (min)= 5.00  
Storage Coeff(%)= 2.81 (ii) 49.87 (iii)  
Unit Hyd. Tpeak (min)= 5.00  
Unit Hyd. peak (cms)= .28 .02

\*TOTALS\*

PEAK FLOW (cms)= .17 .10 .185 (iii)  
TIME TO PEAK (hrs)= 2.33 3.17 2.33  
RUNOFF VOLUME (mm)= 47.64 25.82 29.96  
TOTAL RAINFALL (mm)= 48.64 48.64 48.64

Page 7

ADD HYD (0114)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1	+ 2	= 3		
ID1= 1 (0115):	.83	.048	2.33	32.68
+ ID2= 2 (0107):	3.63	.185	2.33	29.96
ID = 3 (0114):	4.45	.233	2.33	30.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1	+ 2	= 3		
ID1= 1 (0102):	.83	.081	2.15	21.66
+ ID2= 2 (0114):	4.45	.233	2.33	30.46
ID = 3 (0117):	5.85	.293	2.33	28.24

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1	+ 2	= 3		
ID1= 1 (0103):	6.22	.153	2.67	11.73
+ ID2= 2 (0117):	5.85	.293	2.33	28.24
ID = 3 (0106):	12.07	.378	2.33	19.73

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1	+ 2	= 3		
ID1= 1 (0103):	6.22	.106	2.67	10.88
+ ID2= 2 (0117):	1.40	.053	2.50	14.65
ID = 3 (0106):	7.62	.159	2.67	11.73

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CHICAGO STORM	IDF curve parameters:	A=1560.000
Ptotal= 57.49 mm	B= 13.000	C= .860
used in: INTENSITY = A / (t + B) <sup>AC</sup>		

duration of storm = 6.00 hrs

Page 8

Pre-Dev-Uncon-6hr-Chicago  
Storm time step = 10.0 min  
Time to peak ratio = .38

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.15	1.73	1.47	6.29	3.47	7.97	4.57	2.60
.33	1.88	1.83	8.67	3.33	6.51	4.83	2.42
.50	2.06	2.00	14.61	3.50	5.48	5.00	2.27
.67	2.27	2.17	35.36	3.67	4.74	5.17	2.13
.83	2.54	2.33	105.21	3.83	4.17	5.33	2.01
1.00	2.88	2.50	42.69	4.00	3.72	5.50	1.90
1.17	3.33	2.67	21.79	4.17	3.36	5.67	1.81
1.33	3.95	2.83	14.08	4.33	3.06	5.83	1.72
1.50	4.85	3.00	10.23	4.50	2.81	6.00	1.64

Pre-Dev-Uncon-6hr-Chicago

CALIB	NASHYD (0102)	Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .24		
Unit Hyd Qpeak (cms)=	.223		
PEAK FLOW (cms)=	.109 (i)		
TIME TO PEAK (hrs)=	2.500		
RUNOFF VOLUME (mm)=	27.705		
TOTAL RAINFALL (mm)=	57.490		
RUNOFF COEFFICIENT =	.482		

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0105)	Area (ha)= 4.82	Curve Number (CN)= 66.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .35		

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .151 (i)

TIME TO PEAK (hrs)= 2.667

RUNOFF VOLUME (mm)= 14.982

TOTAL RAINFALL (mm)= 57.490

RUNOFF COEFFICIENT = .261

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0112)	Area (ha)= 1.40	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .24		

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .074 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 19.820

TOTAL RAINFALL (mm)= 57.490

RUNOFF COEFFICIENT = .345

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	ADD HYD (0103)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3					
+ ID1= 1 (0105):	4.82	.151	2.67	14.98	
+ ID2= 2 (0112):	1.40	.074	2.50	19.82	

ID = 3 (0103): 6.22 .218 2.67 16.07

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 9

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TRANSFORMED HYETOGRAPH							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	1.73	1.583	6.29	3.083	7.97	4.58	2.60
.167	1.73	1.667	6.29	3.167	7.97	4.67	2.60
.250	1.88	1.750	8.87	3.250	6.51	4.75	2.42
.333	1.88	1.833	8.87	3.333	6.51	4.83	2.27
.417	1.917	1.917	14.61	3.417	5.48	4.92	2.27
.500	2.06	2.000	14.61	3.500	5.48	5.00	2.27
.583	2.27	2.083	35.36	3.583	4.74	5.08	2.13
.667	2.27	2.167	35.36	3.667	4.74	5.17	2.13
.750	2.54	2.250	105.21	3.750	4.17	5.25	2.01
.833	2.54	2.333	105.21	3.833	4.17	5.33	2.01
.917	2.88	2.417	42.69	3.917	3.72	5.42	1.90
1.000	2.88	2.500	42.69	4.000	3.72	5.50	1.90
1.083	3.33	2.583	21.79	4.083	3.36	5.58	1.81
1.167	3.33	2.667	21.79	4.167	3.36	5.67	1.81
1.250	3.95	2.750	14.08	4.250	3.06	5.75	1.72
1.333	3.95	2.833	14.08	4.333	3.06	5.83	1.72
1.417	4.85	2.917	10.23	4.417	2.81	5.92	1.64
1.500	4.85	3.000	10.23	4.500	2.81	6.00	1.64

Max.Eff.Inten.(mm/hr)= 105.21 49.44  
over (min)= 5.00 30.00  
Storage Coeff. (min)= 1.70 (ii) 28.04 (ii)  
Unit Hyd. Tpeak (min)= 5.00 30.00  
Unit Hyd. peak (cms)= .32 .04

\*TOTALS\*  
PEAK FLOW (cms)= .05 .05 .060 (iii)  
TIME TO PEAK (hrs)= 2.33 2.75 2.33

Page 10

Pre-Dev-Uncon-6hr-Chicago				
RUNOFF VOLUME (mm)= 56.49	36.90	40.60		
TOTAL RAINFALL (mm)= 57.49	57.49	57.49		
RUNOFF COEFFICIENT = .98	.64	.71		

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN<sup>x</sup> = 88.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	STANDHYD (0107)	Area (ha)= 3.63	Dir. conn.(%)= 19.00
ID= 1 DT= 5.0 min	Total Imp(%)= 29.40		

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\* \*\*\*\*\* \*\*\*\*\* \*\*\*\*\*

\*\* SIMULATION NUMBER: 4 \*\*

\*\*\*\*\* \*\*\*\*\* \*\*\*\*\* \*\*\*\*\*

CHICAGO STORM Ptotal= 65.65 mm IDF Curve parameters: A=2010.000

B= 14.000 C=.880

used in: INTENSITY = A / (t + B)<sup>AC</sup>

Duration of storm = 6.00 hrs

Storm time step = 10.00 min

Time to peak ratio = .38

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.15	1.20	1.67	6.28	3.17	8.23	4.67	2.75
.33	1.95	1.95	10.23	1.33	7.23	4.83	2.75
.50	2.14	2.00	16.85	3.50	6.04	5.00	2.37
.67	2.38	2.17	41.62	3.67	5.17	5.17	2.22
.83	2.67	2.33	122.63	3.83	4.52	5.33	2.09
1.00	3.05	2.50	50.34	4.00	4.00	5.50	1.97
1.17	3.56	2.67	25.45	4.17	3.60	5.67	1.87
1.33	4.27	2.83	16.21	4.33	3.26	5.83	1.77
1.50	5.31	3.00	11.63	4.50	2.98	6.00	1.69

CALIB	NASHYD (0105)	Area (ha)= 4.82	Curve Number (CN)= 66.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= .35		

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .201 (i)

Page 12

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 11

Pre-Dev-Uncon-6hr-Chicago  
 TIME TO PEAK (hrs)= 2.667  
 RUNOFF VOLUME (mm)= 19.147  
 TOTAL RAINFALL (mm)= 65.646  
 RUNOFF COEFFICIENT = .292

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Pre-Dev-Uncon-6hr-Chicago  
 Average Slope (%)= 2.00 3.00  
 Length (m)= 74.30 275.00  
 Manning's n = 0.013 0.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

CALIB NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
 ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .098 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 24.972

TOTAL RAINFALL (mm)= 65.646

RUNOFF COEFFICIENT = .380

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TRANSFORMED HYETOGRAPH							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	1.78	1.583	6.98	3.083	8.95	4.58	2.75
.167	1.78	1.667	6.98	3.167	8.95	4.67	2.75
.250	1.95	1.750	10.01	3.250	7.23	4.75	2.55
.333	1.95	1.833	10.01	3.333	7.23	4.83	2.55
.417	2.14	1.917	16.85	3.417	6.04	4.92	2.37
.500	2.14	2.000	16.85	3.500	6.04	5.00	2.37
.583	2.38	2.083	16.85	3.583	5.17	5.09	2.22
.667	2.38	2.167	41.62	3.667	5.17	5.17	2.22
.750	2.67	2.250	122.63	3.750	4.52	5.25	2.09
.833	2.67	2.333	122.63	3.833	4.52	5.33	2.09
.917	3.05	2.417	50.34	3.917	4.00	5.42	1.97
1.000	3.05	2.500	50.34	4.000	4.00	5.50	1.97
1.083	3.56	2.583	25.45	4.083	3.60	5.58	1.87
1.167	3.56	2.667	25.45	4.167	3.60	5.67	1.87
1.250	4.27	2.750	16.21	4.250	3.26	5.75	1.77
1.333	4.27	2.833	16.21	4.333	3.26	5.83	1.77
1.417	5.31	2.917	11.63	4.417	2.98	5.92	1.69
1.500	5.31	3.000	11.63	4.500	2.98	6.00	1.69

Max.Eff.Inten.(mm/hr)= 122.63 67.74  
 over (min)= 5.00 25.00  
 Storage Coeff. (min)= 1.60 (ii) 24.82 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 25.00  
 Unit Hyd. peak (cms)= .32 .05

\*TOTALS\*  
 PEAK FLOW (cms)= .05 .07 .077 (i)  
 TIME TO PEAK (hrs)= 2.33 2.67 2.33  
 RUNOFF VOLUME (mm)= 64.65 44.20 48.07  
 TOTAL RAINFALL (mm)= 65.65 65.65 65.65  
 RUNOFF COEFFICIENT = .98 .67 .73

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 CN\* = 88.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0107) | Area (ha)= 3.63  
 ID= 1 DT= 5.0 min | Total Imp(%)= 29.40 Dir. Conn.(%)= 19.00  
 Surface Area (ha)= 1.07 2.56  
 Dep. Storage (mm)= 1.00 3.00  
 Average Slope (%)= 2.00 3.00  
 Length (m)= 155.50 440.00  
 Manning's n = .013 .250

Page 14

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115) | Area (ha)= .83 Dir. Conn.(%)= 19.00  
 ID= 1 DT= 5.0 min | Total Imp(%)= 33.00  
 IMPERVIOUS PERVIOUS (i)  
 Surface Area (ha)= .27 .55  
 Dep. Storage (mm)= 1.00 2.00

Page 13

#### Pre-Dev-Uncon-6hr-Chicago

Max.Eff.Inten.(mm/hr)= 122.63 44.30  
 over (min)= 5.00 40.00  
 Storage Coeff. (min)= 2.49 (ii) 38.98 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 40.00  
 Unit Hyd. peak (cms)= .29 .03  
 \*TOTALS\*  
 PEAK FLOW (cms)= .23 .19 .270 (iii)  
 TIME TO PEAK (hrs)= 2.93 2.92 2.32  
 RUNOFF VOLUME (mm)= 64.65 40.10 44.06  
 TOTAL RAINFALL (mm)= 65.65 65.65 65.65  
 RUNOFF COEFFICIENT = .98 .61 .68

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 CN\* = 86.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114) | AREA QPEAK TPEAK R.V.  
 1 + 2 = 3 | (ha) (cms) (hrs) (mm)  
 ID1= 1 (0115): .83 .077 2.33 48.07  
 + ID2= 2 (0107): 3.63 .270 2.33 44.76  
 ID = 3 (0114): 4.45 .347 2.33 45.37

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117) | AREA QPEAK TPEAK R.V.  
 1 + 2 = 3 | (ha) (cms) (hrs) (mm)  
 ID1= 1 (0102): 1.39 .140 2.50 34.07  
 + ID2= 2 (0114): 1.45 .347 2.33 45.37  
 ID = 3 (0117): 5.85 .451 2.33 42.68

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106) | AREA QPEAK TPEAK R.V.  
 1 + 2 = 3 | (ha) (cms) (hrs) (mm)  
 ID1= 1 (0103): 6.22 .288 2.67 20.45  
 + ID2= 2 (0117): 5.85 .451 2.33 42.68  
 ID = 3 (0106): 12.07 .666 2.67 31.23

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Pre-Dev-Uncon-6hr-Chicago  
 \*\*\*\*\* SIMULATION NUMBER: 5 \*\*\*\*\*

CHICAGO STORM Ptotal= 76.13 mm IDF curve parameters: A=2200.000  
 B= 14.600 C= .870  
 used in: INTENSITY = A / (t + B)AC  
 duration of storm = 6.00 hrs  
 storm time step = 10.00 min  
 Time to peak ratio = .38

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	2.22	1.67	8.42	3.17	10.74	4.67	3.38
.33	2.41	1.83	11.98	3.33	8.72	4.83	3.14
.50	2.65	2.00	19.90	3.50	7.31	5.00	2.93
.67	2.91	2.17	8.81	3.67	6.98	5.17	2.75
.83	3.29	2.33	135.62	3.83	5.50	5.33	2.59
1.00	3.75	2.50	57.60	4.00	4.89	5.50	2.44
1.17	4.36	2.67	29.73	4.17	4.40	5.67	2.32
1.33	5.21	2.83	19.18	4.33	4.00	5.83	2.20
1.50	6.45	3.00	13.86	4.50	3.67	6.00	2.10

CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
 ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .257 (i)  
 TIME TO PEAK (hrs)= 2.667  
 RUNOFF VOLUME (mm)= 24.972  
 TOTAL RAINFALL (mm)= 76.131  
 RUNOFF COEFFICIENT = .328

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
 ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .123 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 32.041

TOTAL RAINFALL (mm)= 76.131

RUNOFF COEFFICIENT = .421

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 15

Page 16

### Pre-Dev-Uncon-6hr-Chicago

ADD HYD (0103)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1	2 = 3				
+ ID1= 1 (0105):		4.82	.257	2.67	24.97
+ ID2= 2 (0112):		1.40	.123	2.50	32.04
ID = 3 (0103):		6.22	.366	2.67	26.56

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)		Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hrs)= .24			

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .171 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 42.587

TOTAL RAINFALL (mm)= 76.131

RUNOFF COEFFICIENT = .559

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANHYD (0115)		Area (ha)= .83	Dir. Conn. (%)= 19.00
ID= 1 DT= 5.0 min	Total Imp(%)= 33.00		

IMPERVIOUS PERVIOUS (i)

Surface Area (ha)= .27 .55

Dep. Storage (mm)= 1.00 2.00

Average Slope (%)= 2.00 3.00

Length (m)= 74.30 275.00

Mannings n = .013 .250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.083	2.22	1.583	8.42	3.083	10.74	4.58	3.38
.167	2.22	1.667	8.42	3.167	10.74	4.67	3.38
.250	2.41	1.750	11.98	3.250	8.72	4.75	3.44
.333	2.41	1.833	11.98	3.333	8.72	4.83	3.44
.417	2.65	1.917	19.90	3.417	7.31	4.92	2.93
.500	2.65	2.000	19.90	3.500	7.31	5.00	2.93
.583	2.93	2.083	47.86	3.583	6.28	5.08	2.75
.667	2.93	2.167	47.86	3.667	6.28	5.17	2.75
.750	3.29	2.250	135.62	3.750	5.50	5.25	2.59
.833	3.29	2.333	135.62	3.833	5.50	5.33	2.59
.917	3.75	2.417	57.60	3.917	4.89	5.42	2.44
1.000	3.75	2.500	57.60	4.000	4.89	5.50	2.44
1.083	4.36	2.583	29.73	4.083	4.40	5.58	2.32
1.167	4.36	2.667	29.73	4.167	4.40	5.67	2.32
1.250	5.21	2.750	19.18	4.250	4.00	5.75	2.20
1.333	5.21	2.833	19.18	4.333	4.00	5.83	2.20

Page 17

### Pre-Dev-Uncon-6hr-Chicago

1.417	6.45	2.917	13.86	4.417	3.67	5.92	2.10
1.500	6.45	3.000	13.86	4.500	3.67	6.00	2.10

Max.Eff.Inten.(mm/hr)= 135.62 79.92

over (min)= 5.00 25.00

Storage Coeff. (min)= 1.54 (ii) 23.27 (ii)

Unit Hyd. Tpeak (min)= 5.00 25.00

Unit Hyd. peak (cms)= .33 .05

\*TOTALS\*

PEAK FLOW (cms)= .06 .08 .094 (iii)

TIME TO PEAK (hrs)= 2.33 2.67 2.67

RUNOFF VOLUME (mm)= 75.13 53.79 57.82

TOTAL RAINFALL (mm)= 76.13 76.13 76.13

RUNOFF COEFFICIENT = .99 .71 .76

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20% YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:

CN\* = 88.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANHYD (0107)		Area (ha)= 3.63	Dir. Conn. (%)= 19.00
ID= 1 DT= 5.0 min	Total Imp(%)= 29.40		

IMPERVIOUS PERVIOUS (i)

Surface Area (ha)= 1.07 2.56

Dep. Storage (mm)= 1.00 3.00

Average Slope (%)= 2.00 3.00

Length (m)= 155.50 440.00

Mannings n = .013 .250

Max.Eff.Inten.(mm/hr)= 135.62 57.63

over (min)= 5.00 40.00

Storage Coeff. (min)= 2.39 (ii) 35.24 (ii)

Unit Hyd. Tpeak (min)= 5.00 40.00

Unit Hyd. peak (cms)= .30 .03

\*TOTALS\*

PEAK FLOW (cms)= .26 .24 .310 (iii)

TIME TO PEAK (hrs)= 2.33 2.92 2.33

RUNOFF VOLUME (mm)= 75.13 49.33 54.23

TOTAL RAINFALL (mm)= 76.13 76.13 76.13

RUNOFF COEFFICIENT = .99 .65 .71

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20% YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:

CN\* = 86.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 18

### Pre-Dev-Uncon-6hr-Chicago

ADD HYD (0114)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3					
+ ID1= 1 (0115):		.83	.094	2.67	57.82
+ ID2= 2 (0107):		3.63	.310	2.33	54.23

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3					
+ ID1= 1 (0102):		1.39	.171	2.50	42.59
+ ID2= 2 (0114):		4.45	.400	2.33	54.90

ID = 3 (0117): 5.85 .529 2.33 51.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3					
+ ID1= 1 (0103):		6.22	.366	2.67	26.56
+ ID2= 2 (0117):		5.85	.529	2.33	51.96

ID = 3 (0106): 12.07 .837 2.67 38.87

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CHICAGO STORM IDF curve parameters:		A=2507.000	B= 14.800	C= .880
PTotal= 81.72 mm				

used in: INTENSITY = A / (t + B)^C

Duration of storm = 6.00 hrs

Storm time step = 10.00 min

Time to peak ratio = .38

TIME hrs	RAIN mm hr						
.12	2.25	1.67	8.85	3.17	11.36	4.67	3.27
.33	2.43	1.83	12.70	3.33	9.17	4.83	3.32
.50	2.70	2.00	21.34	3.50	7.66	5.00	3.00
.67	3.00	2.17	52.05	3.67	6.56	5.17	2.81
.83	3.38	2.33	148.61	3.83	5.72	5.33	2.64
1.00	3.86	2.50	62.77	4.00	5.07	5.50	2.49
1.17	4.51	2.67	32.11	4.17	4.55	5.67	2.36
1.33	5.41	2.83	20.54	4.33	4.12	5.83	2.24
1.50	6.73	3.00	14.75	4.50	3.77	6.00	2.13

Page 19

ADD HYD (0103)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3					
+ ID1= 1 (0105):		4.82	.298	2.67	28.27
+ ID2= 2 (0112):		1.40	.141	2.50	35.99

ID = 3 (0103): 6.22 .422 2.67 30.00

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)		Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hrs)= .24			

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .194 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 47.255

TOTAL RAINFALL (mm)= 81.724

RUNOFF COEFFICIENT = .578

Page 20

Pre-Dev-Uncon-6hr-Chicago  
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115)		Area (ha)= .83	Dir. Conn.(%)= 19.00
		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.27	.55	
Dep. Storage (mm)=	1.00	2.00	
Average Slope (%)=	2.00	3.00	
Length (m)=	74.30	275.00	
Mannings n =	.013	.250	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083 2.25	1.583 8.85	3.083 11.36	4.58 3.47				
.167 2.25	1.667 8.85	3.167 11.36	4.67 3.47				
.250 2.45	1.750 12.70	3.250 9.17	4.75 3.22				
.333 2.45	1.833 12.70	3.333 9.17	4.83 3.22				
.417 2.70	1.917 21.34	3.417 7.66	4.92 3.00				
.500 2.70	2.000 21.34	3.500 7.66	5.00 3.00				
.583 3.00	2.083 52.05	3.583 6.58	5.08 2.81				
.667 3.00	2.167 52.05	3.667 6.58	5.17 2.74				
.750 3.38	2.250 148.61	3.750 9.72	5.25 2.64				
.833 3.38	2.333 148.61	3.833 9.72	5.33 2.64				
.917 3.86	2.417 62.78	3.917 5.07	5.42 2.49				
1.000 3.86	2.500 62.77	4.000 5.07	5.50 2.49				
1.083 4.51	2.583 32.11	4.083 4.55	5.58 2.36				
1.167 4.51	2.667 32.11	4.167 4.55	5.67 2.36				
1.250 5.41	2.750 20.54	4.250 4.12	5.75 2.24				
1.333 5.41	2.833 20.54	4.333 4.12	5.83 2.24				
1.417 6.73	2.917 14.75	4.417 3.77	5.92 2.13				
1.500 6.73	3.000 14.75	4.500 3.77	6.00 2.13				

Max.Eff.Inten.(mm/hr)= 148.61 101.98  
over (min)= 5.00 25.00  
Storage Coeff. (min)= 1.48 (ii) 21.20 (ii)  
Unit Hyd. Tpeak (min)= 5.00 25.00  
Unit Hyd. peak (cms)= .33 .05

\*TOTALS\*

PEAK FLOW (cms)= .06 .09 .108 (iii)  
TIME TO PEAK (hrs)= 2.33 2.67 2.67  
RUNOFF VOLUME (mm)= 80.72 58.97 63.09  
TOTAL RAINFALL (mm)= 81.72 81.72 81.72  
RUNOFF COEFFICIENT = .99 .72 .77

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN\* = 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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Page 21

Pre-Dev-Uncon-6hr-Chicago

CALIB STANDHYD (0107)		Area (ha)= 3.63	Dir. Conn.(%)= 19.00
		Total Imp(%)= 29.40	
Surface Area (ha)=	1.07	2.56	
Dep. Storage (mm)=	2.00	3.00	
Average Slope (%)=	2.31 (ii)	33.68 (ii)	
Length (m)=	155.50	440.00	
Mannings n =	.013	.250	
Max.Eff.Inten.(mm/hr)=	148.61	64.62	
over (min)=	5.00	35.00	
Storage Coeff. (min)=	2.31 (ii)	33.68 (ii)	
Unit Hyd. Tpeak (min)=	5.00	35.00	
Unit Hyd. peak (cms)=	.30	.03	

\*TOTALS\*

PEAK FLOW (cms)= .28 .29 .354 (iii)

TIME TO PEAK (hrs)= 2.33 2.83 2.33

RUNOFF VOLUME (mm)= 80.72 54.35 59.36

TOTAL RAINFALL (mm)= 81.72 81.72 81.72

RUNOFF COEFFICIENT = .99 .67 .73

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN\* = 86.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114)		AREA	OPEAK	TPEAK	R.V.	
1	2	3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0115):			.83	.108	2.67	63.09
+ ID2= 2 (0107):			3.63	.354	2.33	59.36
ID = 3 (0114):			4.45	.455	2.33	60.05

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)		AREA	OPEAK	TPEAK	R.V.	
1	2	3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0102):			1.39	.194	2.50	47.26
+ ID2= 2 (0114):			4.45	.455	2.33	60.05
ID = 3 (0117):			5.85	.603	2.33	57.00

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)		AREA	OPEAK	TPEAK	R.V.	
1	2	3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0103):			6.22	.422	2.67	30.00
+ ID2= 2 (0117):			5.85	.603	2.33	57.00
ID = 3 (0106):			12.07	.989	2.67	43.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

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Page 22

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Page 23

Pre-Dev-Uncon-AES

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V   V   I   SSSSS U   U   A   L
V   V   I   SS   U   U   A   A   L
V   V   I   SS   U   U   AAAAA L
V   V   I   SS   U   U   A   A   L
VV   I   SSSSS UUUUU A   A   LLLL

000   TTTT   TTTT   H   H   Y   Y   M   M   000   TM, Version 2.0
0   0   T   T   H   H   Y   Y   M   M   0   0   Licensed To: MJ Davenport
000   T   T   H   H   Y   M   M   000   vo2-0057

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual otthymo v2.0\voin.dat  
output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Uncontrolled.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Uncontrolled.sum

DATE: 1/23/2019 TIME: 1:53:29 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 1 \*\*  
\*\*\*\*\*

MASS STORM | Filename: C:\visual otthymo files\4456\AES 1-hr.mst  
Ptotal= 22.50 mm | Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=

Duration of storm = 1.00 hrs  
Mass curve time step = 5.00 min

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	10.02	.33	69.93	.58	11.10	.83	.81
.17	30.00	.42	64.29	.67	4.62	.92	.30
.25	49.98	.50	27.03	.75	1.92	1.00	.03

CALIB | NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
Page 1

Pre-Dev-Uncon-AES

TOTAL RAINFALL (mm)= 22.500

RUNOFF COEFFICIENT = .224

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB | STANDHYD (0115) | Area (ha)= .83  
ID= 1 DT= 5.0 min | Total Imp(%)= 33.00 Dir. Conn.()%= 19.00

IMPERVIOUS PERVIOUS (i)  
Surface Area (ha)= .27 .55  
Dep. Storage (mm)= 1.00 2.00  
Average Slope (%)= 2.00 3.00  
Length (m)= 74.30 275.00  
Mannings n = .013 .250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

--- TRANSFORMED HYETOGRAPH ---							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	10.02	.33	69.93	.58	11.10	.83	.81
.167	30.00	.42	64.29	.67	4.62	.92	.30
.250	49.98	.50	27.03	.75	1.92	1.00	.03

Max.Eff.Inten.(mm/hr)= 69.93 14.12  
over (min)= 5.00 50.00  
Storage Coeff. (min)= 2.00 (ii) 45.48 (ii)

Unit Hyd. peak (min)= 3.00 50.00  
Unit Hyd. peak (cms)= .31 .02

\*TOTALS\*

PEAK FLOW (cms)= .03 .01 .030 (iii)  
TIME TO PEAK (hrs)= .33 1.17 .33  
RUNOFF VOLUME (mm)= 21.50 8.78 11.16  
TOTAL RAINFALL (mm)= 22.50 22.50 22.50  
RUNOFF COEFFICIENT = .96 .39 .50

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN<sup>2</sup> = 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB | STANDHYD (0107) | Area (ha)= 3.63  
ID= 1 DT= 5.0 min | Total Imp(%)= 29.40 Dir. Conn.()%= 19.00

IMPERVIOUS PERVIOUS (i)  
Surface Area (ha)= 1.07 2.56  
Dep. Storage (mm)= 1.00 3.00  
Average Slope (%)= 2.00 3.00  
Length (m)= 155.50 440.00  
Mannings n = .013 .250

Page 3

Pre-Dev-Uncon-AES

U.H. Tp(hrs)= .35

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

--- TRANSFORMED HYETOGRAPH ---							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.167	20.01	.500	45.66	.833	1.36		
.333	59.95	.667	7.86	1.000	.16		

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .038 (i)

TIME TO PEAK (hrs)= .667

RUNOFF VOLUME (mm)= 2.058

TOTAL RAINFALL (mm)= 22.500

RUNOFF COEFFICIENT = .091

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB   NASHYD (0112)   Area (ha)= 1.40 Curve Number (CN)= 75.0 ID= 1 DT=10.0 min   Ia (mm)= 5.00 # of Linear Res.(N)= 3.00 U.H. Tp(hrs)= .24
---

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .020 (i)

TIME TO PEAK (hrs)= .667

RUNOFF VOLUME (mm)= 2.957

TOTAL RAINFALL (mm)= 22.500

RUNOFF COEFFICIENT = .131

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)   1 + 2 = 3   AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm) + ID1= 1 (0105): 4.82 .038 .67 2.00 + ID2= 2 (0112): 1.40 .020 .67 2.96 ID = 3 (0103): 6.22 .058 .67 2.26
---

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB   NASHYD (0102)   Area (ha)= 1.39 Curve Number (CN)= 84.0 ID= 1 DT=10.0 min   Ia (mm)= 4.00 # of Linear Res.(N)= 3.00 U.H. Tp(hrs)= .24
---

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .034 (i)

TIME TO PEAK (hrs)= .500

RUNOFF VOLUME (mm)= 5.048

Page 2

Max.Eff.Inten.(mm/hr)= 69.93 8.11  
over (min)= 5.00 80.00  
Storage Coeff. (min)= 3.12 (ii) 75.07 (ii)  
Unit Hyd. Tpeak (min)= 5.00 80.00  
Unit Hyd. peak (cms)= .27 .01

\*TOTALS\*

PEAK FLOW (cms)= .12 .03 .125 (i)  
TIME TO PEAK (hrs)= .33 1.67 1.42  
RUNOFF VOLUME (mm)= 21.50 7.07 9.80  
TOTAL RAINFALL (mm)= 22.50 22.50 22.50  
RUNOFF COEFFICIENT = .96 .31 .44

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN<sup>2</sup> = 86.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114)   1 + 2 = 3   AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm) + ID1= 1 (0115): .83 .030 .33 11.16 + ID2= 2 (0107): 3.63 .125 .42 9.80 ID = 3 (0114): 4.45 .155 .42 10.05
--

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)   1 + 2 = 3   AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm) + ID1= 1 (0102): 1.39 .034 .50 5.05 + ID2= 2 (0114): 4.45 .155 .42 10.05 ID = 3 (0117): 5.85 .178 .42 8.86
--

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)   1 + 2 = 3   AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm) + ID1= 1 (0103): 0.22 .058 .67 2.26 + ID2= 2 (0117): 5.85 .178 .42 8.86 ID = 3 (0106): 12.07 .208 .42 5.46
--

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*

Page 3

Page 4

Pre-Dev-Uncon-AES

\*\* SIMULATION NUMBER: 2 \*\*

\*\*\*\*\*

MASS STORM | Filename: C:\visual otthymo files\4456\AES 1-hr.mst  
Ptotal= 30.50 mm | Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=

Duration of storm = 1.00 hrs  
Mass curve time step = 5.00 min

TIME hrs	RAIN mm/hr						
.08	13.58	.33	94.79	.58	15.04	.83	1.10
.17	40.66	.42	87.14	.67	6.26	.92	.40
.25	67.75	.50	36.64	.75	2.60	1.00	.04

CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .35

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.167	27.12	.500	61.89	.833	1.85	.22	
.333	81.27	.667	10.65	1.000			

Unit Hyd Ppeak (cms)= .522

PEAK FLOW (cms)= .076 (i)

TIME TO PEAK (hrs)= .667

RUNOFF VOLUME (mm)= 4.146

TOTAL RAINFALL (mm)= 30.500

RUNOFF COEFFICIENT = .136

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .24

Unit Hyd Ppeak (cms)= .222

PEAK FLOW (cms)= .039 (i)

TIME TO PEAK (hrs)= .500

RUNOFF VOLUME (mm)= 5.823

TOTAL RAINFALL (mm)= 30.500

RUNOFF COEFFICIENT = .191

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103) |

Page 5

Pre-Dev-Uncon-AES  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN\* = 88.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANHYD (0107) | Area (ha)= 3.63 Total Imp(%)= 29.40 Dir. Conn.()%= 19.00  
ID= 1 DT= 5.0 min

IMPERVIOUS PERVIOUS (i)

Surface Area (ha)= 1.07 2.56

Dep. Storage (mm)= 1.00 3.00

Average Slope (%)= 2.00 3.00

Length (m)= 155.50 440.00

Mannings n = .013 .250

Max.Eff.Inten.(mm/hr)= 94.79 13.96

over (min)= 5.00 65.00

Storage Coeff. (min)= 2.76 (ii) 60.68 (ii)

Unit Hyd. Tpeak (min)= 5.00 65.00

Unit Hyd. peak (cms)= .28 .02

\*TOTALS\*

PEAK FLOW (cms)= .17 .06 .174 (iii)

TIME TO PEAK (hrs)= .33 1.42 .33

RUNOFF VOLUME (mm)= 29.50 12.16 15.45

TOTAL RAINFALL (mm)= 30.50 30.50 30.50

RUNOFF COEFFICIENT = .97 .40 .51

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN\* = 86.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114) | 1 + 2 = 3 | AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
ID1= 1 (0115): .83 .044 .42 17.30  
+ ID2= 2 (0107): 3.63 .174 .33 15.45  
=====  
ID = 3 (0114): 4.45 .218 .42 15.79

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117) | 1 + 2 = 3 | AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
ID1= 1 (0102): 1.39 .064 .50 9.25

Pre-Dev-Uncon-AES  
| 1 + 2 = 3 | AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
+ ID1= 1 (0105): 4.82 .076 .67 4.15  
+ ID2= 2 (0112): 1.40 .039 .50 5.82  
=====  
ID = 3 (0103): 6.22 .115 .67 4.52

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
ID= 1 DT=10.0 min | Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .24

Unit Hyd Ppeak (cms)= .223

PEAK FLOW (cms)= .064 (i)

TIME TO PEAK (hrs)= .500

RUNOFF VOLUME (mm)= 9.250

TOTAL RAINFALL (mm)= 30.500

RUNOFF COEFFICIENT = .303

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115) | Area (ha)= .83 Total Imp(%)= 33.00 Dir. Conn.()%= 19.00  
ID= 1 DT= 5.0 min

IMPERVIOUS PERVIOUS (i)

Surface Area (ha)= .27 .55

Dep. Storage (mm)= 1.00 2.00

Average Slope (%)= 2.00 3.00

Length (m)= 74.30 275.00

Mannings n = .013 .250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TIME RAIN ---- TRANSFORMED HYETOGRAPH ----  
hrs mm/hr hrs mm/hr hrs mm/hr hrs mm hr  
.083 13.58 .333 94.79 .583 15.04 .83 1.10  
.167 40.66 .417 87.14 .667 6.26 .92 .40  
.250 67.75 .500 36.64 .750 2.60 1.00 .04  
  
Max.Eff.Inten.(mm/hr)= 94.79 29.46  
over (min)= 5.00 35.00  
Storage Coeff. (min)= 1.77 (ii) 34.17 (ii)  
Unit Hyd. Tpeak (min)= 5.00 35.00  
Unit Hyd. peak (cms)= .32 .03  
  
\*TOTALS\*  
PEAK FLOW (cms)= .04 .03 .044 (i)  
TIME TO PEAK (hrs)= .33 .92 .42  
RUNOFF VOLUME (mm)= 29.50 14.47 17.30  
TOTAL RAINFALL (mm)= 30.50 30.50 30.50  
RUNOFF COEFFICIENT = .97 .47 .57

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%

Page 6

Pre-Dev-Uncon-AES  
+ ID2= 2 (0114): 4.45 .218 .42 15.79  
ID = 3 (0117): 5.85 .262 .42 14.23

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106) | 1 + 2 = 3 | AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
ID1= 1 (0103): 6.22 .115 .67 4.52  
+ ID2= 2 (0117): 5.85 .262 .42 14.23  
=====  
ID = 3 (0106): 12.07 .324 .42 9.23

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

MASS STORM | Filename: C:\visual otthymo files\4456\AES 1-hr.mst  
Ptotal= 35.80 mm | Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=

Duration of storm = 1.00 hrs  
Mass curve time step = 5.00 min

TIME RAIN ---- TRANSFORMED HYETOGRAPH ----  
hrs mm/hr hrs mm/hr hrs mm/hr hrs mm hr  
.08 15.94 .33 111.24 .58 17.66 .83 1.29  
.17 47.73 .42 102.29 .67 7.35 .92 .47  
.25 79.52 .50 43.00 .75 3.05 1.00 .04

CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .35

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TIME RAIN ---- TRANSFORMED HYETOGRAPH ----  
hrs mm/hr hrs mm/hr hrs mm/hr hrs mm hr  
.167 31.83 .500 72.65 .833 2.17  
.333 95.39 .667 12.50 1.000 .26

Unit Hyd Ppeak (cms)= .522

PEAK FLOW (cms)= .108 (i)

TIME TO PEAK (hrs)= .667

RUNOFF VOLUME (mm)= 5.850

TOTAL RAINFALL (mm)= 35.800

RUNOFF COEFFICIENT = .163

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 8

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 7

Pre-Dev-Uncon-AES

CALIB	NASHYD (0112)	Area (ha)= 1.40	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .24			
Unit Hyd Qpeak (cms)= .222			
PEAK FLOW (cms)= .055 (i)			
TIME TO PEAK (hrs)= .500			
RUNOFF VOLUME (mm)= 8.105			
TOTAL RAINFALL (mm)= 35.800			
RUNOFF COEFFICIENT = .226			
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.			

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		(ha)= 1.40	.108	.67	5.85
ID1= 1 (0105):		4.82	.108	.67	5.85
+ ID2= 2 (0112):		1.40	.055	.50	8.11
ID = 3 (0103):		6.22	.161	.67	6.36

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	NASHYD (0102)	Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .24			
Unit Hyd Qpeak (cms)= .223			
PEAK FLOW (cms)= .086 (i)			
TIME TO PEAK (hrs)= .500			
RUNOFF VOLUME (mm)= 12.441			
TOTAL RAINFALL (mm)= 35.800			
RUNOFF COEFFICIENT = .348			
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.			

CALIB	STANDHYD (0115)	Area (ha)= .83	Total Imp(%)= 33.00	Dir. Conn. (%)= 19.00
ID= 1 DT= 5.0 min				
IMPERVIOUS PERVIOUS (i)				
Surface Area (ha)=	.27	.55		
Dep. Storage (mm)=	1.00	2.00		
Average Slope (%)=	2.00	3.00		
Length (m)=	74.30	275.00		
Mannings n =	.013	.250		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

Page 9

Pre-Dev-Uncon-AES

---- TRANSFORMED HYETOGRAPH ----			
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm hr
.083	15.94	.333	111.27
.167	47.73	.417	102.29
.250	79.52	.500	43.00
		.750	.750
		3.05	3.05
		1.00	.04

Max. Eff. Inten. (mm/hr)=	111.27	43.12
over (min)	5.00	30.00
Storage Coeff. (min)=	1.66 (ii)	29.48 (ii)
Unit Hyd. Tpeak (min)=	5.00	30.00
Unit Hyd. peak (cms)=	.32	.04
*TOTALS*		
PEAK FLOW (cms)=	.05	.04
TIME TO PEAK (hrs)=	.33	.83
RUNOFF VOLUME (mm)=	34.80	18.57
TOTAL RAINFALL (mm)=	35.80	35.80
RUNOFF COEFFICIENT =	.97	.52

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN\* = 88.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	STANDHYD (0107)	Area (ha)= 3.63	Total Imp(%)= 29.40	Dir. Conn. (%)= 19.00
ID= 1 DT= 5.0 min				
IMPERVIOUS PERVIOUS (i)				
Surface Area (ha)=	1.07	2.56		
Dep. Storage (mm)=	1.00	3.00		
Average Slope (%)=	2.00	3.00		
Length (m)=	155.50	440.00		
Mannings n =	.013	.250		
Max. Eff. Inten. (mm/hr)=	111.27	21.90		
over (min)	5.00	55.00		
Storage Coeff. (min)=	2.59 (ii)	50.95 (ii)		
Unit Hyd. Tpeak (min)=	5.00	55.00		
Unit Hyd. peak (cms)=	.29	.02		
*TOTALS*				
PEAK FLOW (cms)=	.20	.09	.208 (iii)	
TIME TO PEAK (hrs)=	.33	1.25	.42	
RUNOFF VOLUME (mm)=	34.80	15.91	19.40	
TOTAL RAINFALL (mm)=	35.80	35.80	35.80	
RUNOFF COEFFICIENT =	.97	.44	.54	

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN\* = 86.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 10

Pre-Dev-Uncon-AES

ADD HYD (0114)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		(ha)= .83	.055	.42	21.63
ID1= 1 (0115):		3.63	.208	.42	19.49
+ ID2= 2 (0107):					
ID = 3 (0114):		4.45	.263	.42	19.89

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		(ha)= .83	.086	.50	12.44
ID1= 1 (0102):		1.39	.086	.50	12.44
+ ID2= 2 (0114):		4.45	.263	.42	19.89
ID = 3 (0117):		5.85	.324	.42	18.13

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		(ha)= 6.22	.161	.67	6.36
ID1= 1 (0103):		6.22	.161	.67	6.36
+ ID2= 2 (0117):		5.85	.324	.42	18.13
ID = 3 (0106):		12.07	.413	.42	12.06

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\* SIMULATION NUMBER: 4 \*\*

MASS STORM Filename: C:\visual otthymo files\4456\AES 1-hour.mst  
Ptotal= 42.50 mm Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=

Duration of storm = 1.00 hrs  
Mass curve time step = 5.00 min

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.08	18.92	.33	132.09	.58	20.96
.17	56.66	.42	121.43	.67	8.72
.25	94.40	.50	51.05	.75	3.62
				1.00	.05

CALIB	NASHYD (0105)	Area (ha)= 4.82	Curve Number (CN)= 66.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	

Page 11

Pre-Dev-Uncon-AES

U.H. Tp(hr)= .35

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----			
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm hr
.167	37.79	.500	86.24
.333	113.25	.667	14.84
		1.000	.31

Unit Hyd Qpeak (cms)= .522
PEAK FLOW (cms)= .153 (i)
TIME TO PEAK (hrs)= .667
RUNOFF VOLUME (mm)= 8.327
TOTAL RAINFALL (mm)= 42.500
RUNOFF COEFFICIENT = .196
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0112)	Area (ha)= 1.40	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .24			
Unit Hyd Qpeak (cms)= .222			
PEAK FLOW (cms)= .078 (i)			
TIME TO PEAK (hrs)= .500			
RUNOFF VOLUME (mm)= 11.357			
TOTAL RAINFALL (mm)= 42.500			
RUNOFF COEFFICIENT = .267			
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.			

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		(ha)= 4.82	.153	.67	8.33
ID1= 1 (0105):		1.40	.078	.50	11.36
ID = 3 (0103):		6.22	.227	.67	9.01

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	NASHYD (0102)	Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00	
U.H. Tp(hr)= .24			
Unit Hyd Qpeak (cms)= .223			
PEAK FLOW (cms)= .117 (i)			
TIME TO PEAK (hrs)= .500			
RUNOFF VOLUME (mm)= 16.829			

Page 12

Pre-Dev-Uncon-AES

TOTAL RAINFALL (mm)=	42.500
RUNOFF COEFFICIENT =	.396
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.	
-----	
CALIB STANDHYD (0115)	Area (ha)= .83
ID= 1 DT= 5.0 min	Total Imp(%)= 33.00 Dir. Conn.(%)= 19.00
IMPERVIOUS PERVIOUS (i)	
Surface Area (ha)=	.27 .55
Dep. Storage (mm)=	1.00 2.00
Average Slope (%)=	2.00 3.00
Length (m)=	74.30 275.00
Mannings n =	.013 .250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083	18.92	.333	132.09	.583	20.96
.167	56.66	.417	121.43	.667	8.72
.250	94.40	.500	51.05	.750	3.62
				1.00	.05

Max.Eff.Inten.(mm/hr)=	132.09	64.88
over (min)=	5.00	30.00
Storage Coeff. (min)=	1.55 (ii)	25.18 (ii)
Unit Hyd. Tpeak (min)=	5.00	30.00
Unit Hyd. peak (cms)=	.33	.04
*TOTALS*		
PEAK FLOW (cms)=	.06	.05
TIME TO PEAK (hrs)=	.33	.83
RUNOFF VOLUME (mm)=	41.50	24.01
TOTAL RAINFALL (mm)=	42.50	42.50
RUNOFF COEFFICIENT =	.98	.56

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 86.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0107)	Area (ha)= 3.63
ID= 1 DT= 5.0 min	Total Imp(%)= 29.40 Dir. Conn.(%)= 19.00
IMPERVIOUS PERVIOUS (i)	
Surface Area (ha)=	1.07 2.56
Dep. Storage (mm)=	1.00 3.00
Average Slope (%)=	2.00 3.00
Length (m)=	155.50 440.00
Mannings n =	.013 .250

Page 13

Pre-Dev-Uncon-AES

Max.Eff.Inten.(mm/hr)=	132.09	35.82
over (min)=	5.00	45.00
Storage Coeff. (min)=	2.42 (ii)	42.14 (ii)
Unit Hyd. Tpeak (min)=	5.00	45.00
Unit Hyd. peak (cms)=	.30	.03
PEAK FLOW (cms)=	.24	.14
TIME TO PEAK (hrs)=	.33	1.08
RUNOFF VOLUME (mm)=	41.50	20.95
TOTAL RAINFALL (mm)=	42.50	42.50
RUNOFF COEFFICIENT =	.98	.49

\*TOTALS\*  
\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 86.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114)	1 + 2 = 3
ID1= 1 (0115):	Area (ha) .83 OPEAK (cms) .069 TPEAK (hrs) .42 R.V. (mm) 27.31
+ ID2= 2 (0107):	3.63 .257 .42 24.85
ID = 3 (0114):	4.45 .325 .42 25.31

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)	1 + 2 = 3
ID1= 1 (0102):	Area (ha) 1.39 OPEAK (cms) .117 TPEAK (hrs) .50 R.V. (mm) 16.83
+ ID2= 2 (0114):	4.45 .325 .42 25.31
ID = 3 (0117):	5.85 .409 .42 23.30

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)	1 + 2 = 3
ID1= 1 (0103):	Area (ha) 6.22 OPEAK (cms) .227 TPEAK (hrs) .67 R.V. (mm) 9.01
+ ID2= 2 (0117):	5.85 .409 .42 23.30
ID = 3 (0106):	12.07 .538 .42 15.93

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 14

Pre-Dev-Uncon-AES

\*\* SIMULATION NUMBER: 5 \*\*

MASS STORM	Filename: C:\visual otthymo files\4456\AES 1-hr.mst				
Pttotal= 47.40 mm	Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=				
Duration of storm = 1.00 hrs					
Mass curve time step = 5.00 min					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.08	21.10	.33	147.32	.58	23.38
.17	63.19	.42	135.43	.67	9.73
.25	105.28	.50	56.94	.75	4.04
				1.00	.06

Pre-Dev-Uncon-AES

1 + 2 = 3	AREA (ha) OPEAK (cms) TPEAK (hrs) R.V. (mm)
ID1= 1 (0105):	4.82 .190 .67 10.34
+ ID2= 2 (0112):	1.40 .096 .50 13.96
ID = 3 (0103):	6.22 .281 .67 11.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha) 1.39 Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .24	

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .141 (i)
TIME TO PEAK (hrs)= .500
RUNOFF VOLUME (mm)= 20.244
TOTAL RAINFALL (mm)= 47.400
RUNOFF COEFFICIENT = .427

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115)	Area (ha) .83
ID= 1 DT= 5.0 min	Total Imp(%)= 33.00 Dir. Conn.(%)= 19.00

IMPERVIOUS (ha)	PERVIOUS (i)
Surface Area (ha)= .27 .55	
Dep. Storage (mm)= 1.00 2.00	
Average Slope (%)= 2.00 3.00	
Length (m)= 74.30 275.00	
Mannings n = .013 .250	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083	21.10	.333	147.32	.583	23.38
.167	63.19	.417	135.43	.667	9.73
.250	105.28	.500	56.94	.750	4.04
				1.00	.06

Max.Eff.Inten.(mm/hr)=	147.32	75.84
over (min)=	5.00	25.00
Storage Coeff. (min)=	1.49 (ii)	23.68 (ii)
Unit Hyd. Tpeak (min)=	5.00	25.00
Unit Hyd. peak (cms)=	.33	.05

PEAK FLOW (cms)= .06 .084 (iii)
TIME TO PEAK (hrs)= .33 .75
RUNOFF VOLUME (mm)= 46.40 28.13
TOTAL RAINFALL (mm)= 47.40 47.40
RUNOFF COEFFICIENT = .59 .67

\*TOTALS\*  
\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%

Page 15

Pre-Dev-Uncon-AES  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 $CN^* = 88.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANHYD (0107) ID= 1 DT= 5.0 min	Area (ha)=	3.63	Dir. Conn. (%)= 19.00
	Total Imp(%)=	29.40	
	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	1.00	2.56	
Dep. Storage (mm)=	2.00	3.00	
Average Slope (%)=	2.00	3.00	
Length (m)=	155.50	440.00	
Mannings n =	.013	.250	
Max.Eff.Inten.(mm/hr)=	147.32	42.43	
over (min)=	5.00	40.00	
Storage Coeff. (min)=	2.32 (ii)	39.44 (ii)	
Unit Hyd. Tpeak (min)=	5.00	40.00	
Unit Hyd. peak (cms)=	.30	.03	
PEAK FLOW (cms)=	.27	.18	*TOTALS*
TIME TO PEAK (hrs)=	.33	1.00	.42
RUNOFF VOLUME (mm)=	46.40	24.82	28.91
TOTAL RAINFALL (mm)=	47.40	47.40	47.40
RUNOFF COEFFICIENT =	.98	.52	.61

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 $CN^* = 86.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Pre-Dev-Uncon-AES  
+ ID2= 2 (0114): 4.45 .378 .42 29.41  
ID = 3 (0117): 5.85 .480 .42 27.23

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 +	2 = 3				
ID1= 1 (0103):		6.22	.281	.67	11.16
+ ID2= 2 (0117):		5.85	.480	.42	27.23

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 6 \*\*  
\*\*\*\*\*

MASS STORM Ptotal= 52.40 mm	Filename: C:\visual otthymo files\4456\AES 1-hr.mst
	Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=

DURATION OF STORM = 1.00 hrs

Mass curve time step = 5.00 min

TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.08	23.33	.33	162.86	.58	25.84
.17	69.86	.42	149.72	.67	10.75
.25	116.39	.50	62.94	.75	4.46

CALIB NASHYD (0105) ID= 1 DT=10.0 min	Area (ha)=	4.82	Curve Number (CN)= 66.0
	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	.35	

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TRANSFORMED HYETOGRAPH					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.167	46.59	.520	106.33	.832	3.18
.333	139.63	.667	18.30	1.000	.38

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .231 (i)

TIME TO PEAK (hrs)= .667

RUNOFF VOLUME (mm)= 12.566

TOTAL RAINFALL (mm)= 52.400

RUNOFF COEFFICIENT = .240

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 18

ADD HYD (0114)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0115):		.83	.084	.42	31.59
+ ID2= 2 (0107):		3.63	.295	.42	28.91
ID = 3 (0114):		4.45	.378	.42	29.41

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0102):		1.39	.141	.50	20.24

Page 17

Pre-Dev-Uncon-AES

CALIB NASHYD (0112)	Area (ha)=	1.40	Curve Number (CN)= 75.0
	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	.24	
Unit Hyd Qpeak (cms)=	.222		
PEAK FLOW (cms)=	.115 (i)		
TIME TO PEAK (hrs)=	.500		
RUNOFF VOLUME (mm)=	16.785		
TOTAL RAINFALL (mm)=	52.400		
RUNOFF COEFFICIENT =	.320		

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TRANSFORMED HYETOGRAPH					
TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.083	23.33	.33	162.86	.583	25.84
.17	69.86	.417	149.72	.667	10.75
.25	116.39	.500	62.94	.750	4.46

Max.Eff.Inten.(mm/hr)= 162.86

over (min)= 5.00

Storage Coeff. (min)= 1.43 (ii)

Unit Hyd. Tpeak (min)= 5.00

Unit Hyd. peak (cms)= .33

\*TOTALS\*

PEAK FLOW (cms)=	.07	.09	.096 (iii)
TIME TO PEAK (hrs)=	.33	.75	.42
RUNOFF VOLUME (mm)=	51.40	32.43	36.02
TOTAL RAINFALL (mm)=	52.40	52.40	52.40
RUNOFF COEFFICIENT =	.98	.62	.69

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%

YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 $CN^* = 88.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANHYD (0107)	Area (ha)=	3.63
	Total Imp(%)=	29.40
	Dir. Conn. (%)=	19.00
	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	1.07	2.56
Dep. Storage (mm)=	1.00	3.00
Average Slope (%)=	2.00	3.00
Length (m)=	155.50	440.00
Mannings n =	.013	.250

Max.Eff.Inten.(mm/hr)= 162.86

over (min)= 5.00

Storage Coeff. (min)= 2.23 (ii)

Unit Hyd. Tpeak (min)= 5.00

Unit Hyd. peak (cms)= .30

\*TOTALS\*

PEAK FLOW (cms)=	.30	.22	.331 (iii)
TIME TO PEAK (hrs)=	.33	1.00	.42
RUNOFF VOLUME (mm)=	51.40	28.88	33.15
TOTAL RAINFALL (mm)=	52.40	52.40	52.40
RUNOFF COEFFICIENT =	.98	.55	.63

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%

YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 $CN^* = 86.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 20

Page 19

ADD HYD	(0114)		
1 + 2	= 3		
AREA	QPEAK	TPEAK	R.V.
(ha)	(cms)	(hrs)	(mm)
+ ID1= 1 (0115):	.83	.096	.42 36.02
+ ID2= 2 (0107):	3.63	.331	.42 33.15
=====			
ID = 3 (0114):	4.45	.428	.42 33.69

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD	(0117)		
1 + 2	= 3		
AREA	QPEAK	TPEAK	R.V.
(ha)	(cms)	(hrs)	(mm)
+ ID1= 1 (0102):	1.39	.166	.50 23.88
+ ID2= 2 (0114):	4.45	.428	.42 33.69
=====			
ID = 3 (0117):	5.85	.549	.42 31.36

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD	(0106)		
1 + 2	= 3		
AREA	QPEAK	TPEAK	R.V.
(ha)	(cms)	(hrs)	(mm)
+ ID1= 1 (0103):	6.22	.339	.67 13.51
+ ID2= 2 (0117):	5.85	.549	.42 31.36
=====			
ID = 3 (0106):	12.07	.747	.42 22.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

Pre-Dev-Uncon-SCS

```

V   V   I   SSSSS U   U   A   L
V   V   I   SS   U   U   A   A   L
V   V   I   SS   U   U   AAAAA L
V   V   I   SS   U   U   A   A   L
V   V   I   SSSSS UUUUU A   A   LLLL

000   TTTTT TTTTT H   H   Y   Y   M   M   000   TM, Version 2.0
0   0   T   T   H   H   Y   Y   M   M   0   0   Licensed To: MJ Davenport
000   T   T   H   H   Y   M   M   000   vo2-0057

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual otthymo v2.0\voin.dat

output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Uncontrolled.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Uncontrolled.sum

DATE: 1/23/2019 TIME: 1:51:00 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 1 \*\*  
\*\*\*\*\*

MASS STORM	Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst
Pttotal= 38.40 mm	Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Duration of storm = 6.00 hrs  
Mass curve time step = 10.0 min

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	1.61	1.67	3.92	3.17	8.52	4.67	2.30
.33	1.38	1.83	3.69	3.33	8.29	4.83	2.30
.50	1.61	2.00	3.92	3.50	8.52	5.00	2.30
.67	2.30	2.17	4.61	3.67	3.92	5.17	1.61
.83	2.30	2.33	4.61	3.83	3.69	5.33	1.38
1.00	2.30	2.50	4.61	4.00	3.92	5.50	1.61
1.17	2.30	2.67	23.04	4.17	3.00	5.67	1.61
1.33	2.30	2.83	41.47	4.33	3.23	5.83	1.38
1.50	2.30	3.00	59.90	4.50	3.00	6.00	1.61

Page 1

Pre-Dev-Uncon-SCS

CALIB NASHYD (0105)	Area (ha)= 4.82	Curve Number (CN)= 66.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .35		

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .071 (i)  
TIME TO PEAK (hrs)= 3.167  
RUNOFF VOLUME (mm)= 6.771  
TOTAL RAINFALL (mm)= 38.400  
RUNOFF COEFFICIENT = .176

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0112)	Area (ha)= 1.40	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .24		

Unit Hyd Qpeak (cms)= .222  
PEAK FLOW (cms)= .037 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 9.322  
TOTAL RAINFALL (mm)= 38.400  
RUNOFF COEFFICIENT = .243

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0105):	4.82	.071	3.17	6.77
+ ID2= 2 (0112):	1.40	.037	3.00	9.32
ID = 3 (0103):	6.22	.107	3.17	7.34

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .24		

Unit Hyd Qpeak (cms)= .223  
PEAK FLOW (cms)= .058 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 14.101  
TOTAL RAINFALL (mm)= 38.400  
RUNOFF COEFFICIENT = .367

Page 2

Pre-Dev-Uncon-SCS

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115)	Area (ha)= .83
Total Imp(%)= 33.00	Dir. Conn.(%)= 19.00
ID= 1 DT= 5.0 min	
IMPERVIOUS PERVIOUS (i)	
Surface Area (ha)= .27	.55
Dep. Storage (mm)= 1.00	2.00
Average Slope (%)= 2.00	3.00
Length (m)= 74.30	275.00
Mannings n = .013	.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	1.61	1.583	3.92	3.083	8.53	4.58	2.30
.167	1.61	1.667	3.92	3.167	8.52	4.67	2.30
.250	1.38	1.750	3.69	3.250	8.29	4.75	2.30
.333	1.38	1.833	3.69	3.333	8.29	4.83	2.30
.417	1.61	1.917	3.92	3.417	8.52	4.92	2.30
.500	1.61	2.000	3.92	3.500	8.52	5.00	2.30
.583	2.30	2.083	4.61	3.583	3.92	5.08	1.61
.667	2.30	2.167	4.61	3.667	3.92	5.17	1.61
.750	2.30	2.250	4.61	3.750	3.69	5.25	1.38
.833	2.30	2.333	4.61	3.833	3.69	5.33	1.38
.917	2.30	2.417	4.61	3.917	3.92	5.42	1.61
1.000	2.30	2.500	4.61	4.000	3.92	5.50	1.61
1.083	2.30	2.583	23.04	4.083	3.00	5.58	1.61
1.167	2.30	2.667	23.04	4.167	3.00	5.67	1.61
1.250	2.30	2.750	41.47	4.250	3.23	5.75	1.38
1.333	2.30	2.833	41.47	4.333	3.23	5.83	1.38
1.417	2.30	2.917	59.90	4.417	3.00	5.92	1.61
1.500	2.30	3.000	59.90	4.500	3.00	6.00	1.61

Max.Eff.Inten.(mm/hr)= 59.90 25.36  
over (min)= 5.00 40.00  
Storage Coeff. (min)= 2.13 (ii) 36.53 (ii)  
Unit Hyd. Tpeak (min)= 5.00 40.00  
Unit Hyd. peak (cms)= .31 .03

\*TOTALS\*

PEAK FLOW (cms)= .03 .02 .035 (iii)  
TIME TO PEAK (hrs)= 3.00 3.50 3.00  
RUNOFF VOLUME (mm)= 37.40 20.65 23.80  
TOTAL RAINFALL (mm)= 38.40 38.40 38.40  
RUNOFF COEFFICIENT = .97 .54 .62

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN<sup>2</sup> = 88.0 Ta = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 3

Pre-Dev-Uncon-SCS

CALIB STANDHYD (0107)	Area (ha)= 3.63
Total Imp(%)= 29.40	Dir. Conn.(%)= 19.00
ID= 1 DT= 5.0 min	

IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)= 1.07	2.56
Dep. Storage (mm)= 1.00	3.00
Average Slope (%)= 2.00	3.00
Length (m)= 155.50	440.00
Mannings n = .013	.250
Max.Eff.Inten.(mm/hr)= 59.90	14.73
over (min)= 5.00	60.00
Storage Coeff. (min)= 3.32 (ii)	59.99 (ii)
Unit Hyd. Tpeak (min)= 5.00	60.00
Unit Hyd. peak (cms)= .26	.02

\*TOTALS\*

PEAK FLOW (cms)= .11 .06 .126 (iii)  
TIME TO PEAK (hrs)= 3.00 3.32 3.00  
RUNOFF VOLUME (mm)= 37.40 12.83 21.54  
TOTAL RAINFALL (mm)= 38.40 38.40 38.40  
RUNOFF COEFFICIENT = .97 .46 .56

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN<sup>2</sup> = 86.0 Ta = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0115):	.83	.035	3.00	23.80
+ ID2= 2 (0107):	3.63	.126	3.00	21.54
ID = 3 (0114):	4.45	.161	3.00	21.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (0115):	1.39	.058	3.00	14.10
+ ID2= 2 (0114):	4.45	.161	3.00	21.96
ID = 3 (0117):	5.85	.219	3.00	20.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 4

Pre-Dev-Uncon-SCS

ADD HYD (0106)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0103):	6.22	.107	3.17	7.34	
+ ID2= 2 (0117):	5.85	.219	3.00	20.09	
ID = 3 (0106):	12.07	.309	3.00	13.52	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 2 \*\*  
\*\*\*\*\*

MASS STORM Ptotal= 50.50 mm | Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst  
Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Duration of storm = 6.00 hrs  
Mass curve time step = 10.00 min

TIME hrs	RAIN mm/hr						
.17	2.12	1.67	5.15	3.17	11.21	4.67	3.03
.33	1.82	1.83	4.85	3.33	10.91	4.83	3.03
.50	2.12	2.00	5.15	3.50	11.21	5.00	3.03
.67	3.03	2.17	6.04	3.47	5.15	5.17	2.12
.83	3.03	2.23	6.06	3.83	4.85	5.33	2.35
1.00	3.03	2.50	6.06	4.00	5.15	5.50	2.55
1.17	3.03	2.67	30.30	4.17	3.94	5.67	2.12
1.33	3.03	2.83	54.54	4.33	4.24	5.83	1.82
1.50	3.03	3.00	78.78	4.50	3.94	6.00	2.12

CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .35

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .126 (i)  
TIME TO PEAK (hrs)= 3.167  
RUNOFF VOLUME (mm)= 11.703  
TOTAL RAINFALL (mm)= 50.500  
RUNOFF COEFFICIENT = .232

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .24

unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .064 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 15.692

Page 5

Pre-Dev-Uncon-SCS  
TOTAL RAINFALL (mm)= 50.500  
RUNOFF COEFFICIENT = .311

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103) | 1 + 2 = 3 AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
ID1= 1 (0105): 4.82 .126 3.17 11.21  
+ ID2= 2 (0112): 1.40 .064 3.00 15.69  
ID = 3 (0103): 6.22 .186 3.17 12.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
ID= 1 DT=10.0 min | Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .24

unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .095 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 22.480  
TOTAL RAINFALL (mm)= 50.500  
RUNOFF COEFFICIENT = .445

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115) | Area (ha)= .83  
ID= 1 DT= 5.0 min | Total Imp% = 33.00 Dir. Conn.(%)= 19.00

IMPERVIOUS PERVIOUS (i)  
Surface Area (ha)= .27 .55  
Dep. Storage (mm)= 1.00 2.00  
Average Slope (%)= 2.00 3.00  
Length (m)= 74.30 275.00  
Mannings n = .013 .250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TIME RAIN TRANSFORMED HYETOGRAPH  
hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr  
.083 2.12 1.583 5.15 3.083 11.21 4.58 3.03  
.167 2.12 1.667 5.15 3.167 11.21 4.67 3.03  
.250 1.82 1.750 4.85 3.250 10.91 4.75 3.03  
.333 1.82 1.833 4.85 3.333 10.91 4.83 3.03  
.417 2.12 1.917 5.15 3.417 11.21 4.92 3.03  
.500 2.12 2.000 5.15 3.500 11.21 5.00 3.03  
.583 3.03 2.083 6.06 3.583 5.15 5.08 2.12  
.667 3.03 2.167 6.06 3.667 5.15 5.17 2.12  
.750 3.03 2.250 6.06 3.750 4.85 5.25 1.82

Page 6

Pre-Dev-Uncon-SCS  
.833 3.03 | 2.333 6.06 | 3.833 4.85 | 5.33 1.82  
.917 3.03 | 2.417 6.06 | 3.917 5.15 | 5.42 2.12  
1.000 3.03 | 2.500 6.06 | 4.000 5.15 | 5.50 2.12  
1.083 3.03 | 2.583 30.30 | 4.083 3.94 | 5.58 2.12  
1.167 3.03 | 2.667 30.30 | 4.167 3.94 | 5.67 2.12  
1.250 3.03 | 2.750 54.54 | 4.250 4.24 | 5.75 1.82  
1.333 3.03 | 2.833 54.54 | 4.333 4.24 | 5.83 1.82  
1.417 3.03 | 2.917 78.78 | 4.417 3.94 | 5.92 2.12  
1.500 3.03 | 3.000 78.78 | 4.500 3.94 | 6.00 2.12

Max.Eff.Inten.(mm/hr)= 78.78 42.77  
over (min)= 5.00 30.00  
Storage Coeff. (min)= 1.91 (ii) 29.82 (ii)  
Unit Hyd. Tpeak (min)= 5.00 30.00  
Unit Hyd. peak (cms)= .32 .04

\*TOTALS\*  
PEAK FLOW (cms)= .03 .04 .055 (iii)  
TIME TO PEAK (hrs)= 3.00 3.33 3.00  
RUNOFF VOLUME (mm)= 49.50 30.79 34.32  
TOTAL RAINFALL (mm)= 50.50 50.50 50.50  
RUNOFF COEFFICIENT = .98 .61 .68

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0107) | Area (ha)= 3.63 Dir. Conn.(%)= 19.00  
ID= 1 DT= 5.0 min | Total Imp% = 29.40

IMPERVIOUS PERVIOUS (i)  
Surface Area (ha)= 1.07 2.56  
Dep. Storage (mm)= 1.00 3.00  
Average Slope (%)= 2.00 3.00  
Length (m)= 155.50 440.00  
Mannings n = .013 .230

Max.Eff.Inten.(mm/hr)= 78.78 26.97  
over (min)= 5.00 50.00  
Storage Coeff. (min)= 2.98 (ii) 47.47 (ii)  
Unit Hyd. Tpeak (min)= 5.00 50.00  
Unit Hyd. peak (cms)= .28 .02

\*TOTALS\*  
PEAK FLOW (cms)= .15 .11 .182 (iii)  
TIME TO PEAK (hrs)= 3.00 3.67 3.00  
RUNOFF VOLUME (mm)= 49.50 27.32 31.53  
TOTAL RAINFALL (mm)= 50.50 50.50 50.50  
RUNOFF COEFFICIENT = .98 .54 .62

\*\*\*\*\* WARNING: STORAGE COFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 86.0 Ia = Dep. Storage (Above)

Page 7

Pre-Dev-Uncon-SCS  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114) | 1 + 2 = 3 AREA QPEAK TPEAK R.V.  
ID1= 1 (0115): .83 .055 3.00 34.32  
+ ID2= 2 (0107): 3.63 .182 3.00 31.53  
ID = 3 (0114): 4.45 .237 3.00 32.05

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117) | 1 + 2 = 3 AREA QPEAK TPEAK R.V.  
ID1= 1 (0102): 1.39 .095 3.00 22.48  
+ ID2= 2 (0114): 4.45 .237 3.00 32.05  
ID = 3 (0117): 5.85 .332 3.00 29.77

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106) | 1 + 2 = 3 AREA QPEAK TPEAK R.V.  
ID1= 1 (0103): 6.22 .186 3.17 12.60  
+ ID2= 2 (0117): 5.85 .332 3.00 29.77  
ID = 3 (0106): 12.07 .492 3.00 20.92

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 3 \*\*  
\*\*\*\*\*

MASS STORM Ptotal= 58.60 mm | Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst  
Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Duration of storm = 6.00 hrs  
Mass curve time step = 10.00 min

TIME hrs	RAIN mm/hr						
.17	2.46	1.67	5.98	3.17	13.01	4.67	3.52
.33	2.11	1.83	5.63	3.33	12.66	4.83	3.52
.50	2.46	2.00	5.98	3.50	13.01	5.00	3.52
.67	3.52	2.17	7.03	3.67	5.98	5.17	2.46
.83	3.52	2.33	7.03	3.83	5.63	5.33	2.11
1.00	3.52	2.50	7.03	4.00	5.98	5.50	2.46

Page 8

Pre-Dev-Uncon-SCS							
1.17	3.52	2.67	35.16	4.17	4.57	5.67	2.46
1.33	3.52	2.83	63.29	4.33	4.92	5.83	2.11
1.50	3.52	3.00	91.42	4.50	4.57	6.00	2.46

TOTAL RAINFALL (mm) = 58.600  
RUNOFF COEFFICIENT = .487

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0105)	Area (ha) = 4.82	Curve Number (CN) = 66.0
ID= 1 DT=10.0 min	Ia (mm) = 5.00	# of Linear Res.(N) = 3.00

Unit Hyd Qpeak (cms) = .522

PEAK FLOW (cms) = .169 (i)

TIME TO PEAK (hrs) = 3.167

RUNOFF VOLUME (mm) = 15.528

TOTAL RAINFALL (mm) = 58.600

RUNOFF COEFFICIENT = .265

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115)	Area (ha) = .83	Curve Number (CN) = 75.0
ID= 1 DT= 5.0 min	Total Imp(%) = 33.00	Dir. Conn.(%) = 19.00

IMPERVIOUS PERVIOUS (i)  
Surface Area (ha) = .27 .55  
Dep. Storage (mm) = 1.00 2.00  
Average Slope (%) = 2.00 3.00  
Length (m) = 74.30 275.00  
Mannings n = .013 .250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

CALIB NASHYD (0112)	Area (ha) = 1.40	Curve Number (CN) = 75.0
ID= 1 DT=10.0 min	Ia (mm) = 5.00	# of Linear Res.(N) = 3.00

Unit Hyd Qpeak (cms) = .222

PEAK FLOW (cms) = .084 (i)

TIME TO PEAK (hrs) = 3.000

RUNOFF VOLUME (mm) = 20.501

TOTAL RAINFALL (mm) = 58.600

RUNOFF COEFFICIENT = .350

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0105):		4.82	.169	3.17	15.53
+ ID2= 2 (0112):		1.40	.084	3.00	20.50
ID = 3 (0103):		6.22	.248	3.17	16.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha) = 1.39	Curve Number (CN) = 84.0
ID= 1 DT=10.0 min	Ia (mm) = 4.00	# of Linear Res.(N) = 3.00

U.H. Tp(hrs) = .24

Unit Hyd Qpeak (cms) = .223

PEAK FLOW (cms) = .122 (i)

TIME TO PEAK (hrs) = 3.000

RUNOFF VOLUME (mm) = 28.556

Page 9

Pre-Dev-Uncon-SCS  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0107)	Area (ha) = 3.63	Total Imp(%) = 29.40	Dir. Conn.(%) = 19.00
--------------------------	------------------	----------------------	-----------------------

IMPERVIOUS PERVIOUS (i)  
Surface Area (ha) = 1.07 2.56  
Dep. Storage (mm) = 1.00 3.00  
Average Slope (%) = 2.00 3.00  
Length (m) = 155.50 440.00  
Mannings n = .013 .250

Max.Eff.Inten.(mm/hr)= 91.42 36.55  
over (min) = 5.00 45.00  
Storage Coeff. (min)= 2.80 (ii) 42.21 (ii)  
Unit Hyd. Peak (min)= 5.00 45.00  
Unit Hyd. peak (cms)= .28 .03 \*TOTALS\*  
PEAK FLOW (cms) = .17 .15 .225 (iii)  
TIME TO PEAK (hrs) = 3.00 3.58 3.00  
RUNOFF VOLUME (mm) = 57.60 34.06 38.53  
TOTAL RAINFALL (mm) = 58.60 58.60 58.60  
RUNOFF COEFFICIENT = .98 .58 .66

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN<sup>2</sup> = 86.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0115):		.83	.068	3.00	41.61
+ ID2= 2 (0107):		3.63	.225	3.00	38.53
ID = 3 (0114):		4.45	.293	3.00	39.10

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0102):		1.39	.122	3.00	28.56
+ ID2= 2 (0114):		4.45	.293	3.00	39.10
ID = 3 (0117):		5.85	.415	3.00	36.59

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 11

Pre-Dev-Uncon-SCS

TOTAL RAINFALL (mm) = 58.600  
RUNOFF COEFFICIENT = .487

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115)	Area (ha) = .83	Curve Number (CN) = 75.0
ID= 1 DT= 5.0 min	Total Imp(%) = 33.00	Dir. Conn.(%) = 19.00

IMPERVIOUS PERVIOUS (i)  
Surface Area (ha) = .27 .55  
Dep. Storage (mm) = 1.00 2.00  
Average Slope (%) = 2.00 3.00  
Length (m) = 74.30 275.00  
Mannings n = .013 .250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TRANSFORMED HYETOGRAPH							
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm/hr
.083	2.46	1.583	5.98	3.083	13.01	4.58	3.52
.167	2.46	1.667	5.98	3.167	13.01	4.67	3.52
.250	2.11	1.750	5.63	3.250	12.66	4.75	3.52
.333	2.11	1.833	5.63	3.333	12.36	4.83	3.52
.417	2.46	1.917	5.98	3.417	13.01	4.92	3.52
.500	2.46	2.000	5.98	3.500	13.01	5.00	3.52
.583	3.52	2.083	7.03	3.583	5.98	5.08	2.46
.667	3.52	2.167	7.03	3.667	5.98	5.17	2.46
.750	3.52	2.250	7.03	3.750	5.63	5.25	2.11
.833	3.52	2.333	7.03	3.833	5.63	5.33	2.11
.917	3.52	2.417	7.03	3.917	5.98	5.42	2.46
1.000	3.52	2.500	7.03	4.000	5.98	5.50	2.46
1.083	3.52	2.583	35.16	4.083	4.57	5.58	2.46
1.167	3.52	2.667	35.16	4.167	4.57	5.67	2.46
1.250	3.52	2.750	63.29	4.250	4.92	5.75	2.11
1.333	3.52	2.833	63.29	4.333	4.92	5.83	2.11
1.417	3.52	2.917	91.42	4.417	4.97	5.92	2.46
1.500	3.52	3.000	91.42	4.500	4.57	6.00	2.46

Max.Eff.Inten.(mm/hr)= 91.42 59.44  
over (min) = 5.00 30.00  
Storage Coeff. (min)= 1.80 (ii) 26.27 (ii)  
Unit Hyd. Tpeak (min)= 5.00 30.00  
Unit Hyd. peak (cms)= .32 .04

\*TOTALS\*

PEAK FLOW (cms) = .04 .05 .068 (iii)  
TIME TO PEAK (hrs) = 3.00 3.33 3.00  
RUNOFF VOLUME (mm) = 57.60 37.89 41.61  
TOTAL RAINFALL (mm) = 58.60 58.60 58.60  
RUNOFF COEFFICIENT = .98 .65 .71

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN<sup>2</sup> = 88.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.

Page 10

ADD HYD (0106)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0103):		6.22	.248	3.17	16.64
+ ID2= 2 (0117):		5.85	.415	3.00	36.59
ID = 3 (0106):		12.07	.629	3.00	26.31

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\* SIMULATION NUMBER: 4 \*\*  
\*\*\*\*\*

MASS STORM Ptotal= 68.70 mm	Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst
Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION	

DURATION OF STORM = 6.00 hrs  
Mass curve time step = 10.00 min

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm hr
.17	2.89	1.67	7.01	3.17	15.25
.33	2.47	1.83	6.60	3.33	14.84
.50	2.89	2.00	7.01	3.50	15.25
.67	4.12	2.17	8.24	3.67	7.00
.83	4.12	2.33	8.24	4.83	6.00
1.00	4.12	2.50	8.24	5.00	5.33
1.17	4.12	2.67	41.22	4.17	5.36
1.33	4.12	2.83	74.20	4.33	5.77
1.50	4.12	3.00	107.17	4.50	5.36

CALIB NASHYD (0105)	Area (ha) = 4.82	Curve Number (CN) = 66.0
ID= 1 DT=10.0 min	Ia (mm) = 5.00	# of Linear Res.(N) = 3.00

Unit Hyd Qpeak (cms) = .522

PEAK FLOW (cms) = .228 (i)

TIME TO PEAK (hrs) = 3.167

RUNOFF VOLUME (mm) = 20.792

TOTAL RAINFALL (mm) = 68.700

RUNOFF COEFFICIENT = .303

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0112)	Area (ha) = 1.40	Curve Number (CN) = 75.0
ID= 1 DT=10.0 min	Ia (mm) = 5.00	# of Linear Res.(N) = 3.00

Unit Hyd Qpeak (cms) = .222

Page 12

## Pre-Dev-Uncon-SCS

PEAK FLOW (cms)= .112 (i)  
 TIME TO PEAK (hrs)= 3.000  
 RUNOFF VOLUME (mm)= 26.984  
 TOTAL RAINFALL (mm)= 68.700  
 RUNOFF COEFFICIENT = .393

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0105):	4.82	.228	3.17	20.79	
+ ID2= 2 (0112):	1.40	.112	3.00	26.98	

ID = 3 (0103): 6.22 .332 3.17 22.18

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha)	1.39	Curve Number (CN)= 84.0
ID= 1 DT= 10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00	U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .157 (i)  
 TIME TO PEAK (hrs)= 3.000  
 RUNOFF VOLUME (mm)= 36.516  
 TOTAL RAINFALL (mm)= 68.700  
 RUNOFF COEFFICIENT = .532

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115)	Area (ha)	.83	Total Imp(%)	33.00	Dir. Conn. (%)	19.00
ID= 1 DT= 5.0 min						

IMPERVIOUS		PERVIOUS (i)	
Surface Area (ha)= .27	.55	Dep. Storage (mm)= 1.00	2.00
Average Slope (%)= 2.00	3.00	Length (m)= 74.30	275.00
Mannings n = .013	.250		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----						
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs
.083 2.89	1.583 7.01	3.083 15.25	4.58 4.12			
.167 2.89	1.667 7.01	3.167 15.25	4.67 4.12			
.250 2.47	1.750 6.60	3.250 14.84	4.75 4.12			
.333 2.4	1.833 6.68	3.333 14.84	4.83 4.12			
.417 2.89	1.917 7.01	3.417 15.25	4.92 4.12			
.500 2.89	2.000 7.01	3.500 15.25	5.00 4.12			

Page 13

Pre-Dev-Uncon-SCS					
.583	4.12	2.083	8.24	3.583	7.01
.667	4.12	2.167	8.24	3.667	7.01
.750	4.12	2.250	8.24	3.750	6.60
.833	4.12	2.333	8.24	3.833	6.60
.917	4.12	2.417	8.24	3.917	7.01
1.000	4.12	2.500	8.24	4.000	7.01
1.083	4.12	2.583	41.22	4.083	5.36
1.167	4.12	2.667	41.22	4.167	5.36
1.250	4.12	2.750	74.20	4.250	5.77
1.333	4.12	2.833	74.20	4.333	5.83
1.417	4.12	2.917	107.17	4.417	5.92
1.500	4.12	3.000	107.17	4.500	5.92

Max.Eff.Inten.(mm/hr)= 107.17 73.77

over (min)= 5.00 25.00

Storage Coeff. (min)= 1.60 (ii) 24.13 (ii)

Unit Hyd. Tpeak (min)= 5.00 25.00

Unit Hyd. peak (cms)= .32 .05

\*TOTALS\*

PEAK FLOW (cms)= .05 .07 .092 (iii)

TIME TO PEAK (hrs)= 3.00 3.25 3.00

RUNOFF VOLUME (mm)= 67.70 46.97 50.90

TOTAL RAINFALL (mm)= 68.70 68.70 68.70

RUNOFF COEFFICIENT = .99 .68 .74

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%

YOU SHOULD CONSIDER SPLITTING THE AREA.

\*\*\*\*\* WARNING: CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:

(i) CN = 88.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0107)	Area (ha)	3.63	IMPERVIOUS	PERVIOUS (i)
ID= 1 DT= 5.0 min	Total Imp(%)	29.40	Dir. Conn. (%)	19.00

Surface Area (ha)= .107	.256
Dep. Storage (mm)= 1.00	3.00
Average Slope (%)= 2.00	3.00
Length (m)= 155.50	440.00
Mannings n = .013	.250

Max.Eff.Inten.(mm/hr)= 107.17 50.61  
 over (min)= 5.00 40.00  
 Storage Coeff. (min)= 2.63 (ii) 37.22 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 40.00  
 Unit Hyd. peak (cms)= .29 .03

\*TOTALS\*

PEAK FLOW (cms)= .20 .21 .286 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.50 3.00

RUNOFF VOLUME (mm)= 67.70 42.76 47.50

TOTAL RAINFALL (mm)= 68.70 68.70 68.70

RUNOFF COEFFICIENT = .99 .62 .69

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%

YOU SHOULD CONSIDER SPLITTING THE AREA.

Page 14

Pre-Dev-Uncon-SCS					
.67	4.58	2.17	9.16	3.67	7.78
.83	4.58	2.33	9.16	3.83	7.32
1.00	4.58	2.50	9.16	4.00	7.78
1.17	4.58	2.67	45.78	4.17	5.95
1.33	4.58	2.83	82.40	4.33	6.41
1.50	4.58	3.00	119.03	4.50	5.95

CALIB NASHYD (0105)	Area (ha)	4.82	Curve Number (CN)= 66.0
ID= 1 DT= 10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	U.H. Tp(hrs)= .35

unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .277 (i)

TIME TO PEAK (hrs)= 3.167

RUNOFF VOLUME (mm)= 25.070

TOTAL RAINFALL (mm)= 76.300

RUNOFF COEFFICIENT = .329

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB NASHYD (0112)	Area (ha)	1.40	Curve Number (CN)= 75.0
ID= 1 DT= 10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .134 (i)

TIME TO PEAK (hrs)= 3.000

RUNOFF VOLUME (mm)= 32.159

TOTAL RAINFALL (mm)= 76.300

RUNOFF COEFFICIENT = .421

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0105):	4.82	.277	3.17	25.07	
+ ID2= 2 (0112):	1.40	.134	3.00	32.16	

ID = 3 (0103): 6.22 .401 3.17 26.66

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha)	1.39	Curve Number (CN)= 84.0
ID= 1 DT= 10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00	U.H. Tp(hrs)= .24

unit Hyd Qpeak (cms)= .223

Page 16

Page 15

## Pre-Dev-Uncon-SCS

PEAK FLOW (cms)= .184 (i)  
 TIME TO PEAK (hrs)= 3.000  
 RUNOFF VOLUME (mm)= 42.727  
 TOTAL RAINFALL (mm)= 76.300  
 RUNOFF COEFFICIENT = .560

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Pre-Dev-Uncon-SCS  
 CN\* = 88.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	STANDHYD (0115)	Area (ha)= 33.83	Dir. Conn.(%)= 19.00
ID= 1 DT= 5.0 min		Total Imp(%)= 33.00	

Surface Area (ha)= .27	IMPERVIOUS .55
Dep. Storage (mm)= 1.00	PERVIOUS .00
Average Slope (%)= 1.00	
Length (m)= 74.30	275.00
Mannings n = .013	.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME hrs	RAIN mm hr <sup>-1</sup>	TIME hrs	RAIN mm hr <sup>-1</sup>	TIME hrs	RAIN mm hr <sup>-1</sup>	TIME hrs	RAIN mm hr <sup>-1</sup>
.083	3.20	1.383	7.78	3.083	16.94	4.58	4.58
.167	3.20	1.697	7.78	3.167	16.94	4.57	4.58
.250	3.75	1.750	7.32	3.250	16.48	4.75	4.58
.333	2.75	1.833	7.32	3.333	16.48	4.83	4.58
.417	3.20	1.917	7.78	3.417	16.94	4.92	4.58
.500	3.20	2.000	7.78	3.500	16.94	5.00	4.58
.583	4.58	2.083	9.16	3.583	7.78	5.08	3.20
.667	4.58	2.167	9.16	3.667	7.78	5.17	3.20
.750	4.58	2.250	9.16	3.750	7.32	5.25	2.75
.833	4.58	2.333	9.16	3.833	7.32	5.33	2.75
.917	4.58	2.417	9.16	3.917	7.32	5.42	3.20
1.000	4.58	2.500	9.16	4.000	7.78	5.50	3.20
1.083	4.58	2.583	45.78	4.183	5.95	5.58	3.20
1.167	4.58	2.667	45.78	4.267	5.95	5.67	3.20
1.250	4.58	2.750	82.40	4.250	6.41	5.75	2.75
1.333	4.58	2.833	82.40	4.333	6.41	5.83	2.75
1.417	4.58	2.917	119.03	4.417	5.95	5.92	3.20
1.500	4.58	3.000	119.03	4.500	5.95	6.00	3.20

Max.Eff.Inten.(mm/hr)= 119.03	84.71
over (min)= 5.00	25.00
Storage Coeff. (min)= 1.62 (ii)	22.85 (ii)
Unit Hyd. Tpeak (min)= 5.00	25.00
Unit Hyd. peak (cms)= .32	.05

\*TOTALS\*

PEAK FLOW (cms)= .05	.08	.106 (iii)
TIME TO PEAK (hrs)= 3.00	3.25	3.00
RUNOFF VOLUME (mm)= 75.30	53.94	57.98
TOTAL RAINFALL (mm)= 76.30	76.30	76.30
RUNOFF COEFFICIENT = .99	.71	.76

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 Page 17

CALIB	STANDHYD (0107)	Area (ha)= 3.63	Dir. Conn.(%)= 19.00
ID= 1 DT= 5.0 min		Total Imp(%)= 29.40	

Surface Area (ha)= 1.07	IMPERVIOUS .256
Dep. Storage (mm)= 1.00	PERVIOUS .300
Average Slope (%)= 2.00	
Length (m)= 155.50	440.00
Mannings n = .013	.250

Max.Eff.Inten.(mm/hr)= 119.03	58.72
over (min)= 5.00	40.00

Storage Coeff. (min)= 2.52 (ii)	35.12 (ii)
---------------------------------	------------

Unit Hyd. Tpeak (min)= 5.00	40.00
-----------------------------	-------

Unit Hyd. peak (cms)= .29	.03
---------------------------	-----

\*TOTALS\*

PEAK FLOW (cms)= .23	.25	.327 (iii)
TIME TO PEAK (hrs)= 3.00	3.50	3.00
RUNOFF VOLUME (mm)= 75.30	49.48	54.38
TOTAL RAINFALL (mm)= 76.30	76.30	76.30
RUNOFF COEFFICIENT = .99	.65	

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:

Page 17

ADD HYD (0114)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0115):		.83	.106	3.00	57.98
+ ID2= 2 (0107):		3.63	.327	3.00	54.38

ID = 3 (0114): 4.45 .433 3.00 55.05

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0102):		1.39	.184	3.00	42.73
+ ID2= 2 (0114):		4.45	.433	3.00	55.05

ID = 3 (0117): 5.85 .617 3.00 52.12

Page 18

## Pre-Dev-Uncon-SCS

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
		6.22	.401	3.17	26.66
+ ID1= 1 (0103):		5.85	.617	3.00	52.12

ID = 3 (0106): 12.07 .968 3.00 39.00

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
 \*\* SIMULATION NUMBER: 6 \*\*  
 \*\*\*\*\*

MASS STORM	Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst
Pttotal= 83.80 mm	Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Duration of storm = 6.00 hrs  
 Mass curve time step = 10.00 min

TIME hrs	RAIN mm hr <sup>-1</sup>						
.33	3.20	1.383	8.55	3.33	18.60	4.67	5.03
.50	3.52	2.00	8.55	3.50	18.60	5.00	5.03
.67	5.03	2.17	10.06	3.67	8.55	5.17	3.52
.83	5.03	2.33	10.06	3.83	8.04	5.33	3.02
1.00	5.03	2.50	10.06	4.00	8.55	5.50	3.52
1.17	5.03	2.67	50.28	4.17	6.54	5.67	3.52
1.33	5.03	2.83	90.50	4.33	7.04	5.83	3.02
1.50	5.03	3.00	130.73	4.50	6.54	6.00	3.52

CALIB	NASHYD (0105)	Area (ha)= 4.82	Curve Number (CN)= 66.0
ID= 1 DT=10.0 min		Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
		U.H. Tp(hrs)= .35	

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	NASHYD (0112)	Area (ha)= 1.40	Curve Number (CN)= 75.0
ID= 1 DT=10.0 min		Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
		U.H. Tp(hrs)= .24	

Page 19

## Pre-Dev-Uncon-SCS

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .157 (i)
TIME TO PEAK (hrs)= 3.000
RUNOFF VOLUME (mm)= 37.478
TOTAL RAINFALL (mm)= 83.800
RUNOFF COEFFICIENT = .447

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0105):		4.82	.327	3.17	29.53
+ ID2= 2 (0112):		1.40	.157	3.00	37.48

ID = 3 (0103): 6.22 .472 3.17 31.31

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	NASHYD (0102)	Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min		Ia (mm)= 4.00	# of Linear Res.(N)= 3.00
		U.H. Tp(hrs)= .24	

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .212 (i)
TIME TO PEAK (hrs)= 3.000
RUNOFF VOLUME (mm)= 49.006
TOTAL RAINFALL (mm)= 83.800
RUNOFF COEFFICIENT = .585

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	STANDHYD (0115)	Area (ha)= .83	Dir. Conn.(%)= 19.00
ID= 1 DT= 5.0 min		Total Imp(%)= 33.00	

Surface Area (ha)= .27	IMPERVIOUS .55
Dep. Storage (mm)= 1.00	PERVIOUS .200
Average Slope (%)= 2.00	
Length (m)= 74.30	275.00
Mannings n = .013	.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME hrs	RAIN mm/hr <sup>-1</sup>	TIME hrs	RAIN mm hr <sup>-1</sup>	TIME hrs	RAIN mm hr <sup>-1</sup>	TIME hrs	RAIN mm hr <sup>-1</sup>
.083	3.52	1.583	8.55	3.083	18.60	4.58	5.03
.167	3.52	1.667	8.55	3.167	8.55	3.167	18.60
.250	3.02	1.750	8.04	3.250	8.04	3.250	18.60

Page 20

Pre-Dev-Uncon-SCS						
.333	3.02	1.833	8.04	3.333	18.10	4.83
.417	3.52	1.917	8.55	3.417	18.60	4.92
.500	3.52	2.000	8.55	3.500	18.60	5.00
.583	5.03	2.083	10.06	3.583	8.52	5.08
.667	5.03	2.167	10.06	3.667	8.52	5.17
.750	5.03	2.250	10.06	3.750	8.04	5.25
.833	5.03	2.333	10.06	3.833	8.04	5.33
.917	5.03	2.417	10.06	3.917	8.55	5.42
1.000	5.03	2.500	10.06	4.000	8.55	5.50
1.083	5.03	2.583	50.28	4.083	6.54	5.58
1.167	5.03	2.667	50.28	4.167	6.54	5.67
1.250	5.03	2.750	90.50	4.250	7.04	5.75
1.333	5.03	2.833	90.50	4.333	7.04	5.83
1.417	5.03	2.917	130.73	4.417	6.54	5.92
1.500	5.03	3.000	130.73	4.500	6.54	3.52

Max.Eff.Inten.(mm/hr)= 130.73 109.46  
 over (min)= .00 20.00  
 Storage Coeff. (min)= 1.56 (ii) 20.72 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 25.00  
 Unit Hyd. peak (cms)= .33 .05

\*TOTALS\*

PEAK FLOW (cms)= .06 .10 .122 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.25 3.00  
 RUNOFF VOLUME (mm)= 82.80 60.90 65.05  
 TOTAL RAINFALL (mm)= 83.80 83.80 83.80  
 RUNOFF COEFFICIENT = .99 .73 .67

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 88.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Pre-Dev-Uncon-SCS  
 \*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 $CN^* = 86.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0114)		AREA	QPEAK	TPEAK	R.V.
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)
+ ID1= 1 (0115):		1.39	.212	3.00	65.05
+ ID2= 2 (0107):		3.63	.391	3.00	61.27
ID = 3 (0114):		4.45	.512	3.00	61.97

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0117)		AREA	QPEAK	TPEAK	R.V.
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)
+ ID1= 1 (0102):		1.39	.212	3.00	49.01
+ ID2= 2 (0114):		4.45	.512	3.00	61.97
ID = 3 (0117):		5.85	.724	3.00	58.88

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)		AREA	QPEAK	TPEAK	R.V.
1 +	2 = 3	(ha)	(cms)	(hrs)	(mm)
+ ID1= 1 (0103):		6.22	.472	3.17	31.31
+ ID2= 2 (0117):		5.85	.724	3.00	58.88
ID = 3 (0106):		12.07	1.140	3.00	44.67

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

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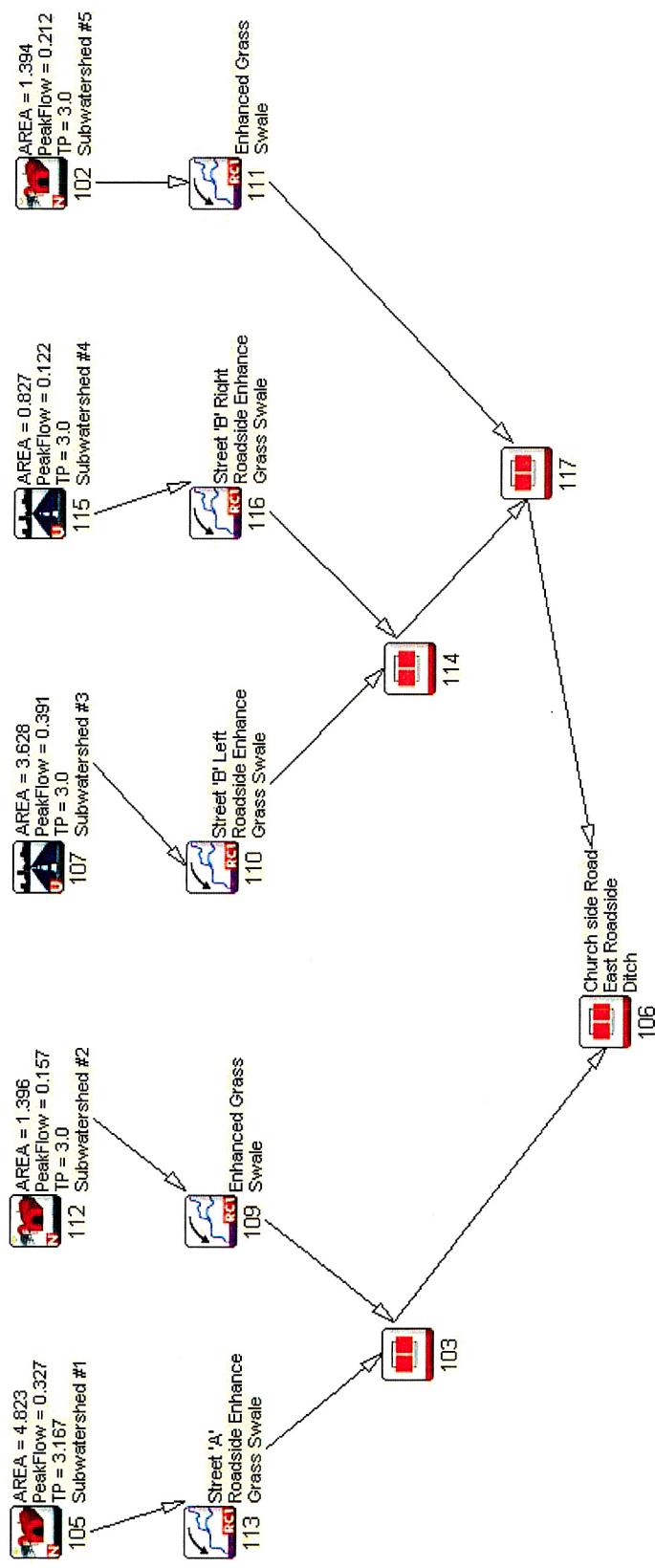
**APPENDIX IV**

**VISUAL OTTHYMO OUTPUT**

**POST DEVELOPMENT CONTROLLED**

---

2 Post-Dev Controlled



## Pre-Dev-Con-25mm

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V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U AAAA L
V V I SS U U A A L
VV I SSSSS UUUU A A LLLL

000 TTTT H H Y Y M M 000 TM, Version 2.0
0 0 T T H H Y Y M M 0 0 Licensed To: MJ Davenport
000 T T H H Y M M 000 vo2-0057

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual OTTHYMO v2.0\voin.dat

Output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Controlled.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Controlled.sum

DATE: 1/23/2019 TIME: 2:11:33 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 9 \*\*  
\*\*\*\*\*

CHICAGO STORM IDF curve parameters: A= 486.300  
Ptotal= 25.00 mm B= 7.500  
C= .790

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs  
Storm time step = 10.00 min  
Time to peak ratio = .38

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	1.66	1.17	6.41	2.17	4.73	3.17	2.05
.33	1.87	1.33	14.61	2.33	3.84	3.33	1.89
.50	2.16	1.50	50.69	2.50	3.25	3.50	1.75
.67	2.55	1.67	17.59	2.67	2.82	3.67	1.63
.83	3.16	1.83	9.15	2.83	2.50	3.83	1.53
1.00	4.20	2.00	6.21	3.00	2.25	4.00	1.44

Page 1

## Pre-Dev-Con-25mm

CALIB STANDHYD (0115)	Area (ha)= 3.83	Total Imp(%)= 33.00	Dir. Conn.(%)= 19.00
ID= 1 DT= 5.0 min	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)= .27		.55	
Dep. Storage (mm)= 1.00		2.00	
Average Slope (%)= 2.00		3.00	
Length (m)= 74.30		275.00	
Mannings n = .013		.250	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	1.66	1.083	6.41	2.083	4.73	3.08	2.05
.167	1.66	1.167	6.41	2.167	4.73	3.17	2.05
.250	1.87	1.250	14.61	2.250	3.84	3.25	1.89
.333	1.87	1.333	14.61	2.333	3.84	3.33	1.89
.417	2.16	1.417	50.69	2.417	3.25	3.42	1.75
.500	2.16	1.500	50.69	2.500	3.25	3.50	1.75
.583	2.51	1.583	17.59	2.583	2.82	3.58	1.63
.667	2.55	1.667	17.59	2.667	2.82	3.67	1.53
.750	3.16	1.750	9.15	2.750	2.50	3.75	1.53
.833	3.16	1.833	9.15	2.833	2.50	3.83	1.53
.917	4.20	1.917	6.21	2.917	2.25	3.92	1.44
1.000	4.20	2.000	6.21	3.000	2.25	4.00	1.44

Max.Eff.Inten.(mm/hr)= 50.69 10.32  
over (min)= 5.00 55.00  
Storage Coeff. (min)= 2.28 (ii) 51.57 (ii)  
Unit Hyd. Tpeak (min)= 5.00 55.00  
Unit Hyd. peak (cms)= .30 .02

\*TOTALS\*

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN\* = 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0116)	IN= 2--> OUT= 1	Routing time step (min)'= 5.00
------------------	-----------------	--------------------------------

<----- DATA FOR SECTION ( 1.1) ----->  
Distance Elevation Manning  
Page 2

Pre-Dev-Con-25mm  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

TRAVEL TIME TABLE							
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME	(m)	(m)
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)		
.03	215.03	675E+01	0	.13	10.24		
.06	215.09	150E+02	0	.21	10.61		
.09	215.15	248E+02	0	.29	14.23		
.13	215.13	360E+02	.1	.37	11.28		
.16	215.16	488E+02	.1	.44	9.41		
.19	215.19	630E+02	.1	.51	8.11		
.22	215.22	787E+02	.2	.58	7.15		
.25	215.25	960E+02	.2	.65	6.41		
.28	215.28	115E+03	.3	.72	5.83		
.32	215.32	135E+03	.4	.78	5.35		
.35	215.35	157E+03	.5	.84	4.95		
.38	215.38	180E+03	.6	.90	4.62		
.41	215.41	205E+03	.8	.96	4.33		
.44	215.44	231E+03	.9	1.02	4.09		
.47	215.47	258E+03	1.1	1.08	3.87		
.51	215.51	288E+03	1.3	1.13	3.68		
.54	215.54	318E+03	1.5	1.19	3.51		
.57	215.57	350E+03	1.7	1.24	3.35		
.60	215.60	384E+03	2.0	1.30	3.22		

<---- hydrograph ----> <-pipe / channel->  
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0115) .83 .02 1.50 13.01 .08 .48  
OUTFLOW: ID= 1 (0116) .83 .01 1.58 12.95 .06 .49

TRAVEL TIME TABLE							
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME	(m)	(m)
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)		
.03	215.03	947E+01	0	.15	38.53		
.06	215.06	210E+02	0	.25	23.36		
.09	215.09	347E+02	0	.34	17.30		
.13	215.13	504E+02	.1	.42	13.94		
.16	215.16	683E+02	.1	.50	11.77		
.19	215.19	882E+02	.1	.57	10.25		
.22	215.22	110E+03	.2	.64	9.11		
.25	215.25	134E+03	.3	.71	8.23		
.28	215.28	161E+03	.4	.78	7.53		
.32	215.32	190E+03	.5	.84	6.95		
.35	215.35	219E+03	.6	.90	6.47		
.38	215.38	252E+03	.7	.96	6.05		
.41	215.41	286E+03	.8	1.02	5.70		
.44	215.44	323E+03	1.0	1.08	5.39		
.47	215.47	362E+03	1.2	1.14	5.12		
.51	215.51	403E+03	1.4	1.20	4.88		
.54	215.54	446E+03	1.6	1.25	4.66		
.57	215.57	491E+03	1.8	1.30	4.47		
.60	215.60	.538E+03	2.1	1.36	4.30		

<---- hydrograph ----> <-pipe / channel->  
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0110) 3.63 .09 1.50 11.49 .16 .49  
OUTFLOW: ID= 1 (0110) 3.63 .06 1.58 11.48 .12 .41

ADD HYD (0114)	1 + 2 + 3	AREA	QPEAK	TPEAK	R.V.
ID1= 1 (0116):		(ha)	(cms)	(hrs)	(mm)
+ ID2= 2 (0110):					
ID = 3 (0114):					

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

Page 3

Page 4

## Pre-Dev-Con-25mm

CALIB	NASHYD	(0102)	Area (ha)=	1.39	Curve Number (CN)=	84.0
ID= 1	DT=10.0	min	Ia (mm)=	4.00	# of Linear Res.(N)=	3.00
U.H. Tp(hr(s))=.24						

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----									
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.167	1.66	1.167	6.41	2.167	4.73	3.17	2.05		
.333	1.87	1.333	14.61	2.333	3.84	3.33	1.89		
.500	2.16	1.500	50.69	2.500	3.25	3.50	1.75		
.667	2.55	1.667	17.59	2.667	2.82	3.67	1.63		
.833	3.16	1.833	9.15	2.833	2.50	3.83	1.53		
1.000	4.20	2.000	6.21	3.000	2.25	4.00	.00		

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .023 (i)  
TIME TO PEAK (hrs)= 1.667  
RUNOFF VOLUME (mm)= 6.146  
TOTAL RAINFALL (mm)= 24.755  
RUNOFF COEFFICIENT = .248

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

## Pre-Dev-Con-25mm

<---- hydrograph ---->				<-pipe / channel->		
AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)	
INFLOW : ID= 2 (0102)	1.39	.02	1.67	6.15	.07	
OUTFLOW : ID= 1 (0111)	1.39	.02	1.92	6.06	.06	

.31 .07 .31 .29

ADD HYD (0117)		1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0114):			4.45	.070	1.58	11.75
+ ID2= 2 (0111):			1.39	.019	1.92	6.06
ID = 3 (0117):			5.85	.076	1.58	10.40

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| ROUTE CHN (0111) | IN= 2 --> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1) ----->

Distance	Elevation	Manning
.00	215.60	.0500
3.00	215.00	.0500
3.76	215.00	.0500
5.56	215.60	.0000

Main Channel

TRAVEL TIME TABLE					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.701E+01	.0	.18	22.93
.06	215.06	.160E+02	.0	.29	14.14
.09	215.09	.270E+02	.0	.39	10.61
.13	215.13	.400E+02	.1	.48	8.65
.16	215.16	.550E+02	.1	.56	7.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.216E+03	.9	1.05	3.95
.41	215.41	.247E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.314E+03	1.6	1.23	3.38
.51	215.51	.351E+03	1.8	1.29	3.23
.54	215.54	.390E+03	2.1	1.35	3.09
.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

Page 5

<---- hydrograph ---->				<-pipe / channel->		
AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)	
INFLOW : ID= 1 (0114)	4.45	.070	1.58	11.75	.31	
OUTFLOW : ID= 2 (0111)	1.39	.019	1.92	6.06	.06	

ADD HYD (0117)		1 + 2 = 3	ROUTE CHN (0113)	IN= 2 --> OUT= 1   Routing time step (min)'= 5.00	
<---- DATA FOR SECTION ( 1.1) ----->			<---- DATA FOR SECTION ( 1.1) ----->		
Distance	Elevation	Manning	Distance	Elevation	
.00	215.60	.0500	1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel	4.36	215.60	.0500

TRAVEL TIME TABLE					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.541E+01	.0	.15	22.38
.06	215.06	.120E+02	.0	.25	13.54
.09	215.09	.198E+02	.0	.33	10.01
.13	215.13	.288E+02	.1	.41	8.05
.16	215.16	.390E+02	.1	.49	6.79
.19	215.19	.504E+02	.1	.56	5.91
.22	215.22	.630E+02	.2	.63	5.25
.25	215.25	.768E+02	.3	.70	4.74
.28	215.28	.917E+02	.4	.77	4.33
.32	215.32	.108E+03	.4	.83	4.00

Page 6

Pre-Dev-Con-25mm					
.35	215.35	.125E+03	.6	.90	3.72
.38	215.38	.144E+03	.7	.96	3.48
.41	215.41	.164E+03	.8	1.02	3.28
.44	215.44	.185E+03	1.0	1.08	3.10
.47	215.47	.207E+03	1.2	1.13	2.94
.51	215.51	.230E+03	1.4	1.19	2.80
.54	215.54	.255E+03	1.6	1.24	2.68
.57	215.57	.280E+03	1.8	1.30	2.57
.60	215.60	.307E+03	2.1	1.35	2.47

<---- hydrograph ---->

AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm) MAX DEPTH (m) MAX VEL (m/s)

INFLOW : ID= 2 (0105) 4.82 .02 1.83 2.58 .08 .28  
OUTFLOW : ID= 1 (0113) 4.82 .02 2.08 2.56 .08 .28

<---- hydrograph ---->				<-pipe / channel->		
AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)	
INFLOW : ID= 2 (0112)	1.40	.01	1.67	3.69	.04	
OUTFLOW : ID= 1 (0109)	1.40	.01	2.00	3.62	.03	

.208 .1.98 .1.89 .1.81 .1.74 .1.74

ADD HYD (0103)		1 + 2 = 3	ROUTE CHN (0112)	IN= 2 --> OUT= 1   Routing time step (min)'= 5.00	
<---- DATA FOR SECTION ( 1.1) ----->			<---- DATA FOR SECTION ( 1.1) ----->		
Distance	Elevation	Manning	Distance	Elevation	
.00	215.60	.0500	1.80	215.00	.0500 / .0500 Main Channel
3.80	215.00	.0500 / .0500 Main Channel	5.60	215.60	.0500

TRAVEL TIME TABLE					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.170E+02	.0	.23	8.87
.09	215.09	.266E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.464E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.857E+02	.4	.62	3.30
.28	215.28	.997E+02	.5	.68	3.03
.32	215.32	.114E+03	.7	.73	2.80
.35	215.35	.130E+03	.8	.78	2.61
.38	215.38	.146E+03	1.0	.84	2.45
.41	215.41	.163E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18

Page 7

FINISH

Page 8

Pre-Dev-Con-6hr-Chicago

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=====
V   V   I   SSSSS U   U   A   L
V   V   I   SS  U   U   A   A   L
V   V   I   SS  U   U   AAAAA L
V   V   I   SS  U   U   A   A   L
V   V   I   SSSSS UUUUU A   A   LLLL
=====
000   TTTT  TTTT  H   H   Y   Y   M   M   M   000   TM, Version 2.0
0   0   T   T   H   H   Y   Y   M   M   M   0   Licensed To: MJ Davenport
000   T   T   H   H   Y   M   M   000   vo2-0057

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual OTTHYMO v2.0\voin.dat

Output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Controlled.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Controlled.sum

DATE: 1/23/2019 TIME: 1:59:05 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 1 \*\*  
\*\*\*\*\*

CHICAGO STORM IDF curve parameters: A= 662.000  
Ptotal= 37.36 mm B= 7.500  
C= .790

used in: INTENSITY = A / (t + b)^c

Duration of storm = 6.00 hrs  
Storm time step = 10.00 min  
Time to peak ratio = .38

TIME hrs	RAIN mm/hr						
.17	1.48	1.67	4.30	3.17	5.23	4.67	2.08
.33	1.59	1.83	5.71	3.33	4.42	4.83	1.96
.50	1.71	2.00	8.73	3.50	3.84	5.00	1.86
.67	1.86	2.17	19.94	3.67	3.41	5.17	1.76
.83	2.04	2.33	69.00	3.83	3.41	5.25	1.68
1.00	2.26	2.417	23.94	3.917	3.41	5.33	1.61

Page 1

1.17	2.55	2.67	12.46	4.17	2.57	5.67	1.54				
1.33	2.94	2.83	8.46	4.33	2.38	5.83	1.48				
1.50	3.48	3.00	6.44	4.50	2.22	6.00	1.42				

CALIB STANDHYD (0115)	Area (ha)=	.83
ID= 1 DT= 5.0 min	Total Imp(%)=	33.00
	Dir. Conn.(%)=	19.00

Surface Area (ha)=	.27	.55
Dep. Storage (mm)=	1.00	2.00
Average Slope (%)=	2.00	3.00
Length (m)=	74.30	275.00
Mannings n =	.013	.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083	1.48	1.583	4.30	3.083	5.23
.167	1.48	1.667	4.30	3.167	5.23
.250	1.59	1.750	5.71	3.250	4.42
.333	1.59	1.833	5.71	3.333	4.42
.417	1.71	1.917	8.73	3.417	4.83
.500	1.71	2.000	8.73	3.500	5.00
.583	1.86	2.083	19.90	3.583	5.08
.667	1.86	2.167	19.90	3.667	5.17
.750	2.04	2.250	69.00	3.750	5.25
.833	2.04	2.333	69.00	3.833	5.33
.917	2.26	2.417	23.94	3.917	5.42
1.000	2.26	2.500	23.94	4.000	5.50
1.083	2.55	2.583	12.46	4.083	5.57
1.167	2.55	2.667	12.46	4.167	5.67
1.250	2.91	2.750	8.46	4.250	5.75
1.333	2.94	2.833	8.46	4.333	5.83
1.417	3.48	3.917	6.46	4.417	5.92
1.500	3.48	3.000	6.44	4.500	6.00

Max.Eff.Inten.(mm/hr)=	69.00	20.78
over (min)=	5.00	40.00
Storage Coeff. (min)=	2.01 (ii)	39.27 (ii)
Unit Hyd. Tpeak (min)=	5.00	40.00
Unit Hyd. peak (cms)=	.31	.03

*TOTALS*
PEAK FLOW (cms)= .03
TIME TO PEAK (hrs)= 2.33
RUNOFF VOLUME (mm)= 26.36
TOTAL RAINFALL (mm)= 37.36
RUNOFF COEFFICIENT = .97

.03 (iii)  
2.33  
26.36  
37.36

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN<sup>n</sup> = 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.

Page 2

Pre-Dev-Con-6hr-Chicago  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0116) | Routing time step (min)'= 5.00

<--> DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.676E+01	.0	.13	33.24
.06	215.06	.150E+02	.0	.21	19.61
.09	215.09	.240E+02	.0	.29	11.23
.13	215.13	.360E+02	.1	.37	11.28
.16	215.16	.488E+02	.1	.44	9.41
.19	215.19	.630E+02	.1	.51	8.11
.22	215.22	.787E+02	.2	.58	7.15
.25	215.25	.960E+02	.2	.65	6.41
.28	215.28	.115E+03	.3	.72	5.83
.32	215.32	.135E+03	.4	.78	5.35
.35	215.35	.157E+03	.5	.84	4.95
.38	215.38	.180E+03	.6	.90	4.62
.41	215.41	.205E+03	.8	.96	4.33
.44	215.44	.230E+03	1.02	.49	4.09
.47	215.47	.258E+03	1.1	.08	3.87
.51	215.51	.288E+03	1.2	1.13	3.68
.54	215.54	.318E+03	1.5	1.19	3.51
.57	215.57	.350E+03	1.7	1.24	3.35
.60	215.60	.384E+03	2.0	1.30	3.22

<--> hydrograph -----> <-pipe / channel->  
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (cms) (hrs) (mm) (m) (m/s)  
INFLOW : ID= 2 (0115) .83 .03 2.33 22.93 .10 .31  
OUTFLOW: ID= 1 (0116) .83 .02 3.08 22.84 .08 .25

Pre-Dev-Con-6hr-Chicago					
PEAK FLOW (cms)=	.13	.05	.133	(iii)	
TIME TO PEAK (hrs)=	2.33	3.42	2.33		
RUNOFF VOLUME (mm)=	36.36	17.06	20.72		
TOTAL RAINFALL (mm)=	37.36	37.36	37.36		
RUNOFF COEFFICIENT =	.97	.46	.55		

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN<sup>n</sup> = 86.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0110) | IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

<--> DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.92E+01	.0	.15	38.93
.06	215.06	.210E+02	.0	.25	23.36
.09	215.09	.347E+02	.0	.34	17.30
.13	215.13	.504E+02	.1	.42	13.94
.16	215.16	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23
.28	215.28	.161E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.247E+03	.7	.96	6.05
.41	215.41	.286E+03	.8	1.02	5.70
.44	215.44	.323E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.403E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

<--> hydrograph -----> <-pipe / channel->  
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (cms) (hrs) (mm) (m) (m/s)  
INFLOW : ID= 2 (0110) .363 .13 2.23 20.72 .18 .35  
OUTFLOW: ID= 1 (0110) .363 .09 2.42 20.70 .15 .47

ADD HYD (0114)	1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
					Page 4

Page 3

Pre-Dev-Con-6hr-Chicago  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0116): .83 .021 3.08 22.84  
 + ID2= 2 (0110): 3.63 .088 2.42 20.70  
 ID = 3 (0114): 4.45 .108 2.42 21.10

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
 ID= 1 DT=10.0 min | Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.167	1.48	1.667	4.30	3.167	5.23	4.67	2.08
.333	1.59	1.833	5.71	3.333	4.42	4.83	1.96
.500	1.71	2.000	8.73	3.500	3.84	5.00	1.86
.667	1.86	2.167	19.90	3.667	3.41	5.17	1.76
.833	2.04	2.333	69.00	3.833	3.07	5.33	1.68
1.000	2.26	2.500	23.94	4.000	2.77	5.50	1.61
1.167	2.55	2.667	12.46	4.167	2.57	5.67	1.54
.333	2.94	2.833	8.46	4.333	2.38	5.83	1.48
1.500	3.48	3.000	6.44	4.500	2.22	6.00	1.42

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .048 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 13.432  
 TOTAL RAINFALL (mm)= 37.363  
 RUNOFF COEFFICIENT = .359

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0111) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 3.00 215.00 .0500 Main Channel  
 .76 215.00 .0500  
 5.36 215.60 .0000

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .701E+01 .0 .18 22.93  
 .06 215.06 .120E+02 .0 .25 13.54  
 .09 215.09 .198E+02 .0 .33 10.01  
 .13 215.13 .288E+02 .1 .41 8.05  
 .16 215.16 .390E+02 .1 .49 6.79  
 .19 215.19 .504E+02 .1 .56 5.91  
 .22 215.22 .630E+02 .2 .63 5.25  
 .25 215.25 .768E+02 .3 .70 4.74  
 .28 215.28 .917E+02 .4 .77 4.33  
 .32 215.32 .108E+03 .4 .83 4.00  
 .35 215.35 .125E+03 .6 .90 3.72  
 .38 215.38 .144E+03 .7 .96 3.48  
 .41 215.41 .164E+03 .8 1.02 3.28  
 .44 215.44 .185E+03 1.0 1.08 3.10  
 .47 215.47 .207E+03 1.2 1.13 2.94  
 .51 215.51 .230E+03 1.4 1.19 2.80  
 .54 215.54 .255E+03 1.6 1.24 2.68  
 .57 215.57 .280E+03 1.8 1.30 2.57  
 .60 215.60 .307E+03 2.1 1.35 2.47

Page 5

Pre-Dev-Con-6hr-Chicago  
 (ha) (cms) (hrs) (mm)  
 .25 215.25 .112E+03 .4 .79 5.27  
 .28 215.28 .135E+03 .5 .86 4.85  
 .32 215.32 .160E+03 .6 .93 4.50  
 .35 215.35 .187E+03 .7 .99 4.21  
 .38 215.38 .215E+03 .9 1.05 3.95  
 .41 215.41 .245E+03 1.1 1.12 3.74  
 .44 215.44 .280E+03 1.3 1.17 3.55  
 .47 215.47 .314E+03 1.6 1.23 3.38  
 .51 215.51 .351E+03 1.8 1.29 3.23  
 .54 215.54 .390E+03 2.1 1.35 3.09  
 .57 215.57 .431E+03 2.4 1.40 2.97  
 .60 215.60 .474E+03 2.8 1.46 2.86

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0102) 1.39 .05 2.50 13.43 .10 .40  
 OUTFLOW: ID= 1 (0111) 1.39 .04 2.67 13.36 .09 .39

| ADD HYD (0117) |  
 1 + 2 = 3 |  
 AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0114): 4.45 .108 2.42 21.10  
 + ID2= 2 (0111): 1.39 .041 2.67 13.36  
 ID = 3 (0117): 5.85 .129 2.42 19.25

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
 ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .057 (i)  
 TIME TO PEAK (hrs)= 2.667  
 RUNOFF VOLUME (mm)= 6.397  
 TOTAL RAINFALL (mm)= 37.363  
 RUNOFF COEFFICIENT = .171

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0113) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 Page 6

Pre-Dev-Con-6hr-Chicago  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .541E+01 .0 .15 22.38  
 .06 215.06 .120E+02 .0 .25 13.54  
 .09 215.09 .198E+02 .0 .33 10.01  
 .13 215.13 .288E+02 .1 .41 8.05  
 .16 215.16 .390E+02 .1 .49 6.79  
 .19 215.19 .504E+02 .1 .56 5.91  
 .22 215.22 .630E+02 .2 .63 5.25  
 .25 215.25 .768E+02 .3 .70 4.74  
 .28 215.28 .917E+02 .4 .77 4.33  
 .32 215.32 .108E+03 .4 .83 4.00  
 .35 215.35 .125E+03 .6 .90 3.72  
 .38 215.38 .144E+03 .7 .96 3.48  
 .41 215.41 .164E+03 .8 1.02 3.28  
 .44 215.44 .185E+03 1.0 1.08 3.10  
 .47 215.47 .207E+03 1.2 1.13 2.94  
 .51 215.51 .230E+03 1.4 1.19 2.80  
 .54 215.54 .255E+03 1.6 1.24 2.68  
 .57 215.57 .280E+03 1.8 1.30 2.57  
 .60 215.60 .307E+03 2.1 1.35 2.47

INFLOW : ID= 2 (0105) 4.82 .06 2.67 6.40 .12 .40  
 OUTFLOW: ID= 1 (0113) 4.82 .05 2.83 6.37 .12 .39

Pre-Dev-Con-6hr-Chicago  
 (ha) (cms) (hrs) (mm)  
 .09 215.09 .266E+02 .1 .31 6.68  
 .13 215.13 .369E+02 .1 .38 5.45  
 .16 215.16 .480E+02 .2 .44 4.64  
 .19 215.19 .598E+02 .2 .50 4.07  
 .22 215.22 .724E+02 .3 .56 3.64  
 .25 215.25 .857E+02 .4 .62 3.30  
 .28 215.28 .997E+02 .5 .68 3.03  
 .32 215.32 .114E+03 .6 .73 2.80  
 .35 215.35 .130E+03 .7 .78 2.61  
 .38 215.38 .146E+03 1.0 .84 2.45  
 .41 215.41 .163E+03 1.2 .89 2.31  
 .44 215.44 .181E+03 1.4 .94 2.18  
 .47 215.47 .199E+03 1.6 .99 2.08  
 .51 215.51 .218E+03 1.8 1.04 1.98  
 .54 215.54 .238E+03 2.1 1.08 1.89  
 .57 215.57 .259E+03 2.4 1.13 1.81  
 .60 215.60 .280E+03 2.7 1.18 1.74

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0112) 1.40 .03 2.50 8.83 .06 .22  
 OUTFLOW: ID= 1 (0109) 1.40 .03 2.67 8.77 .05 .20

| ADD HYD (0103) |  
 1 + 2 = 3 |  
 AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0113): 4.82 .054 2.83 6.57  
 + ID2= 2 (0109): 1.40 .025 2.67 8.77  
 ID = 3 (0103): 6.22 .079 2.75 6.91

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| ADD HYD (0106) |  
 1 + 2 = 3 |  
 AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0117): 5.85 .129 2.42 19.25  
 + ID2= 2 (0103): 6.22 .079 2.75 6.91  
 ID = 3 (0106): 12.07 .190 2.67 12.89

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
 \*\* SIMULATION NUMBER: 2 \*\*  
 \*\*\*\*\*

| CHICAGO STORM | IDF curve parameters: A=1098.000  
 Pttotal= 48.64 mm | B= 10.100  
 C= .830  
 used in: INTENSITY = A / (t + B)^AC  
 duration of storm = 6.00 hrs  
 Page 8

| ROUTE CHN (0109) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 3.80 215.00 .0500 / .0500 Main Channel  
 5.60 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .813E+01 .0 .14 14.28  
 .06 215.06 .170E+02 .0 .23 8.87

Page 7

Pre-Dev-Con-6hr-Chicago  
Storm time step = 10.0 min  
Time to peak ratio = .38

TIME hrs	RAIN mm/hr						
.15	1.65	1.67	5.38	3.47	6.69	4.67	2.40
.33	1.78	1.63	7.98	3.33	5.55	4.83	2.25
.50	1.93	2.00	11.78	4.74	5.00	5.67	2.12
.67	2.12	2.17	28.11	3.67	4.15	5.17	2.00
.83	2.35	2.33	90.98	3.83	3.69	5.33	1.90
1.00	2.63	2.50	33.98	4.00	3.33	5.50	1.80
1.17	3.01	2.67	17.30	4.17	3.03	5.67	1.72
1.33	3.51	2.83	11.37	4.33	2.79	5.83	1.64
1.50	4.24	3.00	8.43	4.50	2.58	6.00	1.58

TOTAL RAINFALL (mm)= 48.64 48.64 48.64  
RUNOFF COEFFICIENT = .98 .60 .67

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
 $CN^2 = 88.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD (0115)	Area (ha)=	.83
ID= 1 DT= 5.0 min	Total Imp(%)=	33.00
	Dir. Conn.(%)=	19.00
	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.27	.55
Dep. Storage (mm)=	1.00	2.00
Average Slope (%)=	2.00	3.00
Length (m)=	74.30	275.00
Mannings n =	.013	.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.083	1.65	1.583	5.38	3.083	6.69	4.58	2.40
.167	1.65	1.667	5.38	3.167	6.69	4.67	2.40
.250	1.78	1.750	7.38	3.250	5.52	4.75	2.25
.33	1.78	1.833	7.38	3.333	5.52	4.83	2.25
.417	1.83	1.917	11.78	3.417	4.74	5.92	2.12
.500	1.93	2.000	11.78	3.500	4.74	5.00	2.12
.583	2.12	2.083	28.11	3.583	4.15	5.08	2.00
.667	2.12	2.167	28.11	3.667	4.15	5.17	2.00
.750	2.35	2.250	90.98	3.750	3.69	5.25	1.90
.833	2.35	2.333	90.98	3.833	3.69	5.33	1.90
.917	2.63	2.417	33.98	3.917	3.33	5.42	1.80
1.000	2.63	2.500	33.98	4.000	3.33	5.50	1.80
1.083	3.01	2.583	17.30	4.083	3.03	5.58	1.72
1.167	3.01	2.667	17.30	4.167	3.03	5.67	1.72
1.250	3.17	2.750	11.37	4.250	2.73	5.75	1.64
1.333	3.51	2.833	11.37	4.333	2.79	5.83	1.64
1.417	4.24	2.917	8.43	4.417	2.58	5.92	1.58
1.500	4.24	3.000	8.43	4.500	2.58	6.00	1.58

Max.Eff.Inten.(mm/hr)= 90.98 38.59  
over (min)= 5.00 35.00  
Storage Coeff. (min)= 1.80 (ii) 30.88 (ii)  
Unit Hyd. Tpeak (min)= 5.00 35.00  
Unit Hyd. peak (cms)= .32 .04  
PEAK FLOW (cms)= .04 .04 .04 .048 (iii)  
TIME TO PEAK (hrs)= 2.33 2.83 2.33 2.33  
RUNOFF VOLUME (mm)= 47.64 29.19 32.68

Page 9

| ROUTE CHN (0116) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cm³)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	6.67E+01	.0	.15	38.53
.06	215.06	9.70E+02	.0	.25	38.36
.09	215.09	3.47E+02	.0	.34	17.30
.13	215.13	.504E+02	.1	.42	13.94
.16	215.16	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23
.28	215.28	.161E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.249E+03	.7	.96	6.05
.41	215.41	.286E+03	.8	1.02	5.70
.44	215.44	.323E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.403E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

<---- hydrograph ----> <-pipe / channel->  
AREA (ha)= 0.83 QPEAK (cms)= 0.05 TPEAK (hrs)= 2.33 R.V. (mm)= 32.68 MAX DEPTH (m)= .21 MAX VEL (m/s)= .62  
INFLOW: ID= 2 (0115) .83 .05 2.33 32.68  
OUTFLOW: ID= 1 (0116) .83 .04 2.92 32.55 .12 .35

| CALIB STANDHYD (0107) | Area (ha)= 3.63  
| ID= 1 DT= 5.0 min | Total Imp(%)= 29.40 Dir. Conn.(%)= 19.00  
| IMPERVIOUS PERVIOUS (i)  
Surface Area (ha)= 1.07 2.56

Page 10

Pre-Dev-Con-6hr-Chicago  
Dep. Storage (mm)= 1.00 3.00  
Average Slope (%)= 2.00 3.00  
Length (m)= 155.50 440.00  
Mannings n = .013 .250  
Max.Eff.Inten.(mm/hr)= 90.98 23.44  
over (min)= 5.00 50.00  
Storage Coeff. (min)= 2.81 (ii) 49.87 (ii)  
Unit Hyd. Tpeak (min)= 5.00 50.00  
Unit Hyd. peak (cms)= .28 .02  
PEAK FLOW (cms)= .17 .10 .185 (iii)  
TIME TO PEAK (hrs)= 2.33 3.17 2.33 2.33  
RUNOFF VOLUME (mm)= 47.64 25.82 29.96  
TOTAL RAINFALL (mm)= 48.64 48.64 48.64  
RUNOFF COEFFICIENT = .98 .53 .62

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:  
 $CN^2 = 86.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0110)	IN= 2--> OUT= 1	Routing time step (min)'= 5.00
<---- DATA FOR SECTION ( 1.1 ) ----->		
Distance Elevation Manning .00 215.60 .0500 1.80 215.00 .0500 / .0500 Main Channel 2.56 215.00 .0500 / .0500 Main Channel 4.36 215.60 .0500		
<----- TRAVEL TIME TABLE ----->		
DEPTH (m) TIME hrs RAIN mm/hr TIME hrs RAIN mm/hr TIME hrs RAIN mm/hr .03 215.03 9.47E+01 .0 .15 38.53 .06 215.06 2.10E+02 .0 .25 38.36 .09 215.09 3.47E+02 .0 .34 17.30 .13 215.13 .504E+02 .1 .42 13.94 .16 215.16 .683E+02 .1 .50 11.77 .19 215.19 .882E+02 .1 .57 10.25 .22 215.22 .110E+03 .2 .64 9.11 .25 215.25 .134E+03 .3 .71 8.23 .28 215.28 .161E+03 .4 .78 7.53 .32 215.32 .189E+03 .5 .84 6.95 .35 215.35 .219E+03 .6 .90 6.47 .38 215.38 .249E+03 .7 .96 6.05 .41 215.41 .286E+03 .8 1.02 5.70 .44 215.44 .323E+03 1.0 1.08 5.39 .47 215.47 .362E+03 1.2 1.14 5.12 .51 215.51 .403E+03 1.4 1.20 4.88 .54 215.54 .446E+03 1.6 1.25 4.66 .57 215.57 .491E+03 1.8 1.30 4.47 .60 215.60 .538E+03 2.1 1.36 4.30		
<---- hydrograph ----> <-pipe / channel-> Page 11		

| ADD HYD (0114) | 1 + 2 = 3 | AREA (ha)= 1.39 Curve Number (CN)= 84.0  
| ID1= 1 (0116): .83 QPEAK (cms)= .038 TPEAK (hrs)= 2.92 R.V. (mm)= 32.55  
+ ID2= 2 (0110): 3.63 .130 2.42 29.93  
===== ID = 3 (0114): 4.45 .162 2.42 30.42

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB NASHYD (0102) | Area (ha)= 1.39 # of Linear Res.(N)= 3.00  
| ID= 1 DT=10.0 min | Ia (mm)= 4.00 U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.167	1.65	1.667	5.38	3.167	6.69	4.67	2.40
.33	1.78	1.833	7.38	3.333	5.55	4.83	2.25
.50	1.93	2.000	11.78	3.500	4.74	5.00	2.12
.67	2.12	2.167	28.11	3.667	4.15	5.17	2.00
.83	2.35	2.333	90.98	3.833	3.69	5.33	1.90
.100	2.63	2.500	33.98	4.000	3.33	5.50	1.80
.117	3.01	2.667	17.30	4.167	3.03	5.67	1.72
.133	3.51	2.833	11.37	4.333	2.79	5.83	1.64
.150	4.24	3.000	8.43	4.500	2.58	6.00	1.58

Unit Hyd peak (cms)= .223

PEAK FLOW (cms)= .081 (i)  
TIME TO PEAK (hrs)= 2.500  
RUNOFF VOLUME (mm)= 21.135  
TOTAL RAINFALL (mm)= 48.645  
RUNOFF COEFFICIENT = .434

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0111) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance Elevation Manning  
.00 215.60 .0500  
3.00 215.00 .0500  
3.76 215.00 .0500  
5.56 215.60 .0500

Page 12

Pre-Dev-Con-6hr-Chicago

TRAVEL TIME TABLE					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.704E+01	.0	.18	22.93
.06	215.06	.160E+02	.0	.29	10.14
.09	215.09	.470E+02	.0	.39	10.61
.13	215.13	.400E+02	.1	.48	8.65
.16	215.16	.550E+02	.1	.56	7.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.216E+03	.9	1.05	3.95
.41	215.41	.245E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.314E+03	1.6	1.23	3.38
.51	215.51	.351E+03	1.8	1.29	3.23
.54	215.54	.390E+03	2.1	1.35	3.09
.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

<---- hydrograph ----> <--pipe / channel-->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
1.39	.08	2.50	21.13	.13	.49
INFLOW : ID= 2 (0102)					
OUTFLOW: ID= 1 (0111)	1.39	.07	2.67	21.06	.12
					.47

INFLOW : ID= 2 (0102) 1.39 .08 2.50 21.13 .13 .49  
OUTFLOW: ID= 1 (0111) 1.39 .07 2.67 21.06 .12 .47

Pre-Dev-Con-6hr-Chicago

| ROUTE CHN (0113) | IN= 2---> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
0.0 215.00 .0500 / .0500 Main Channel  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

<---- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.541E+01	.0	.15	22.38
.06	215.06	.120E+02	.0	.25	13.54
.09	215.09	.198E+02	.0	.33	10.01
.13	215.13	.280E+02	.1	.41	8.95
.16	215.16	.390E+02	.1	.49	6.79
.19	215.19	.504E+02	.1	.56	5.91
.22	215.22	.630E+02	.2	.63	5.25
.25	215.25	.768E+02	.3	.70	4.74
.28	215.28	.917E+02	.4	.77	4.33
.32	215.32	.108E+03	.4	.83	4.00
.35	215.35	.125E+03	.6	.90	3.72
.38	215.38	.144E+03	.7	.96	3.48
.41	215.41	.164E+03	.8	1.02	3.28
.44	215.44	.185E+03	1.0	1.08	3.10
.47	215.47	.207E+03	1.2	1.13	2.94
.51	215.51	.230E+03	1.4	1.19	2.80
.54	215.54	.255E+03	1.6	1.24	2.68
.57	215.57	.280E+03	1.8	1.30	2.57
.60	215.60	.307E+03	2.1	1.35	2.47

<---- hydrograph ----> <--pipe / channel-->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
4.82	.11	2.67	10.88	.16	.50
INFLOW : ID= 2 (0105)	4.82	.11	2.67	10.88	.16
OUTFLOW: ID= 1 (0113)	4.82	.10	2.75	10.86	.16
					.50

INFLOW : ID= 2 (0105) 4.82 .11 2.67 10.88 .16 .50  
OUTFLOW: ID= 1 (0113) 4.82 .10 2.75 10.86 .16 .50

ADD HYD (0117)  
| 1 + 2 = 3 | AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
+ ID1= 1 (0114): 4.45 .162 2.42 30.42  
+ ID2= 2 (0111): 1.39 .072 2.67 21.06  
ID = 3 (0117): 5.85 .207 2.50 28.19

CALIB NASHYD (0105) Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .35

Unit Hyd Qpeak (cms)= .522  
PEAK FLOW (cms)= .106 (i)  
TIME TO PEAK (hrs)= 2.667  
RUNOFF VOLUME (mm)= 10.883  
TOTAL RAINFALL (mm)= 48.645  
RUNOFF COEFFICIENT = .224

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 13

Pre-Dev-Con-6hr-Chicago  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
3.80 215.00 .0500 Main Channel  
5.60 215.60 .0500

TRAVEL TIME TABLE					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.170E+02	.0	.23	8.87
.09	215.09	.266E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.857E+02	.4	.62	3.30
.28	215.28	.997E+02	.5	.68	3.03
.32	215.32	.114E+03	.7	.73	2.80
.35	215.35	.130E+03	.8	.78	2.61
.38	215.38	.146E+03	1.0	.84	2.45
.41	215.41	.163E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18
.47	215.47	.199E+03	1.6	.99	2.08
.51	215.51	.218E+03	1.8	1.04	1.98
.54	215.54	.238E+03	2.1	1.08	1.89
.57	215.57	.259E+03	2.4	1.13	1.81
.60	215.60	.280E+03	2.7	1.18	1.74

<---- hydrograph ----> <--pipe / channel-->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
1.40	.05	2.50	14.65	.08	.97
INFLOW : ID= 2 (0112)					
OUTFLOW: ID= 1 (0109)	1.40	.05	2.67	14.59	.08
					.97

ADD HYD (0103)  
| 1 + 2 = 3 | AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
+ ID1= 1 (0113): 4.82 .102 2.75 10.86  
+ ID2= 2 (0109): 1.40 .049 2.67 14.59  
ID = 3 (0103): 6.22 .148 2.75 11.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Pre-Dev-Con-6hr-Chicago

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 3 \*\*  
\*\*\*\*\*

| CHICAGO STORM mm | IDF curve parameters: A=1560.000  
Ptotal= 57.49 mm | B= 13.000  
C= .860

used in: INTENSITY = A / (t + B)\*C

DURATION OF STORM = 6.00 hrs

STORM TIME STEP = 10.00 min

TIME TO PEAK RATIO = .38

TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.17	1.73	1.67	6.29	3.17	7.97
.33	1.88	1.83	8.87	3.33	6.53
.50	2.06	2.00	14.61	3.50	5.48
.67	2.24	2.17	35.39	3.67	5.00
.83	2.54	2.43	10.21	3.83	5.33
1.00	2.88	2.50	42.69	4.00	3.72
1.17	3.33	2.67	21.79	4.17	3.36
1.33	3.95	2.83	14.08	4.33	3.06
1.50	4.85	3.00	10.23	4.50	2.81

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TRANSFORMED HYETOGRAPH					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.083	1.73	1.583	6.29	3.083	7.97
.167	1.73	1.667	6.29	3.167	7.97
.250	1.88	1.750	8.87	3.250	6.51
.333	1.88	1.833	8.87	3.333	6.51
.417	2.06	1.917	14.61	3.417	4.92
.583	2.27	2.083	35.36	3.583	4.74
.667	2.47	2.167	35.36	3.667	4.74
.750	2.54	2.240	103.20	4.75	5.25
.833	2.54	2.333	105.21	3.833	4.17
.917	2.88	2.417	42.69	3.917	3.72
1.000	2.88	2.500	42.69	4.000	3.72
1.083	3.33	2.583	21.79	4.083	3.36
1.167	3.33	2.667	21.79	4.167	3.36
1.250	3.95	2.750	14.08	4.250	3.06
1.333	3.95	2.833	14.08	4.333	3.06
1.417	4.85	2.917	10.23	4.417	2.81

Page 16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 15

1.500 4.85 | Pre-Dev-Con-6hr-Chicago  
 3.000 10.23 | 4.500 2.81 | 6.00 1.64

Max.Eff.Inten.(mm/hr)= 105.21 49.44  
 over (.min)= 5.00 30.00  
 Storage Coeff. (.min)= 1.70 (ii) 28.04 (ii)  
 Unit Hyd. Tpeak (.min)= 5.00 30.00  
 Unit Hyd. peak (cms)= .32 .04  
 \*TOTALS\*  
 PEAK FLOW (cms)= .05 .05 .060 (iii)  
 TIME TO PEAK (hrs)= 2.33 2.75 2.33  
 RUNOFF VOLUME (mm)= 56.49 36.90 40.60  
 TOTAL RAINFALL (mm)= 57.49 57.49 57.49  
 RUNOFF COEFFICIENT = .98 .64 .71

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 $CN^* = 88.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0116) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1) ----->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

TRAVEL TIME TABLE					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	676E+01	0	.13	33.24
.06	215.06	150E+02	.0	.21	19.61
.09	215.09	248E+02	.0	.29	14.23
.13	215.13	360E+02	.1	.37	11.28
.16	215.16	488E+02	.1	.44	9.41
.19	215.19	630E+02	.1	.51	8.11
.22	215.22	787E+02	.2	.58	7.15
.25	215.25	.960E+02	.2	.65	6.41
.28	215.28	1.15E+03	.3	.72	5.83
.32	215.32	1.35E+03	.4	.78	5.35
.35	215.35	1.57E+03	.5	.84	4.95
.38	215.38	1.80E+03	.6	.90	4.62
.41	215.41	2.05E+03	.8	.96	4.33
.44	215.44	2.31E+03	.9	1.02	4.09
.47	215.47	2.58E+03	1.1	1.08	3.87
.51	215.51	2.88E+03	1.3	1.13	3.68
.54	215.54	3.18E+03	1.5	1.19	3.51
.57	215.57	3.50E+03	1.7	1.24	3.35
.60	215.60	3.84E+03	2.0	1.30	3.22

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPKEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0115) .83 .06 2.33 40.60 .13 .38

Page 17

OUTFLOW: ID= 1 (0116) .83 .05 2.83 40.46 .13 .37

CALIB STANDHYD (0107) | Area (ha)= 3.63  
 ID= 1 DT= 5.0 min | Total Imp(%)= 29.40 Dir. Conn.(%)= 19.00

IMPERVIOUS PERVIOUS (i)  
 Surface Area (ha)= 1.07 2.56  
 Dep. Storage (mm)= 1.00 3.00  
 Average Slope (%)= 2.00 3.00  
 Length (m)= 155.50 440.00  
 Manning's n = .013 .250

Max.Eff.Inten.(mm/hr)= 105.21 35.48  
 over (.min)= 5.00 45.00  
 Storage Coeff. (.min)= 2.65 (ii) 42.52 (ii)  
 Unit Hyd. Tpeak (.min)= 5.00 45.00  
 Unit Hyd. peak (cms)= .29 .03

\*TOTALS\*  
 PEAK FLOW (cms)= .20 .14 .223 (iii)  
 TIME TO PEAK (hrs)= 2.33 3.00 2.33  
 RUNOFF VOLUME (mm)= 56.49 33.12 37.56  
 TOTAL RAINFALL (mm)= 57.49 57.49 57.49  
 RUNOFF COEFFICIENT = .98 .58 .65

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 $CN^* = 86.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0110) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1) ----->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

TRAVEL TIME TABLE					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	947E+01	0	.15	38.53
.06	215.06	210E+02	.0	.25	23.36
.09	215.09	347E+02	.0	.34	17.30
.13	215.13	504E+02	.1	.42	13.94
.16	215.16	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	1.10E+03	.2	.64	9.11
.25	215.25	1.34E+03	.3	.71	8.23
.28	215.28	1.61E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95

Page 18

### Pre-Dev-Con-6hr-Chicago

.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.252E+03	.7	.96	6.05
.41	215.41	.286E+03	.8	1.02	5.70
.44	215.44	.323E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.403E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPKEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0115) 3.63 .22 2.33 37.56 .23 .66

OUTFLOW: ID= 1 (0110) 3.63 .16 2.42 37.53 .20 .59

ADD HYD (0114) | AREA QPEAK TPKEAK R.V.  
 1 + 2 = 3 | (ha) (cms) (hrs) (mm)  
 ID1= 1 (0116): .83 .054 2.83 40.46  
 + ID2= 2 (0110): 3.63 .165 2.42 37.53  
 ID = 3 (0114): 4.45 .208 2.42 38.07

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

### Pre-Dev-Con-6hr-Chicago

| ROUTE CHN (0111) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1) ----->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 3.00 215.00 .0500 Main Channel  
 3.76 215.00 .0500  
 5.56 215.60 .0000

TRAVEL TIME TABLE					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.701E+01	0	.18	22.93
.06	215.06	.160E+02	0	.29	14.14
.09	215.09	.270E+02	0	.39	10.61
.13	215.13	.400E+02	.1	.48	8.65
.16	215.16	.530E+02	.1	.56	7.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.216E+03	.9	1.05	3.95
.41	215.41	.247E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.314E+03	1.6	1.23	3.38
.51	215.51	.350E+03	1.8	1.29	3.23
.54	215.54	.390E+03	2.1	1.35	3.09
.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPKEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0102) 1.39 .11 2.50 27.71 .15 .54  
 OUTFLOW: ID= 1 (0111) 1.39 .10 2.58 27.62 .14 .52

ADD HYD (0117) | AREA QPEAK TPKEAK R.V.  
 1 + 2 = 3 | (ha) (cms) (hrs)  
 ID1= 1 (0114): 4.45 .208 2.42 38.07  
 + ID2= 2 (0111): 1.39 .099 2.58 27.62  
 ID = 3 (0117): 5.85 .282 2.58 35.58

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
 ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= .522

Page 20

PEAK FLOW (cms)= .109 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 27.705  
 TOTAL RAINFALL (mm)= 57.490  
 RUNOFF COEFFICIENT = .482

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 19

## Pre-Dev-Con-6hr-Chicago

PEAK FLOW (cms)= .151 (i)  
 TIME TO PEAK (hrs)= 2.667

RUNOFF VOLUME (mm)= 14.982  
 TOTAL RAINFALL (mm)= 57.490

RUNOFF COEFFICIENT = .261

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0113) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
0.00	215.00	.0500 / .0500 Main Channel
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ---->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.541E+01	.0	.15	22.38
.06	215.06	.120E+02	.0	.25	13.54
.09	215.09	.198E+02	.0	.33	10.01
.13	215.13	.294E+02	.1	.41	8.05
.19	215.19	.504E+02	.1	.56	6.91
.22	215.22	.630E+02	.2	.63	5.25
.25	215.25	.768E+02	.3	.70	4.74
.28	215.28	.917E+02	.4	.77	4.33
.32	215.32	.108E+03	.4	.83	4.00
.35	215.35	.125E+03	.6	.90	3.72
.38	215.38	.144E+03	.7	.96	3.48
.41	215.41	.164E+03	.8	1.02	3.28
.44	215.44	.185E+03	1.0	1.08	3.10
.47	215.47	.207E+03	1.2	1.13	2.94
.51	215.51	.230E+03	1.4	1.19	2.80
.54	215.54	.255E+03	1.6	1.24	2.68
.57	215.57	.280E+03	1.8	1.30	2.57
.60	215.60	.307E+03	2.1	1.35	2.47

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0105)	4.82	.15	2.67	14.98	.19
OUTFLOW: ID= 1 (0113)	4.82	.15	2.75	14.96	.19

INFLOW : ID= 2 (0105) 4.82 .15 2.67 14.98 .19 .57  
 OUTFLOW: ID= 1 (0113) 4.82 .15 2.75 14.96 .19 .57

## Pre-Dev-Con-6hr-Chicago

TOTAL RAINFALL (mm)= 57.490  
 RUNOFF COEFFICIENT = .345

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0109) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
0.00	215.00	.0500 / .0500 Main Channel
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ---->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.170E+02	.0	.23	8.87
.09	215.09	.266E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.857E+02	.4	.62	3.30
.28	215.28	.987E+02	.5	.68	3.03
.32	215.32	.114E+03	.7	.73	2.80
.35	215.35	.130E+03	.8	.78	2.61
.38	215.38	.146E+03	1.0	.84	2.45
.41	215.41	.163E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18
.47	215.47	.199E+03	1.6	.99	2.08
.51	215.51	.218E+03	1.8	1.04	1.98
.54	215.54	.238E+03	2.1	1.08	1.89
.57	215.57	.259E+03	2.4	1.13	1.81
.60	215.60	.280E+03	2.7	1.18	1.74

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0112)	1.40	.07	2.50	19.82	.10
OUTFLOW: ID= 1 (0109)	1.40	.07	2.58	19.77	.10

| CALIB | NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
 ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .24

unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .074 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 19.820

Page 21

ADD HYD (0103)   1 + 2 = 3   AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0113): 4.82	.147	2.75	14.96
+ ID2= 2 (0109): 1.40	.071	2.58	19.77
ID = 3 (0103): 6.22	.212	2.75	16.04

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 22

## Pre-Dev-Con-6hr-Chicago

ADD HYD (0106)   1 + 2 = 3   AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0117): 5.85	.282	2.58	35.58
+ ID2= 2 (0103): 6.22	.212	2.75	16.04
ID = 3 (0106): 12.07	.488	2.67	25.51

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Max.Eff.Inten.(mm/hr)= over (min)=	67.74
Storage Coeff. (min)=	25.00
Unit Hyd. Tpeak (min)=	14.82 (ii)
Unit Hyd. peak (cms)=	.32 .05
PAGE NO.	*TOTALS*
PEAK FLOW (cms)= .05	.07 .072
TIME TO PEAK (hrs)= 2.33	2.67 .23
RUNOFF VOLUME (mm)= 64.65	44.20 48.07
TOTAL RAINFALL (mm)= 65.65	65.65 65.65
RUNOFF COEFFICIENT = .98	.67 .73

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 CN' = 88.0 (iii) Dep. Storage (Above)  
 (ii) TIME STEP (hr)= 10.00 min  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0116) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
0.00	215.00	.0500 / .0500 Main Channel
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.676E+01	.0	.13	33.24
.06	215.06	.150E+02	.0	.21	19.61
.09	215.09	.248E+02	.0	.29	14.23
.13	215.13	.346E+02	.1	.37	11.28
.16	215.16	.448E+02	.1	.44	9.41
.19	215.19	.630E+02	.1	.51	8.11
.22	215.22	.787E+02	.2	.58	7.15
.25	215.25	.960E+02	.2	.65	6.41
.28	215.28	.115E+03	.3	.72	5.83
.32	215.32	.135E+03	.4	.78	5.35
.35	215.35	.157E+03	.5	.84	4.95
.38	215.38	.180E+03	.6	.90	4.62
.41	215.41	.205E+03	.8	.96	4.33

Page 24

Page 23

Pre-Dev-Con-6hr-Chicago

.44	215.44	.231E+03	.9	1.02	4.09
.47	215.47	.258E+03	1.1	1.08	3.87
.51	215.51	.288E+03	1.3	1.13	3.68
.54	215.54	.318E+03	1.5	1.19	3.51
.57	215.57	.350E+03	1.7	1.24	3.35
.60	215.60	.384E+03	2.0	1.30	3.22

<---- hydrograph ----> <pipe / channel>

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
.83	.08	2.33	48.07	.15	.42

INFLOW : ID= 2 (0115) .83 .08 2.33 48.07 .15 .42  
OUTFLOW: ID= 1 (0116) .83 .07 2.75 47.89 .14 .41

Pre-Dev-Con-6hr-Chicago

(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.947E+01	.0	.15	38.53
.06	215.06	.210E+02	.0	.25	23.36
.09	215.09	.347E+02	.0	.34	17.30
.13	215.13	.504E+02	.1	.42	13.94
.19	215.19	.682E+02	.1	.50	11.77
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23
.28	215.28	.161E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.252E+03	.7	.96	6.05
.41	215.41	.286E+03	.8	1.02	5.70
.44	215.44	.323E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.404E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

CALIB STANDHYD (0107) | Area (ha)= 3.63 Total Imp(%)= 29.40 Dir. Conn.(%)= 19.00

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IMPERVIOUS PERVIOUS (i)

Surface Area (ha)	1.07	2.56
Dep. Storage (mm)	1.00	3.00
Average Slope (%)	2.00	3.00
Length (m)	155.50	440.00
Mannings n	.013	.250

Max.Eff.Inten.(mm/hr)= 122.63 44.30  
over (min)= 3.00 40.00  
Storage Coeff (min)= 5.49 (ii) 38.98 (ii)  
Unit Hyd. Tpeak (min)= 5.00 40.00  
Unit Hyd. peak (cms)= .29 .03

\*TOTALS\*

PEAK FLOW (cms)	.23	.19	.270 (iii)
TIME TO PEAK (hrs)	2.33	2.92	2.33
RUNOFF VOLUME (mm)	64.65	40.10	44.76
TOTAL RAINFALL (mm)	65.65	65.65	65.65
RUNOFF COEFFICIENT	= .98	.61	

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN\* = 86.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0110) | Routing time step (min)'= 5.00

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<---- DATA FOR SECTION ( 1.1) ---->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
-------	------	--------	-----------	----------	-----------

Page 25

<---- hydrograph ----> <pipe / channel>

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
3.63	.27	2.33	44.76	.25	.71

INFLOW : ID= 2 (0107) 3.63 .27 2.33 44.76 .25 .71  
OUTFLOW: ID= 1 (0110) 3.63 .21 3.00 44.73 .22 .65

---

ADD HYD (0114) | ADD HYD (0114) | AREA QPEAK TPEAK R.V. R.V.  
1 + 2 = 3 | ID1= 1 (0116): .83 .072 2.75 47.89  
+ ID2= 2 (0110): 3.63 .210 3.00 44.73  
ID = 3 (0114): 4.45 .271 3.00 45.31

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
ID= 1 DT=10.0 min Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TIME RAIN TRANSFORMED HYETOGRAPH  
hrs mm/hr hrs mm/hr hrs mm/hr hrs mm  
0.167 1.78 1.667 6.98 3.167 8.95 4.67 2.75  
.333 1.95 1.833 10.01 3.333 7.23 4.83 2.55  
.500 2.14 2.000 16.85 3.500 6.04 5.00 2.37  
.667 2.38 2.167 41.62 3.667 5.17 5.17 2.22  
.833 2.67 2.333 122.63 3.833 4.52 5.33 2.09  
1.000 3.05 2.500 50.34 4.000 4.00 5.50 1.97  
1.167 3.56 2.667 25.45 4.167 3.60 5.67 1.87  
1.333 4.27 2.833 16.21 4.333 3.26 5.83 1.77  
1.500 5.31 3.000 11.63 4.500 2.98 6.00 1.69

### Pre-Dev-Con-6hr-Chicago

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .201 (i)  
TIME TO PEAK (hrs)= 2.667  
RUNOFF VOLUME (mm)= 19.147  
TOTAL RAINFALL (mm)= 65.646  
RUNOFF COEFFICIENT = .292

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0111) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1) ---->

Distance	Elevation	Manning
.00	215.60	.0500
3.00	215.00	.0500 Main Channel
3.76	215.00	.0500
5.56	215.60	.0000

<---- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
-------	------	--------	-----------	----------	-----------

<---- DATA FOR SECTION ( 1.1) ---->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
-------	------	--------	-----------	----------	-----------

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0105) 4.82 .20 2.67 19.15 .22 .64  
OUTFLOW: ID= 1 (0113) 4.82 .20 2.75 19.12 .22 .63

ADD HYD (0117) | ADD HYD (0117) | AREA QPEAK TPEAK R.V.  
1 + 2 = 3 | ID1= 1 (0116): 4.45 .271 3.00 45.31  
+ ID2= 2 (0111): 1.39 .129 2.58 34.00  
ID = 3 (0117): 5.85 .373 2.58 42.62

Page 27

Page 28

## Pre-Dev-Con-6hr-Chicago

CALIB	
NASHYD (0112)	Area (ha)= 1.40 Curve Number (CN)= 75.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hr(s))=.24	

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .098 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 24.972

TOTAL RAINFALL (mm)= 65.646

RUNOFF COEFFICIENT = .380

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0109) | IN= 2--&gt; OUT= 1 | Routing time step (min)'= 5.00

&lt;---- DATA FOR SECTION ( 1.1 ) ----&gt;

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
3.80	215.00	.0500 Main Channel
5.60	215.60	.0500

DEPTH (m)	ELEV (m)	TRAVEL TIME TABLE	TIME	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.813E+01	.0	.14	.14	14.28	
.06	215.06	.170E+02	.0	.23	.23	8.87	
.09	215.09	.266E+02	.1	.31	.31	6.68	
.13	215.13	.369E+02	.1	.38	.38	5.45	
.16	215.16	.480E+02	.2	.44	.44	4.64	
.19	215.19	.598E+02	.2	.50	.50	4.07	
.22	215.22	.724E+02	.3	.56	.56	3.64	
.25	215.25	.850E+02	.4	.62	.62	3.30	
.28	215.28	.997E+02	.5	.68	.68	3.03	
.32	215.32	.114E+03	.7	.73	.73	2.80	
.35	215.35	.130E+03	.8	.78	.78	2.61	
.38	215.38	.146E+03	1.0	.84	.84	2.45	
.41	215.41	.163E+03	1.2	.89	.89	2.31	
.44	215.44	.181E+03	1.4	.94	.94	2.18	
.47	215.47	.199E+03	1.6	.99	.99	2.08	
.51	215.51	.218E+03	1.8	1.04	1.04	1.98	
.54	215.54	.238E+03	2.1	1.08	1.08	1.89	
.57	215.57	.259E+03	2.4	1.13	1.13	1.81	
.60	215.60	.280E+03	2.7	1.18	1.18	1.74	

	<--- hydrograph --->			<pipe / channel>		
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0112)	1.40	.10	2.50	24.97	.12	.35
OUTFLOW: ID= 1 (0109)	1.40	.09	2.58	24.92	.11	.34

ADD HYD (0103) | AREA QPEAK TPEAK R.V.  
1 + 2 = 3 | Page 29

Pre-Dev-Con-6hr-Chicago			
ID1= 1 (0113):	(ha)	(cms)	(hrs)
+ ID2= 2 (0109):	1.40	.093	2.58
			24.92
ID = 3 (0103):	6.22	.281	2.67
			20.42

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)			
1 + 2 = 3	AREA	QPEAK (cms)	TPEAK (hrs)
+ ID1= 1 (0117):	5.85	.373	2.58
+ ID2= 2 (0103):	6.22	.281	2.67
ID = 3 (0106):	12.07	.652	2.67
			31.18

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

*****			
** SIMULATION NUMBER: 5 **			
*****			
CHICAGO STORM Ptotal= 76.13 mm   IDF curve parameters: A=2200.000			
B= 14.600			
C= .870			
used in: INTENSITY = A / (t + B)^AC			
Duration of storm = 6.00 hrs			
Storm time step = 10.00 min			
Time to peak ratio = .38			

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.17	2.21	1.67	8.72	3.17	10.74
.33	2.41	1.43	11.98	3.33	9.72
.50	2.65	2.00	19.90	3.50	7.31
.83	3.29	2.33	135.62	3.83	5.50
1.00	3.75	2.50	157.60	4.00	4.89
1.17	4.36	2.67	29.73	4.17	4.40
1.33	5.21	2.83	19.18	4.33	4.00
1.50	6.45	3.00	13.86	4.50	3.67

CALIB STANDHYD (0115)	Area (ha)= .83
ID= 1 DT= 5.0 min	Total Imp(%)= 33.00
Dir. Conn.()%= 19.00	
	IMPERVIOUS SURFACE Area (ha)= .27
Dep. Storage (mm)= 1.00	2.00
Average Slope (%)= 2.00	3.00
Length (m)= 74.30	275.00
Mannings n = .013	.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.  
Page 30

## Pre-Dev-Con-6hr-Chicago

TIME hrs	TRANSFORMED RAIN mm/hr	TIME hrs	TRANSFORMED RAIN mm/hr	TIME hrs	TRANSFORMED RAIN mm/hr
.083	2.22	1.583	8.42	3.083	10.74
.167	2.22	1.667	8.42	3.167	10.74
.250	2.41	1.750	11.98	3.250	8.72
.333	2.65	1.833	11.88	3.333	8.72
.417	2.65	1.917	19.90	3.417	7.31
.500	2.65	2.000	19.90	3.500	7.31
.583	2.93	2.083	47.86	3.583	6.28
.667	2.93	2.167	47.86	3.667	6.28
.750	3.29	2.250	135.62	3.750	5.50
.833	3.29	2.333	135.62	3.833	5.50
.917	3.75	2.417	57.60	3.917	4.89
1.000	3.75	2.500	57.60	4.000	4.89
1.083	4.36	2.583	29.73	4.083	4.40
1.167	4.36	2.667	29.73	4.167	4.40
1.250	5.21	2.750	19.18	4.250	5.75
1.333	5.21	2.833	19.18	4.333	5.75
1.417	6.45	2.917	13.86	4.417	3.67
1.500	6.45	3.000	13.86	4.500	3.67

Max.Eff.Inten.(mm/hr)= 135.62	79.92
over (min)= 5.00	25.00
Storage Coeff. (min)= 1.54 (ii)	23.27 (ii)
Unit Hyd. Tpeak (min)= 5.00	25.00
Unit Hyd. peak (cms)= .33	.05
	*TOTALS*
PEAK FLOW (cms)= .06	.08
TIME TO PEAK (hrs)= 2.33	2.67
RUNOFF VOLUME (mm)= 75.13	53.79
TOTAL RAINFALL (mm)= 76.13	76.13
RUNOFF COEFFICIENT = .99	.71

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN= 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0116) | IN= 2--&gt; OUT= 1 | Routing time step (min)'= 5.00

&lt;---- DATA FOR SECTION ( 1.1 ) ----&gt;

Distance	Elevation	Manning
.00	215.00	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

DEPTH (m)	ELEV (m)	TRAVEL TIME TABLE	TIME	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.676E+01	.0	.13	.13	33.24	
.06	215.06	.150E+02	.0	.21	.21	19.61	

Pre-Dev-Con-6hr-Chicago			
.09	215.09	.248E+02	.0
.13	215.13	.360E+02	.1
.16	215.16	.488E+02	.1
.19	215.19	.630E+02	.1
.22	215.22	.787E+02	.2
.25	215.25	.960E+02	.2
.28	215.28	.115E+03	.3
.32	215.32	.135E+03	.4
.35	215.35	.155E+03	.5
.38	215.38	.180E+03	.6
.41	215.41	.205E+03	.8
.44	215.44	.231E+03	.9
.47	215.47	.258E+03	1.1
.51	215.51	.288E+03	1.3
.54	215.54	.318E+03	1.5
.57	215.57	.350E+03	1.7
.60	215.60	.384E+03	2.0

<--- hydrograph ---> <-pipe / channel->			
AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0115)	.83	.09	2.67
OUTFLOW: ID= 1 (0116)	.83	.09	2.75

CALIB STANDHYD (0107)	Area (ha)= 3.63
ID= 1 DT= 5.0 min	Total Imp(%)= 29.40
Dir. Conn.()%= 19.00	
	IMPERVIOUS SURFACE Area (ha)= 1.07
Dep. Storage (mm)= 1.00	2.56
Average Slope (%)= 2.00	3.00
Length (m)= 155.50	440.00
Mannings n = .013	.250

Max.Eff.Inten.(mm/hr)= 135.62	57.63
over (min)= 5.00	40.00
Storage Coeff. (min)= 2.39 (ii)	35.24 (ii)
Unit Hyd. Tpeak (min)= 5.00	40.00
Unit Hyd. peak (cms)= .30	.03
	*TOTALS*

PEAK FLOW (cms)= .26	.24
TIME TO PEAK (hrs)= 2.33	2.92
RUNOFF VOLUME (mm)= 75.13	49.33
TOTAL RAINFALL (mm)= 76.13	76.13
RUNOFF COEFFICIENT = .99	.65

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN= 86.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0110) |

Pre-Dev-Con-6hr-Chicago

| IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance	Elevation	Manning
.00	215.00	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.947E+01	.0	.15	38.53
.06	215.06	.210E+02	.0	.25	23.36
.09	215.09	.347E+02	.0	.34	17.30
.13	215.13	.504E+02	.1	.42	13.94
.17	215.17	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23
.28	215.28	.161E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.252E+03	.7	.96	6.05
.41	215.41	.286E+03	.8	1.02	5.70
.44	215.44	.323E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.403E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

<---- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0107) 3.63	.31	2.33	54.23	.27	.74
OUTFLOW: ID= 1 (0110) 3.63	.27	3.00	54.19	.25	.70

<---- ADD HYD (0114) ----->

1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0116): .83	.089	2.75	57.62	
+ ID2= 2 (0110): 3.63	.267	3.00	54.19	
ID = 3 (0114): 4.45	.341	2.92	54.82	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
ID= 1 DT=10.0 min | IA (mm)= 4.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH -----  
Page 33

Pre-Dev-Con-6hr-Chicago

| IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
3.80	215.00	.0500 / .0500 Main Channel
5.60	215.60	.0500

<---- TRAVEL TIME TABLE ----->

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.167	2.22	1.667	8.42	3.167	10.74
.333	2.41	1.833	11.98	3.333	8.72
.500	2.60	2.000	9.98	3.000	7.31
.667	2.93	2.337	4.76	3.667	6.78
.833	3.29	2.333	135.62	1.833	5.50
1.000	3.56	5.760	4.000	4.89	5.50
1.167	4.36	2.667	29.73	4.167	4.40
1.333	5.21	2.833	19.18	4.333	4.00
1.500	6.45	3.000	13.86	4.500	3.67

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= 171 (i)  
TIME TO PEAK (hrs)= 2.500  
RUNOFF VOLUME (mm)= 42.587  
TOTAL RAINFALL (mm)= 76.131  
RUNOFF COEFFICIENT = .559

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0111) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance	Elevation	Manning
.00	215.60	.0500
3.00	215.00	.0500
3.76	215.00	.0500
5.56	215.60	.0000

<---- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.701E+01	.0	.18	22.93
.06	215.06	.180E+02	.0	.29	14.14
.09	215.09	.470E+02	.1	.39	10.61
.13	215.13	.400E+02	.1	.48	8.65
.16	215.16	.550E+02	.1	.56	7.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.216E+03	.9	1.05	3.95
.41	215.41	.247E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.314E+03	1.6	1.23	3.38
.51	215.51	.351E+03	1.8	1.29	3.23
.54	215.54	.390E+03	2.1	1.35	3.09
.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

<---- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0102) 1.39	.17	2.50	42.59	.18	.62
OUTFLOW: ID= 1 (0111) 1.39	.16	2.58	42.51	.18	.61

Page 34

Pre-Dev-Con-6hr-Chicago

<---- ADD HYD (0117) ----->

1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0114): .83	.089	2.75	57.62	
+ ID2= 2 (0111): 3.63	.267	3.00	54.19	
ID = 3 (0117): 5.85	.461	2.75	51.89	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min | IA (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .257 (i)  
TIME TO PEAK (hrs)= 2.667  
RUNOFF VOLUME (mm)= 24.972  
TOTAL RAINFALL (mm)= 76.131  
RUNOFF COEFFICIENT = .328

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0113) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.541E+01	.0	.15	22.38
.06	215.06	.120E+02	.0	.25	13.54
.09	215.09	.198E+02	.0	.33	10.01
.13	215.13	.288E+02	.1	.41	8.05
.16	215.16	.390E+02	.1	.49	6.79
.19	215.19	.504E+02	.1	.56	5.91
.22	215.22	.630E+02	.2	.63	5.25
.25	215.25	.767E+02	.3	.70	4.74
.28	215.28	.917E+02	.4	.77	4.33
.32	215.32	.108E+03	.4	.83	4.00
.35	215.35	.125E+03	.6	.90	3.72
.38	215.38	.144E+03	.7	.96	3.48
.41	215.41	.164E+03	.8	1.02	3.28
.44	215.44	.185E+03	1.0	1.08	3.10
.47	215.47	.207E+03	1.2	1.13	2.94
.51	215.51	.230E+03	1.4	1.19	2.80
.54	215.54	.255E+03	1.6	1.24	2.68

<---- ADD HYD (0118) ----->

1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0114): .83	.089	2.75	57.62	
+ ID2= 2 (0111): 3.63	.267	3.00	54.19	
ID = 3 (0118): 5.85	.461	2.75	51.89	

ROUTE CHN (0109) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
3.80	215.00	.0500 / .0500 Main Channel
5.60	215.60	.0500

<---- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.170E+02	.0	.23	8.87
.09	215.09	.266E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.857E+02	.4	.62	3.30
.28	215.28	.997E+02	.5	.68	3.03
.32	215.32	.114E+03	.7	.73	2.80
.35	215.35	.130E+03	.8	.78	2.61
.38	215.38	.146E+03	1.0	.84	2.45
.41	215.41	.162E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18
.47	215.47	.199E+03	1.6	.99	2.08
.51	215.51	.218E+03	1.8	1.04	1.98
.54	215.54	.238E+03	2.1	1.08	1.89
.57	215.57	.259E+03	2.4	1.13	1.81
.60	215.60	.280E+03	2.7	1.18	1.74

<---- hydrograph -----> <-pipe / channel->

Pre-Dev-Con-6hr-Chicago  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0112) 1.40 .12 2.50 32.04 .13 .39  
 OUTFLOW: ID= 1 (0109) 1.40 .12 2.58 31.99 .13 .38

Pre-Dev-Con-6hr-Chicago  
 STANDHY (0115) Area (ha)= .83  
 ID= 1 DT= 5.0 min Total Imp(%)= 33.00 Dir. Conn.(%)= 19.00  
 IMPERVIOUS PERVIOUS (i)  
 Surface Area (ha)= .27 .55  
 Dep. Storage (mm)= 1.00 2.00  
 Average Slope (%)= 2.00 3.00  
 Length (m)= 74.30 275.00  
 Manning's n = .013 .250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

ADD HYD (0103)  
 1 + 2 = 3 AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0113): 4.82 .252 2.75 24.95  
 + ID2= 2 (0109): 1.40 .119 2.58 31.99  
 ID = 3 (0103): 6.22 .359 2.67 26.53

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)  
 1 + 2 = 3 AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0117): 5.85 .461 2.75 51.89  
 + ID2= 2 (0103): 6.22 .359 2.67 26.53  
 ID = 3 (0106): 12.07 .819 2.67 38.82

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
 \*\* SIMULATION NUMBER: 6 \*\*  
 \*\*\*\*\*

CHICAGO STORM Ptotal= 81.72 mm | IDF curve parameters: A=2507.000  
 B= 14.800 C= .880  
 used in: INTENSITY = A / (t + B)^AC  
 Duration of storm = 6.00 hrs  
 Storm time step = 10.00 min  
 Time to peak ratio = .38

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.15	2.02	1.67	8.87	3.17	11.36	4.67	3.47
.33	2.45	1.73	12.07	3.33	9.17	4.83	3.22
.50	2.70	2.00	11.34	3.50	7.66	5.00	3.00
.67	3.00	2.17	52.05	3.67	6.56	5.17	2.81
.83	3.38	2.33	148.61	3.83	5.72	5.33	2.64
1.00	3.86	2.50	62.77	4.00	5.07	5.42	2.49
1.17	4.51	2.67	32.11	4.17	4.00	5.50	2.49
1.33	5.41	2.83	20.54	4.55	3.33	5.58	2.36
1.50	6.73	3.00	14.75	4.50	2.77	5.67	2.36
						1.417	2.917 14.75 4.417 3.77 5.92 2.13
						1.500	6.73 3.000 14.75 4.500 3.77 6.00 2.13

TRANSFORMED HYETROGRAPH			
TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr
.093	2.43	1.13	8.88
.167	2.23	1.667	8.95
.250	2.45	1.750	12.70
.333	2.45	1.833	12.70
.417	2.70	1.917	21.34
.500	2.70	2.000	21.34
.583	3.00	2.083	52.05
.667	3.00	2.167	52.05
.750	3.38	2.250	148.61
.833	3.38	2.333	148.61
.917	3.86	2.417	62.78
1.000	3.86	2.500	62.78
1.083	4.51	2.583	32.11
.167	4.51	2.667	32.11
1.250	5.41	2.750	20.54
1.333	5.41	2.833	20.54
1.417	6.73	2.917	14.75
1.500	6.73	3.000	14.75

Max.Eff.Inten.(mm/hr)= 148.61 101.98  
 over (min)= 5.00 25.00  
 Storage Coeff. (min)= 1.48 (ii) 21.20 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 25.00  
 Unit Hyd. peak (cms)= .33 .05  
 \*TOTALS\*  
 PEAK FLOW (cms)= .06 .09 .108 (iii)  
 TIME TO PEAK (hrs)= 2.33 2.67 2.67  
 RUNOFF VOLUME (mm)= 80.72 58.97 63.09  
 TOTAL RAINFALL (mm)= 81.72 81.72 81.72  
 RUNOFF COEFFICIENT = .99 .72 .77

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES;  
 $CN^* = 88.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0116) IN= Z--> OUT= 1 Routing time step (min)'= 5.00  
 <---- DATA FOR SECTION ( 1,1) ----->  
 Page 38

CALIB Page 37

Pre-Dev-Con-6hr-Chicago  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 676E+01 0 .13 33.24  
 .06 215.06 150E+02 .0 .21 19.61  
 .09 215.09 248E+02 .0 .29 14.23  
 .13 215.13 360E+02 .1 .37 11.28  
 .16 215.16 488E+02 .1 .44 9.41  
 .19 215.19 630E+02 .1 .51 8.11  
 .22 215.22 787E+02 .2 .58 7.15  
 .25 215.25 960E+02 .2 .65 6.41  
 .28 215.28 115E+03 .3 .72 5.83  
 .32 215.32 135E+03 .4 .78 5.35  
 .35 215.35 157E+03 .5 .84 4.95  
 .38 215.38 180E+03 .6 .90 4.62  
 .41 215.41 205E+03 .8 .96 4.33  
 .44 215.44 231E+03 .9 1.02 4.09  
 .47 215.47 258E+03 1.1 1.08 3.87  
 .51 215.51 288E+03 1.3 1.13 3.68  
 .54 215.54 318E+03 1.5 1.19 3.51  
 .57 215.57 350E+03 1.7 1.24 3.35  
 .60 215.60 .384E+03 2.0 1.30 3.22

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0115) .83 .11 2.67 63.09 .17 .48  
 OUTFLOW: ID= 1 (0116) .83 .10 2.75 62.87 .17 .47

CALIB STANDHY (0107) Area (ha)= 3.63 dir. conn.(%)= 19.00  
 ID= 1 DT= 5.0 min Total Imp(%)= 29.40 Dir. Conn.(%)= 19.00  
 IMPERVIOUS PERVIOUS (i)

Surface Area (ha)= 1.07 2.56  
 Dep. Storage (mm)= 1.00 3.00  
 Average Slope (%)= 2.00 3.00  
 Length (m)= 155.50 440.00  
 Manning's n = .013 .250

Max.Eff.Inten.(mm/hr)= 148.61 64.62  
 over (min)= 5.00 35.00  
 Storage Coeff. (min)= 2.31 (ii) 33.68 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 35.00  
 Unit Hyd. peak (cms)= .30 .03  
 \*TOTALS\*  
 PEAK FLOW (cms)= .28 .29 .354 (iii)  
 TIME TO PEAK (hrs)= 2.33 2.83 2.33  
 RUNOFF VOLUME (mm)= 80.72 54.35 59.36  
 TOTAL RAINFALL (mm)= 81.72 81.72 81.72  
 RUNOFF COEFFICIENT = .99 .67 .73

Pre-Dev-Con-6hr-Chicago  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES;  
 $CN^* = 86.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0110) IN= 2--> OUT= 1 Routing time step (min)'= 5.00  
 <---- DATA FOR SECTION ( 1,1) ----->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 947E+01 0 .15 38.53  
 .06 215.06 210E+02 .0 .25 23.36  
 .09 215.09 347E+02 .0 .34 17.30  
 .13 215.13 504E+02 .1 .42 13.94  
 .16 215.16 683E+02 .1 .50 11.77  
 .19 215.19 882E+02 .1 .57 10.25  
 .22 215.22 110E+03 .2 .64 9.11  
 .25 215.25 134E+03 .3 .71 8.23  
 .28 215.28 160E+03 .4 .78 7.93  
 .32 215.32 189E+03 .5 .84 6.95  
 .35 215.35 219E+03 .6 .90 6.47  
 .38 215.38 252E+03 .7 .96 6.05  
 .41 215.41 286E+03 .8 1.02 5.70  
 .44 215.44 323E+03 1.0 1.08 5.39  
 .47 215.47 362E+03 1.2 1.14 5.12  
 .51 215.51 403E+03 1.4 1.20 4.88  
 .54 215.54 446E+03 1.6 1.25 4.66  
 .57 215.57 491E+03 1.8 1.30 4.47  
 .60 215.60 .538E+03 2.1 1.36 4.30

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0107) 3.63 .35 2.33 59.36 .28 .77  
 OUTFLOW: ID= 1 (0110) 3.63 .31 2.92 59.31 .27 .74

ADD HYD (0114) 1 + 2 = 3 AREA QPEAK TPEAK R.V.  
 ID1= 1 (0116): .83 .102 2.75 62.87  
 + ID2= 2 (0110): 3.63 .314 2.92 59.31  
 ID = 3 (0114): 4.45 .405 2.83 59.97

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 39

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 Page 39

## Pre-Dev-Con-6hr-Chicago

CALIB	NASHYD (0102)	Area (ha)=	1.39	Curve Number (CN)=	84.0
ID= 1 DT=10.0 min	Ia (mm)=	4.00	# of Linear Res.(N)=	3.00	
U.H. Tp(hr)= .24					

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.167	2.25	1.667	8.85	3.167	11.36
.333	2.45	1.833	12.70	3.333	9.17
.500	2.70	2.000	21.34	3.500	7.66
.667	3.00	2.167	52.00	4.000	5.00
.833	3.38	2.333	148.61	3.833	9.92
1.000	3.86	2.500	62.78	4.000	5.07
1.167	4.51	2.667	32.11	4.167	4.55
1.333	5.41	2.833	20.54	4.333	4.12
1.500	6.73	3.000	14.75	4.500	3.77
					6.00
					2.13

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .194 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 47.255  
 TOTAL RAINFALL (mm)= 81.724  
 RUNOFF COEFFICIENT = .578

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0111)	IN= 2--> OUT= 1	Routing time step (min)'= 5.00
------------------	-----------------	--------------------------------

---- DATA FOR SECTION ( 1.1) ---->		
Distance	Elevation	Manning
.00	215.60	.0500
3.00	215.00	.0500
3.76	215.00	.0500
5.56	215.60	.0000

<---- TRAVEL TIME TABLE ---->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.701E+01	.0	.18	22.93
.06	215.06	.160E+02	.0	.29	10.14
.09	215.09	.270E+02	.0	.39	10.61
.13	215.13	.400E+02	.1	.48	9.65
.16	215.16	.550E+02	.1	.56	9.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.216E+03	.9	1.05	3.95
.41	215.41	.247E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.314E+03	1.6	1.23	3.38

Pre-Dev-Con-6hr-Chicago					
.51	215.51	.351E+03	1.8	1.29	3.23
.54	215.54	.390E+03	2.1	1.35	3.09
.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

<---- hydrograph ----> <-pipe / channel->					
INFLOW : ID= 2 (0102)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
OUTFLOW: ID= 1 (0111)	5.39	.19	2.50	47.26	.19
					.65

<---- hydrograph ----> <-pipe / channel->					
ADD HYD (0117)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0114):		4.45	.405	2.83	59.97
+ ID2= 2 (0111):		1.39	.182	2.58	47.18
ID = 3 (0117):		5.85	.552	2.75	56.92

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0111)	IN= 2--> OUT= 1	Routing time step (min)'= 5.00
------------------	-----------------	--------------------------------

---- DATA FOR SECTION ( 1.1) ---->		
Distance	Elevation	Manning
.00	215.60	.0500
3.00	215.00	.0500
3.76	215.00	.0500
5.56	215.60	.0000

<---- TRAVEL TIME TABLE ---->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.701E+01	.0	.18	22.93
.06	215.06	.160E+02	.0	.29	10.14
.09	215.09	.270E+02	.0	.39	10.61
.13	215.13	.400E+02	.1	.48	9.65
.16	215.16	.550E+02	.1	.56	9.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.216E+03	.9	1.05	3.95
.41	215.41	.247E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.314E+03	1.6	1.23	3.38

CALIB	NASHYD (0112)	Area (ha)=	1.40	Curve Number (CN)=	75.0
ID= 1 DT=10.0 min	Ia (mm)=	5.00	# of Linear Res.(N)=	3.00	
U.H. Tp(hr)= .24					

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .141 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 35.987  
 TOTAL RAINFALL (mm)= 81.724  
 RUNOFF COEFFICIENT = .440

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0109)	IN= 2--> OUT= 1	Routing time step (min)'= 5.00
------------------	-----------------	--------------------------------

---- DATA FOR SECTION ( 1.1) ---->		
Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500
3.80	215.00	.0500
5.60	215.60	.0500

<---- TRAVEL TIME TABLE ---->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.813E+01	.0	.14	5.69
.06	215.06	.170E+02	.0	.23	8.67
.09	215.09	.266E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.857E+02	.4	.62	3.30
.28	215.28	.997E+02	.5	.68	3.03
.32	215.32	.114E+03	.7	.73	2.80

Pre-Dev-Con-6hr-Chicago					
.35	215.35	.130E+03	.8	.78	2.61
.38	215.38	.146E+03	1.0	.84	2.45
.41	215.41	.163E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18
.47	215.47	.199E+03	1.6	.99	2.08

<---- hydrograph ----> <-pipe / channel->					
INFLOW : ID= 2 (0112)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)
OUTFLOW: ID= 1 (0109)	1.40	.14	2.58	35.94	.14
					.40

<---- hydrograph ----> <-pipe / channel->					
ADD HYD (0103)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0113):		4.82	.292	2.75	28.25
+ ID2= 2 (0109):		1.40	.137	2.58	35.94
ID = 3 (0103):		6.22	.416	2.67	29.98

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<---- hydrograph ----> <-pipe / channel->					
ADD HYD (0106)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0117):		5.85	.552	2.75	56.92
+ ID2= 2 (0103):		6.22	.416	2.67	29.98
ID = 3 (0106):		12.07	.964	2.67	43.04

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

Pre-Dev-Con-AES

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V V I SSSSS U U A L
V V I SS U U A A L
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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual otthymo v2.0\voin.dat  
output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Controlled.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Controlled.sum

DATE: 1/23/2019 TIME: 2:12:48 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 1 \*\*  
\*\*\*\*\*  

MASS STORM	Filename: C:\visual otthymo files\4456\AES 1-hr.mst
Ptotal= 22.50 mm	Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=

Duration of storm = 1.00 hrs  
Mass curve time step = 5.00 min  

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs mm/hr							
.08 10.02	.33 69.93	.58 11.10	.83 .81	.17 30.00	.42 64.29	.67 4.62	.92 .30
.25 49.98	.50 27.03	.75 1.92	1.00 .03				

CALIB	STANDHYD (0115)	Area (ha)= .83
ID= 1 DT= 5.0 min	Total Imp(%)= 33.00	Dir. Conn.(%)= 19.00

Page 1

Pre-Dev-Con-AES

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.27	.55
Dep. Storage (mm)=	1.00	2.00
Average Slope (%)=	2.00	3.00
Length (m)=	74.30	275.00
Mannings n =	.013	.250
Max.Eff.Inten.(mm/hr)=	69.93	14.12
over (min)=	5.00	50.00
Storage Coeff. (min)=	2.00 (ii)	45.48 (ii)
Unit Hyd. Tpeak (min)=	5.00	50.00
Unit Hyd. peak (cms)=	.31	.02
PEAK FLOW (cms)=	.03	.01
TIME TO PEAK (hrs)=	.33	.17
RUNOFF VOLUME (mm)=	21.50	8.78
TOTAL RAINFALL (mm)=	22.50	22.50
RUNOFF COEFFICIENT =	.96	.50

\*TOTALS\*

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN<sup>\*</sup> = 88.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0116)		Routing time step (min)'= 5.00	
IN= 2-->	OUT= 1	<---- DATA FOR SECTION ( 1.1 ) ----->	
Distance	Elevation	Manning	
.00	215.60	.0500	Main Channel
1.80	215.00	.0500 / .0500	Main Channel
2.56	215.00	.0500 / .0500	Main Channel
4.36	215.60	.0500	

TRAVEL TIME TABLE							
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)		
.03	215.03	.676E+01	.0	.13	33.24		
.06	215.06	.150E+02	.0	.21	19.61		
.09	215.09	.248E+02	.0	.29	14.23		
.13	215.13	.360E+02	.1	.37	11.28		
.19	215.19	.488E+02	.1	.44	9.41		
.19	215.19	.608E+02	.1	.51	8.11		
.23	215.23	.787E+02	.2	.58	7.35		
.25	215.25	.960E+02	.2	.65	6.41		
.28	215.28	.115E+03	.3	.72	5.83		
.32	215.32	.135E+03	.4	.78	5.35		
.35	215.35	.157E+03	.5	.84	4.95		
.38	215.38	.180E+03	.6	.90	4.62		
.41	215.41	.205E+03	.8	.96	4.33		
.44	215.44	.231E+03	.9	1.02	4.09		
.47	215.47	.258E+03	1.1	1.08	3.87		
.51	215.51	.288E+03	1.3	1.13	3.68		
.54	215.54	.318E+03	1.5	1.19	3.51		
.57	215.57	.350E+03	1.7	1.24	3.35		

Page 2

Pre-Dev-Con-AES

.60	215.60	.384E+03	2.0	1.30	3.22
<---- hydrograph ----> <-pipe / channel->					
AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
.83	.03	.33	11.16	.10	.30

INFLOW : ID= 2 (0115) OUTFLOW: ID= 1 (0116) .83 .02 .50 11.08 .07 .23

CALIB	STANDHYD (0107)	Area (ha)= 3.63
ID= 1 DT= 5.0 min	Total Imp(%)= 29.40	Dir. Conn.(%)= 19.00

IMPERVIOUS PERVIOUS (i)

Surface Area (ha)=	1.07	2.56
Dep. Storage (mm)=	1.00	3.00
Average Slope (%)=	2.00	3.00
Length (m)=	155.50	440.00
Mannings n =	.013	.250

Max.Eff.Inten.(mm/hr)= 69.93 over (min)= 5.00 8.11  
Storage Coeff. (min)= 3.12 (ii) 75.07 (ii)  
Unit Hyd. Tpeak (min)= 5.00 80.00  
Unit Hyd. peak (cms)= .27 .01

\*TOTALS\*

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN<sup>\*</sup> = 86.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0110)	IN= 2--> OUT= 1	Routing time step (min)'= 5.00
<---- DATA FOR SECTION ( 1.1 ) ----->		
Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

TRAVEL TIME TABLE							
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)		
.03	215.03	.947E+01	.0	.15	38.53		
.06	215.06	.210E+02	.0	.25	23.36		
.09	215.09	.347E+02	.0	.34	17.30		
.13	215.13	.504E+02	.1	.42	13.94		

Page 3

Pre-Dev-Con-AES

.16	215.16	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23
.28	215.28	.161E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.252E+03	.7	.96	6.05
.41	215.41	.280E+03	.8	1.02	5.70
.44	215.44	.322E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.403E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
3.63	.13	.42	9.80	.18	.54
3.63	.09	.50	9.79	.15	.48

ADD HYD (0114)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0116):		.83	.018	.50	11.08
+ ID2= 2 (0110):		3.63	.089	.50	9.79
ID = 3 (0114):		4.45	.107	.50	10.03

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	NASHYD (0102)	Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00	U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TRANSFORMED HYETOGRAPH							
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.167	20.01	.500	45.66	.833	1.36	.16	
.333	59.95	.667	7.86	1.000			

Unit Hyd Qpeak (cms)= .223  
PEAK FLOW (cms)= .034 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 5.048  
TOTAL RAINFALL (mm)= 22.500  
RUNOFF COEFFICIENT = .224

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 4

## Pre-Dev-Con-AES

| ROUTE CHN (0111) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1  
 <---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500 Main Channel  
 3.00 215.00 .0500 Main Channel  
 3.76 215.00 .0500 Main Channel  
 5.56 215.60 .0000

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .701E+01 .0 .18 22.93  
 .06 215.06 .160E+01 .0 .29 14.14  
 .09 215.09 .240E+02 .0 .39 10.61  
 .13 215.13 .400E+02 .1 .48 8.65  
 .16 215.16 .550E+02 .1 .56 7.38  
 .19 215.19 .720E+02 .2 .64 6.48  
 .22 215.22 .909E+02 .3 .72 5.80  
 .25 215.25 .112E+03 .4 .79 5.27  
 .28 215.28 .135E+03 .5 .86 4.85  
 .32 215.32 .160E+03 .6 .93 4.50  
 .35 215.35 .187E+03 .7 .99 4.21  
 .38 215.38 .216E+03 .9 1.05 3.95  
 .41 215.41 .247E+03 1.1 1.12 3.74  
 .44 215.44 .280E+03 1.3 1.17 3.55  
 .47 215.47 .314E+03 1.6 1.23 3.38  
 .51 215.51 .351E+03 1.8 1.29 3.23  
 .54 215.54 .390E+03 2.1 1.35 3.09  
 .57 215.57 .431E+03 2.4 1.40 2.97  
 .60 215.60 .474E+03 2.8 1.46 2.86

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0102) 1.39 .03 .50 5.05 .08 .35  
 OUTFLOW: ID= 1 (0111) 1.39 .03 .75 4.97 .08 .33

| ADD HYD (0117) |  
 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 + ID1= 1 (0114): 4.45 .107 .50 10.03  
 + ID2= 2 (0111): 1.39 .028 .75 4.97  
 ID = 3 (0117): 5.85 .120 .50 8.82

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

## Pre-Dev-Con-AES

PEAK FLOW (cms)= .038 (i)  
 TIME TO PEAK (hrs)= .667  
 RUNOFF VOLUME (mm)= 2.058  
 TOTAL RAINFALL (mm)= 22.500  
 RUNOFF COEFFICIENT = .091

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0113) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500 Main Channel  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.36 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .541E+01 .0 .15 22.38  
 .06 215.06 .120E+02 .0 .25 13.54  
 .09 215.09 .198E+02 .0 .33 10.01  
 .13 215.13 .288E+02 .1 .41 8.05  
 .16 215.16 .380E+02 .1 .49 6.79  
 .19 215.19 .504E+02 .1 .56 5.91  
 .22 215.22 .630E+02 .2 .63 5.25  
 .25 215.25 .768E+02 .3 .70 4.74  
 .28 215.28 .917E+02 .4 .77 4.33  
 .32 215.32 .108E+03 .4 .83 4.00  
 .35 215.35 .125E+03 .6 .90 3.72  
 .38 215.38 .144E+03 .7 .96 3.48  
 .41 215.41 .164E+03 .8 1.02 3.28  
 .44 215.44 .185E+03 1.0 1.08 3.10  
 .47 215.47 .207E+03 1.2 1.13 2.94  
 .51 215.51 .230E+03 1.4 1.19 2.80  
 .54 215.54 .252E+03 1.6 1.24 2.68  
 .57 215.57 .280E+03 1.8 1.30 2.57  
 .60 215.60 .307E+03 2.1 1.35 2.47

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0105) 4.82 .04 .67 2.06 .10 .35  
 OUTFLOW: ID= 1 (0113) 4.82 .03 .83 2.03 .10 .34

| CALIB NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
 ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222  
 PEAK FLOW (cms)= .020 (i)  
 TIME TO PEAK (hrs)= .667  
 RUNOFF VOLUME (mm)= 2.957  
 TOTAL RAINFALL (mm)= 22.500

Page 6

Page 5

## Pre-Dev-Con-AES

RUNOFF COEFFICIENT = .131  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOWS IF ANY.

| ROUTE CHN (0109) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500 Main Channel  
 1.80 215.00 .0500 / .0500 Main Channel  
 3.80 215.00 .0500 Main Channel  
 5.60 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .813E+01 .0 .14 14.28  
 .06 215.06 .170E+02 .0 .23 10.67  
 .09 215.09 .266E+02 .1 .31 6.68  
 .13 215.13 .369E+02 .1 .38 5.45  
 .16 215.16 .480E+02 .2 .44 4.64  
 .19 215.19 .598E+02 .2 .50 4.07  
 .22 215.22 .724E+02 .3 .56 3.64  
 .25 215.25 .857E+02 .4 .62 3.30  
 .28 215.28 .997E+02 .5 .68 3.03  
 .32 215.32 .114E+03 .7 .73 2.80  
 .35 215.35 .130E+03 .8 .78 2.61  
 .38 215.38 .146E+03 1.0 .84 2.45  
 .41 215.41 .162E+03 1.2 .89 2.11  
 .44 215.44 .181E+03 1.4 .94 2.18  
 .47 215.47 .199E+03 1.6 .99 2.08  
 .51 215.51 .218E+03 1.8 1.04 1.98  
 .54 215.54 .238E+03 2.1 1.08 1.89  
 .57 215.57 .259E+03 2.4 1.13 1.81  
 .60 215.60 .280E+03 2.7 1.18 1.74

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0112) 1.40 .02 .67 2.96 .05 .17  
 OUTFLOW: ID= 1 (0109) 1.40 .02 .75 2.92 .04 .16

| 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 + ID1= 1 (0117): 5.85 .120 .50 8.82  
 + ID2= 2 (0103): 6.22 .049 .83 2.23  
 ID = 3 (0106): 12.07 .137 .50 5.43

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\* SIMULATION NUMBER: 2 \*\*  
 \*\*\*\*\*

| MASS STORM | Filename: C:\visual otthymo files\4456\AES 1-hour.rst  
 Ptotal= 30.50 mm Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=

Duration of storm = 1.00 hrs  
 Mass curve time step = 5.00 min

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	13.58	.33	94.79	.58	15.04	.83	1.10
.17	40.66	.42	87.14	.67	6.26	.92	.40
.25	67.75	.50	36.64	.75	2.60	1.00	.04

| CALIB STANDHYD (0115) | Area (ha)= .83 Total Imp(%)= 33.00 Dir. Conn.(%)= 19.00

IMPERVIOUS PERVIOUS (i)  
 Surface Area (ha)= .27 .55  
 Dep. Storage (mm)= 1.00 2.00  
 Average Slope (%)= 2.00 3.00  
 Length (m)= 74.30 275.00  
 Mannings n = .013 .250

Max.Eff.Inten.(mm/hr)= 94.79 29.46  
 over (min)= 5.00 35.00  
 Storage Coeff. (min)= 1.77 (ii) 34.00 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 35.00  
 Unit Hyd. peak (cms)= .32 .03

\*TOTALS\*

PEAK FLOW (cms)= .04 .03 .044 (iii)  
 TIME TO PEAK (hrs)= .33 .92 .42  
 RUNOFF VOLUME (mm)= 29.50 14.47 17.30  
 TOTAL RAINFALL (mm)= 30.50 30.50 30.50  
 RUNOFF COEFFICIENT = .97 .47 .57

\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = .88.0 Ta = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| ADD HYD (0106) |

Page 7

Page 8

Pre-Dev-Con-AES

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| ROUTE CHN (0116) | Routing time step (min)'= 5.00
| IN= 2--> OUT= 1 |
<---- DATA FOR SECTION ( 1.1 ) ---->
Distance Elevation Manning
.00 215.60 .0500
1.80 215.00 .0500 / .0500 Main Channel
2.56 215.00 .0500 / .0500 Main Channel
4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
(m) (m) (cu.m.) (cms) (m/s) (min)
.03 215.03 .676E+01 .0 .13 33.24
.06 215.06 .150E+02 .0 .21 19.61
.09 215.09 .240E+02 .0 .29 13.23
.13 215.13 .360E+02 .1 .37 11.28
.16 215.16 .488E+02 .1 .44 9.41
.19 215.19 .630E+02 .1 .51 8.11
.22 215.22 .787E+02 .2 .58 7.15
.25 215.25 .960E+02 .2 .65 6.41
.28 215.28 .115E+03 .3 .72 5.83
.32 215.32 .135E+03 .4 .78 5.35
.35 215.35 .157E+03 .5 .84 4.95
.38 215.38 .180E+03 .6 .90 4.62
.41 215.41 .205E+03 .8 .96 4.33
.44 215.44 .230E+03 .9 1.02 4.09
.47 215.47 .258E+03 1.1 1.08 3.87
.51 215.51 .288E+03 1.3 1.13 3.68
.54 215.54 .318E+03 1.5 1.19 3.51
.57 215.57 .350E+03 1.7 1.24 3.35
.60 215.60 .384E+03 2.0 1.30 3.22

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0115) .83 .04 .42 17.30 .11 .34
OUTFLOW: ID= 1 (0116) .83 .03 .50 17.19 .10 .30

-----+
| CALIB STANDHYD (0107) | Area (ha)= 3.63
| ID= 1 DT= 5.0 min | Total Imp(%)= 29.40 Dir. Conn.(%)= 19.00
| IMPERVIOUS PERVERIOUS (i) |
Surface Area (ha)= 1.00 2.56
Dep. Storage (mm)= 1.00 3.00
Average Slope (%)= 1.00 3.00
Length (m)= 155.50 440.00
Mannings n = .013 .250

Max.Eff.Inten.(mm/hr)= 94.79 13.96
over (min)= 5.00 65.00
Storage Coeff. (min)= 2.76 (ii) 60.68 (ii)
Unit Hyd. Peak (min)= 5.00 65.00
Unit Hyd. peak (cms)= .28 .02
PEAK FLOW (cms)= .17 .06 .174 (iii)
TIME TO PEAK (hrs)= .33 1.42 .33
RUNOFF VOLUME (mm)= 29.50 12.16 15.45

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Page 9

TOTAL RAINFALL (mm)=	30.50	30.50	30.50
RUNOFF COEFFICIENT =	.97	.40	.51

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.  
(i) CN PROCEDURE SELECTED FOR PREVIOUS LOSSES:  
CN\* = 86.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0110) | Routing time step (min)'= 5.00
| IN= 2--> OUT= 1 |

<---- DATA FOR SECTION ( 1.1 ) ---->
Distance Elevation Manning
.00 215.60 .0500
1.80 215.00 .0500 / .0500 Main Channel
2.56 215.00 .0500 / .0500 Main Channel
4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
(m) (m) (cu.m.) (cms) (m/s) (min)
.03 215.03 9.7E+01 .0 .15 38.33
.06 215.06 .210E+02 .0 .25 23.36
.09 215.09 .347E+02 .0 .34 17.30
.13 215.13 .504E+02 .1 .42 13.94
.16 215.16 .683E+02 .1 .50 11.77
.19 215.19 .882E+02 .1 .57 10.25
.22 215.22 .110E+03 .2 .64 9.11
.25 215.25 .134E+03 .3 .71 8.23
.28 215.28 .161E+03 .4 .78 7.53
.32 215.32 .189E+03 .5 .84 6.95
.35 215.35 .217E+03 .6 .90 6.47
.38 215.38 .252E+03 .7 .96 6.05
.41 215.41 .286E+03 .8 1.02 5.70
.44 215.44 .323E+03 1.0 1.08 5.39
.47 215.47 .362E+03 1.2 1.14 5.12
.51 215.51 .403E+03 1.4 1.20 4.88
.54 215.54 .446E+03 1.6 1.25 4.66
.57 215.57 .491E+03 1.8 1.30 4.47
.60 215.60 .538E+03 2.1 1.36 4.30

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0107) 3.63 .17 .33 15.45 .21 .60
OUTFLOW: ID= 1 (0110) 3.63 .13 .50 15.43 .18 .55

| ADD HYD (0114) | 1 + 2 = 3
| ID1= 1 (0116): .83 .030 .50 17.19
| + ID2= 2 (0110): 3.63 .130 .50 15.43

Page 10

Pre-Dev-Con-AES

ID = 3 (0114): .445 .160 .50 15.76

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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| CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0
| ID= 1 DT=10.0 min | U.H. Tp(hrs)= .24

```

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.167	.27.12	.500	.61.89	.833	.1.85
.333	.81.27	.667	.10.65	1.000	.22

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .064 (i)
TIME TO PEAK (hrs)= .500
RUNOFF VOLUME (mm)= 9.250
TOTAL RAINFALL (mm)= 30.500
RUNOFF COEFFICIENT = .303

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0102) 1.39 .06 .50 9.25 .11 .44
OUTFLOW: ID= 1 (0111) 1.39 .06 .67 9.16 .11 .42

| ADD HYD (0117) | 1 + 2 = 3
| ID1= 1 (0114): 4.45 .160 .50 15.76
| + ID2= 2 (0111): 1.39 .055 .67 9.16
| ID = 3 (0117): 5.85 .191 .50 14.19

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

| CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0
| ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .35

```

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .076 (i)
TIME TO PEAK (hrs)= .667
RUNOFF VOLUME (mm)= 4.146
TOTAL RAINFALL (mm)= 30.500
RUNOFF COEFFICIENT = .136

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0113) | Routing time step (min)'= 5.00
| IN= 2--> OUT= 1 |

<---- DATA FOR SECTION ( 1.1 ) ---->
Distance Elevation Manning
.00 215.60 .0500
1.80 215.00 .0500 / .0500 Main Channel
2.56 215.00 .0500 / .0500 Main Channel
4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
(m) (m) (cu.m.) (cms) (m/s) (min)
.03 215.03 .541E+01 .0 .15 22.38
.06 215.06 .120E+02 .0 .25 13.54
.09 215.09 .198E+02 .0 .33 10.01
.13 215.13 .288E+02 .1 .41 8.05
.16 215.16 .390E+02 .1 .49 6.79
.19 215.19 .504E+02 .1 .56 5.91
.22 215.22 .630E+02 .2 .63 5.25
.25 215.25 .768E+02 .3 .70 4.74

Page 12

Page 11

Pre-Dev-Con-AES

.28	215.28	.917E+02	.4	.77	4.33
.32	215.32	.108E+03	.4	.83	4.00
.35	215.35	.125E+03	.6	.90	3.72
.38	215.38	.144E+03	.7	.96	3.48
.41	215.41	.163E+03	.8	1.02	3.28
.44	215.44	.185E+03	1.0	1.08	3.00
.47	215.47	.207E+03	1.2	1.13	2.94
.51	215.51	.230E+03	1.4	1.19	2.80
.54	215.54	.255E+03	1.6	1.24	2.68
.57	215.57	.280E+03	1.8	1.30	2.57
.60	215.60	.307E+03	2.1	1.35	2.47

<---- hydrograph ----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0105)	4.82	.08	.67	4.15	.45
OUTFLOW : ID= 1 (0113)	4.82	.07	.75	4.12	.43

Pre-Dev-Con-AES

.41	215.41	.163E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18
.47	215.47	.199E+03	1.6	.99	2.08
.51	215.51	.218E+03	1.8	1.04	1.98
.54	215.54	.238E+03	2.1	1.08	1.89
.57	215.57	.259E+03	2.4	1.13	1.81
.60	215.60	.280E+03	2.7	1.18	1.74

<---- hydrograph ----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0112)	1.40	.04	.50	5.82	.07
OUTFLOW : ID= 1 (0109)	1.40	.04	.67	5.78	.07

CALIB NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .039 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 5.823  
TOTAL RAINFALL (mm)= 30.500  
RUNOFF COEFFICIENT = .191

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0109) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00  
<---- DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
3.80 215.00 .0500 Main Channel  
5.60 215.60 .0500

TRAVEL TIME TABLE  
<---- DATA FOR SECTION ( 1.1 ) ----->  
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV. TIME  
(m) (m) (cu.m.) (cms) (m/s) (min)  
.03 215.03 .813E+01 .0 .14 14.28  
.06 215.06 .170E+02 .0 .23 8.87  
.09 215.09 .266E+02 .1 .31 6.68  
.13 215.13 .369E+02 .1 .38 5.45  
.16 215.16 .480E+02 .2 .44 4.64  
.19 215.19 .598E+02 .2 .50 4.07  
.22 215.22 .724E+02 .3 .56 3.64  
.25 215.25 .857E+02 .4 .62 3.30  
.28 215.28 .997E+02 .5 .68 3.03  
.32 215.32 .114E+03 .7 .73 2.80  
.35 215.35 .130E+03 .8 .78 2.61  
.38 215.38 .146E+03 1.0 .84 2.45

Page 13

ADD HYD (0103) |  
1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0113): 4.82 .071 .75 4.12  
+ ID2= 2 (0109): 1.40 .036 .67 5.78  
=====  
ID = 3 (0103): 6.22 .106 .75 4.49

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106) |  
1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0117): 5.85 .191 .50 14.19  
+ ID2= 2 (0103): 6.22 .106 .75 4.49  
=====  
ID = 3 (0106): 12.07 .248 .58 9.19

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 3 \*\*  
\*\*\*\*\*  
| MASS STORM | Filename: C:\visual otthymo files\4456\AES 1-hr.mst  
| Ptotal= 35.80 mm | Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=1  
Duration of storm = 1.00 hrs  
Mass curve time step = 5.00 min  
TIME RAIN TIME RAIN TIME RAIN TIME RAIN  
hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr  
.08 15.94 .33 111.27 .58 17.66 .83 1.29  
.17 47.73 .42 102.29 .67 7.35 .92 .47  
.25 79.52 .50 43.00 .75 3.05 1.00 .04  
  
| CALIB | STANDHYD (0115) | Area (ha)= .83  
Page 14

Pre-Dev-Con-AES  
| ID= 1 DT= 5.0 min | Total Imp(%)= 33.00 Dir. Conn.()%= 19.00  
IMPERVIOUS PERVIOUS (i)  
Surface Area (ha)= .27 .55  
Dep. Storage (mm)= 1.00 2.00  
Average Slope (%)= 2.00 3.00  
Length (m)= 74.30 275.00  
Mannings n = .013 .250  
Max.Eff.Inten.(mm/hr)= 111.27 43.12  
over (min) 5.00 30.00  
Storage Coeff. (min)= 1.66 (ii) 29.48 (ii)  
Unit Hyd. Tpeak (min)= 5.00 30.00  
Unit Hyd. peak (cms)= .32 .04  
\*TOTALS\*

PEAK FLOW (cms)= .05 .04 .055 (iii)  
TIME TO PEAK (hrs)= .33 .83 .42  
RUNOFF VOLUME (mm)= 34.80 18.57 21.63  
TOTAL RAINFALL (mm)= 35.80 35.80 35.80  
RUNOFF COEFFICIENT = .97 .52 .60

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN<sup>e</sup> = 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0116) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

TRAVEL TIME TABLE  
<---- DATA FOR SECTION ( 1.1 ) ----->  
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV. TIME  
(m) (m) (cu.m.) (cms) (m/s) (min)  
.03 215.03 .676E+01 .0 .13 33.24  
.06 215.06 .150E+02 .0 .21 19.61  
.09 215.09 .248E+02 .0 .29 14.23  
.13 215.13 .360E+02 .1 .37 11.28  
.16 215.16 .488E+02 .1 .44 9.41  
.19 215.19 .630E+02 .1 .51 8.11  
.22 215.22 .787E+02 .2 .58 7.15  
.25 215.25 .935E+02 .2 .65 6.41  
.28 215.28 .115E+03 .3 .72 5.83  
.32 215.32 .135E+03 .4 .78 5.35  
.35 215.35 .157E+03 .5 .84 4.95  
.38 215.38 .180E+03 .6 .90 4.62  
.41 215.41 .205E+03 .8 .96 4.33  
.44 215.44 .231E+03 .9 .102 4.09  
.47 215.47 .258E+03 1.1 .108 3.87  
.51 215.51 .288E+03 1.3 .113 3.68  
.54 215.54 .318E+03 1.5 .119 3.51

Page 15

Pre-Dev-Con-AES  
.57 215.57 .350E+03 1.7 1.24 3.35  
.60 215.60 .384E+03 2.0 1.30 3.22  
<---- hydrograph ----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0115)	.83	.06	.42	21.63	.13
OUTFLOW : ID= 1 (0116)	.83	.04	.50	21.48	.11

| CALIB | STANDHYD (0107) | Area (ha)= 3.63  
| ID= 1 DT= 5.0 min | Total Imp(%)= 29.40 Dir. Conn.()%= 19.00  
IMPERVIOUS PERVIOUS (i)  
Surface Area (ha)= 1.07 2.56  
Dep. Storage (mm)= 1.00 3.00  
Average Slope (%)= 2.00 3.00  
Length (m)= 155.30 440.00  
Mannings n = .013 .250

Max.Eff.Inten.(mm/hr)= 111.27 21.90  
over (min) 5.00 55.00  
Storage Coeff. (min)= 2.59 (ii) 50.95 (ii)  
Unit Hyd. Tpeak (min)= 5.00 55.00  
Unit Hyd. peak (cms)= .29 .02  
\*TOTALS\*  
PEAK FLOW (cms)= .20 .09 .208 (iii)  
TIME TO PEAK (hrs)= .33 1.25 .42  
RUNOFF VOLUME (mm)= 34.80 15.93 19.19  
TOTAL RAINFALL (mm)= 35.80 35.80 35.80  
RUNOFF COEFFICIENT = .97 .44 .54

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
CN<sup>e</sup> = 86.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0110) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

TRAVEL TIME TABLE  
<---- DATA FOR SECTION ( 1.1 ) ----->  
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV. TIME  
(m) (m) (cu.m.) (cms) (m/s) (min)  
.03 215.03 .947E+01 .0 .15 38.53  
.06 215.06 .210E+02 .0 .25 23.36  
.09 215.09 .347E+02 .0 .34 17.30

Page 16

Pre-Dev-Con-AES

.13	215.13	.504E+02	.1	.42	13.94
.16	215.16	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.132E+03	.3	.71	8.23
.28	215.28	.161E+03	.4	.78	6.95
.32	215.32	.189E+03	.5	.84	6.35
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.252E+03	.7	.96	6.05
.41	215.41	.286E+03	.8	1.02	5.70
.44	215.44	.323E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.403E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

INFLOW : ID= 2 (0107) 3.63 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
OUTFLOW: ID= 1 (0110) 3.63 (.ha) (.cms) (hrs) (mm) (m) (m/s)

ADD HYD (0114)  
1 + 2 = 3  
ID1= 1 (0116): .83 .040 .50 21.48  
+ ID2= 2 (0110): .363 .161 .42 19.47  
ID = 3 (0114): 4.45 .199 .50 19.84

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102) Area (ha)= 1.39 Curve Number (CN)= 84.0  
ID= 1 DT=10.0 min Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----				
TIME	RAIN	TIME	RAIN	TIME
hrs	mm/hr	hrs	mm/hr	hrs
.167	31.83	.500	72.65	.833
.333	95.39	.667	12.30	1.000
				.26

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .086 (i)  
TIME TO PEAK (hrs)= .667  
RUNOFF VOLUME (mm)= 12.441  
TOTAL RAINFALL (mm)= 35.800  
RUNOFF COEFFICIENT = .348

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 17

Pre-Dev-Con-AES

ROUTE CHN (0111) IN= 2--> OUT= 1 Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

<----- TRAVEL TIME TABLE ----->  
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
(m) (m) (cu.m.) (cms) (m/s) (min)  
.03 215.03 .541E+01 .0 .15 22.38  
.06 215.06 .120E+02 .0 .25 13.54  
.09 215.09 .198E+02 .0 .33 10.01  
.13 215.13 .288E+02 .1 .41 8.05  
.16 215.16 .390E+02 .1 .49 6.79  
.19 215.19 .504E+02 .1 .56 5.91  
.22 215.22 .630E+02 .2 .63 5.25  
.25 215.25 .757E+02 .2 .70 4.44  
.28 215.28 .917E+02 .4 .77 4.33  
.32 215.32 .108E+03 .4 .83 4.00  
.35 215.35 .125E+03 .6 .90 3.72  
.38 215.38 .144E+03 .7 .96 3.48  
.41 215.41 .164E+03 .8 1.02 3.28  
.44 215.44 .185E+03 1.0 1.08 3.10  
.47 215.47 .207E+03 1.2 1.13 2.94  
.51 215.51 .230E+03 1.4 1.19 2.80  
.54 215.54 .255E+03 1.6 1.24 2.68  
.57 215.57 .280E+03 1.8 1.30 2.57  
.60 215.60 .307E+03 2.1 1.35 2.47

<--- hydrograph ---> <-pipe / channel->  
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (.cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0107) 4.82 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
OUTFLOW: ID= 1 (0110) 4.82 (.ha) (.cms) (hrs) (mm) (m) (m/s)

<----- TRAVEL TIME TABLE ----->  
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
(m) (m) (cu.m.) (cms) (m/s) (min)  
.03 215.03 .785E+01 .0 .14 14.38  
.06 215.06 .170E+02 .0 .23 8.87  
.09 215.09 .266E+02 .1 .31 6.68  
.13 215.13 .369E+02 .1 .38 5.45  
.16 215.16 .480E+02 .2 .44 4.64  
.19 215.19 .598E+02 .2 .50 4.07  
.22 215.22 .724E+02 .3 .56 3.64  
.25 215.25 .857E+02 .4 .62 3.30  
.28 215.28 .997E+02 .5 .68 3.03  
.32 215.32 .114E+03 .7 .73 2.80  
.35 215.35 .130E+03 .8 .78 2.61  
.38 215.38 .146E+03 1.0 .84 2.45  
.41 215.41 .163E+03 1.2 .89 2.31  
.44 215.44 .181E+03 1.4 .94 2.18  
.47 215.47 .199E+03 1.6 .99 2.08  
.51 215.51 .218E+03 1.8 1.04 1.98  
.54 215.54 .238E+03 2.1 1.08 1.89  
.57 215.57 .259E+03 2.4 1.13 1.81  
.60 215.60 .280E+03 2.7 1.18 1.74

<--- hydrograph ---> <-pipe / channel->  
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (.cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0102) 1.39 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
OUTFLOW: ID= 1 (0111) 1.39 (.ha) (.cms) (hrs) (mm) (m) (m/s)

ADD HYD (0117)  
1 + 2 = 3  
ID1= 1 (0114): 4.45 .199 .50 19.84  
+ ID2= 2 (0111): 1.39 .077 .67 12.36  
ID = 3 (0117): 5.85 .247 .50 18.00

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0105) Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= .522

Page 18

Pre-Dev-Con-AES

PEAK FLOW (cms)= .108 (i)
TIME TO PEAK (hrs)= .667
RUNOFF VOLUME (mm)= 5.850
TOTAL RAINFALL (mm)= 35.800
RUNOFF COEFFICIENT = .163

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Pre-Dev-Con-AES

TOTAL RAINFALL (mm)= 35.800  
RUNOFF COEFFICIENT = .226

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0109) IN= 2--> OUT= 1 Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.60 .0500 / .0500 Main Channel  
3.80 215.60 .0500 / .0500 Main Channel  
5.60 215.60 .0500

<----- TRAVEL TIME TABLE ----->  
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
(m) (m) (cu.m.) (cms) (m/s) (min)  
.03 215.03 .835E+01 .0 .14 14.38  
.06 215.06 .170E+02 .0 .23 8.87  
.09 215.09 .266E+02 .1 .31 6.68  
.13 215.13 .369E+02 .1 .38 5.45  
.16 215.16 .480E+02 .2 .44 4.64  
.19 215.19 .598E+02 .2 .50 4.07  
.22 215.22 .724E+02 .3 .56 3.64  
.25 215.25 .857E+02 .4 .62 3.30  
.28 215.28 .997E+02 .5 .68 3.03  
.32 215.32 .114E+03 .7 .73 2.80  
.35 215.35 .130E+03 .8 .78 2.61  
.38 215.38 .146E+03 1.0 .84 2.45  
.41 215.41 .163E+03 1.2 .89 2.31  
.44 215.44 .181E+03 1.4 .94 2.18  
.47 215.47 .199E+03 1.6 .99 2.08  
.51 215.51 .218E+03 1.8 1.04 1.98  
.54 215.54 .238E+03 2.1 1.08 1.89  
.57 215.57 .259E+03 2.4 1.13 1.81  
.60 215.60 .280E+03 2.7 1.18 1.74

<--- hydrograph ---> <-pipe / channel->  
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (.cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0112) 4.82 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
OUTFLOW: ID= 1 (0109) 4.82 (.ha) (.cms) (hrs) (mm) (m) (m/s)

ADD HYD (0103)  
1 + 2 = 3  
ID1= 2 (0113): 4.82 .10 .75 5.83  
+ ID2= 1 (0109): 1.40 .052 .67 8.07  
ID = 3 (0103): 6.22 .151 .75 6.33

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0112) Area (ha)= 1.40 Curve Number (CN)= 75.0  
ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .055 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 8.105

Page 19

Pre-Dev-Con-AES

Page 20

Pre-Dev-Con-AES

ADD HYD (0106)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0117)		5.85	.247	.50	18.06
+ ID2= 2 (0103)		6.22	.151	.75	6.33
ID = 3 (0106):		12.07	.347	.67	12.01

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 4 \*\*  
\*\*\*\*\*

MASS STORM Ptotal= 42.50 mm	Filename: C:\visual otthymo files\4456\AES 1-hr.mst				
Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=					
Duration of storm = 1.00 hrs					
Mass curve time step = 5.00 min					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm hr
.08	18.92	.33	132.09	.58	20.96
.17	56.66	.42	121.43	.67	8.72
.25	94.40	.50	51.05	.75	3.62
1.00				1.00	.05

CALIB STANDHYD (0115)	Area (ha)= .83	Total Imp(%)= 33.00	Dir. Conn.(%)= 19.00
IMPERVIOUS PERVIOUS (i)			
Surface Area (ha)= .27	.55		
Dep. Storage (mm)= 1.00	2.00		
Average Slope (%)= 2.00	3.00		
Length (m)= 74.30	275.00		
Mannings n = .013	.230		
Max.Eff.Inten.(mm/hr)= 132.09	64.88		
over (min)= 5.00	30.00		
Storage Coeff. (min)= 1.55 (ii)	25.18 (ii)		
Unit Hyd. Tpeak (min)= 5.00	30.00		
Unit Hyd. peak (cms)= .33	.04		
*TOTALS*			
PEAK FLOW (cms)= .06	.05	.069	(iii)
TIME TO PEAK (hrs)= .33	.83	.42	
RUNOFF VOLUME (mm)= 41.50	24.00	27.31	
TOTAL RAINFALL (mm)= 42.50	42.50	42.50	
RUNOFF COEFFICIENT = .98	.56	.64	

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 $CN^* = 88.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 21

Pre-Dev-Con-AES

ROUTE CHN (0116)	IN= 2--> OUT= 1	Routing time step (min)'= 5.00		
<---- DATA FOR SECTION ( 1.1 ) ---->				
Distance .00	Elevation 215.60	Manning .0500		
1.80	215.00	.0500 / .0500 Main Channel	2.56	215.00 .0500 / .0500 Main Channel
4.36	215.60	.0500		
<---- hydrograph ----> <-pipe / channel->				
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)
.03	215.03	.676E+01	.0	.13
.06	215.06	.947E+01	.0	.21
.09	215.09	.210E+02	.0	.29
.13	215.13	.360E+02	.1	.37
.16	215.16	.488E+02	.1	.44
.19	215.19	.630E+02	.1	.51
.22	215.22	.787E+02	.2	.58
.25	215.25	.960E+02	.2	.65
.28	215.28	.115E+03	.3	.72
.32	215.32	.135E+03	.4	.78
.35	215.35	.157E+03	.5	.84
.38	215.38	.180E+03	.6	.90
.41	215.41	.203E+03	.8	.96
.44	215.44	.225E+03	.9	1.02
.47	215.47	.258E+03	1.1	1.08
.51	215.51	.288E+03	1.3	1.13
.54	215.54	.318E+03	1.5	1.19
.57	215.57	.350E+03	1.7	1.24
.60	215.60	.384E+03	2.0	1.30

INFLOW : ID= 2 (0115)	Area (ha)= .83	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
OUTFLOW: ID= 1 (0116)		.05	.83	27.31	.14	.40

CALIB STANDHYD (0107)	Area (ha)= 3.63	Total Imp(%)= 29.40	Dir. Conn.(%)= 19.00
IMPERVIOUS PERVIOUS (i)			
Surface Area (ha)= 1.97	2.56		
Dep. Storage (mm)= 1.00	3.00		
Average Slope (%)= 3.00	3.00		
Length (m)= 155.50	440.00		
Mannings n = .013	.250		
Max.Eff.Inten.(mm/hr)= 132.09	35.82		
over (min)= 5.00	45.00		
Storage Coeff. (min)= 2.42 (ii)	42.14 (ii)		
Unit Hyd. Tpeak (min)= 5.00	45.00		
Unit Hyd. peak (cms)= .30	.03		
*TOTALS*			
PEAK FLOW (cms)= .24	.14	.257	(iii)
TIME TO PEAK (hrs)= .33	1.08	.42	

Page 22

Pre-Dev-Con-AES

RUNOFF VOLUME (mm)= 41.50	20.95	24.85
TOTAL RAINFALL (mm)= 42.50	42.50	42.50
RUNOFF COEFFICIENT = .98	.49	.58

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 $CN^* = 86.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0110)	IN= 2--> OUT= 1	Routing time step (min)'= 5.00		
<---- DATA FOR SECTION ( 1.1 ) ---->				
Distance .00	Elevation 215.60	Manning .0500		
1.80	215.00	.0500 / .0500 Main Channel	2.56	215.00 .0500 / .0500 Main Channel
4.36	215.60	.0500		
<---- TRAVEL TIME TABLE ---->				
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)
.03	215.03	.947E+01	.0	.15
.06	215.06	.210E+02	.0	.25
.09	215.09	.504E+02	.0	.34
.13	215.13	.104E+02	.1	.42
.16	215.16	.168E+02	.1	.50
.19	215.19	.288E+02	.1	.57
.22	215.22	.410E+03	.2	.64
.25	215.25	.134E+03	.3	.71
.28	215.28	.161E+03	.4	.78
.32	215.32	.189E+03	.5	.84
.35	215.35	.219E+03	.6	.90
.38	215.38	.252E+03	.7	.96
.41	215.41	.286E+03	.8	1.02
.44	215.44	.320E+03	1.0	1.08
.47	215.47	.362E+03	1.2	1.14
.51	215.51	.403E+03	1.4	1.20
.54	215.54	.446E+03	1.6	1.25
.57	215.57	.491E+03	1.8	1.30
.60	215.60	.538E+03	2.1	1.36

ADD HYD (0114)	1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0116):		.83	.054	.83	27.10

Page 23

Pre-Dev-Con-AES

+ ID2= 2 (0110):	3.63	.204	.42	24.82	
ID = 3 (0114):		4.45	.254	.50	25.25

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102)	Area (ha)= 1.39	Curve Number (CN)= 84.0
ID= 1 DT=10.0 min	Ia (mm)= 4.00	# of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .24		

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

<---- TRANSFORMED HYETOGRAPH ---->					
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.167	.37.79	.500	.86.24	.833	.25.58
.333	113.25	.667	14.84	1.000	.31

ROUTE CHN (0111)	IN= 2--> OUT= 1	Routing time step (min)'= 5.00		
<---- DATA FOR SECTION ( 1.1 ) ---->				
Distance .00	Elevation 215.60	Manning .0500		
3.00	215.00	.0500 / .0500 Main Channel	3.76	215.00 .0500 / .0500 Main Channel
5.56	215.60	.0500		
<---- TRAVEL TIME TABLE ---->				
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)
.03	215.03	.701E+01	.0	.18
.06	215.06	.160E+02	.0	.29
.09	215.09	.320E+02	.0	.39
.13	215.13	.400E+02	.1	.48
.16	215.16	.550E+02	.1	.56
.19	215.19	.720E+02	.2	.64
.22	215.22	.900E+02	.3	.72
.25	215.25	.112E+03	.4	.79
.28	215.28	.135E+03	.5	.86
.32	215.32	.160E+03	.6	.93
.35	215.35	.187E+03	.7	.99
.38	215.38	.216E+03	.9	1.05
.41	215.41	.247E+03	1.1	1.12
.44	215.44	.280E+03	1.3	1.17
.47	215.47	.314E+03	1.6	1.23
.51	215.51	.351E+03	1.8	1.29

Page 24

Pre-Dev-Con-AES						
.54	215.54	.390E+03	2.1	1.35	3.09	
.57	215.57	.431E+03	2.4	1.40	2.97	
.60	215.60	.474E+03	2.8	1.46	2.86	
<---- hydrograph ----> <-pipe / channel->						
AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL	
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)	
ID1= 1 (0114):	4.45	.254	.50	25.25		
+ ID2= 2 (0111):	1.39	.106	.67	16.76	.15	.55
INFLOW: ID= 2 (0102)	1.39	.11	.67	16.76	.15	.53
OUTFLOW: ID= 1 (0111)	1.39					

ADD HYD (0117)			
1 + 2 = 3	AREA	QPEAK	TPEAK
(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0114):	4.45	.254	.50
+ ID2= 2 (0111):	1.39	.106	.67
ID = 3 (0117):	5.85	.326	.50
			23.22

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0105)		
Area (ha)=	4.82	Curve Number (CN)= 66.0
Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hr)=	.35	
Unit Hyd Qpeak (cms)=	.522	
PEAK FLOW (cms)=	.153 (i)	
TIME TO PEAK (hrs)=	.667	
RUNOFF VOLUME (mm)=	8.327	
TOTAL RAINFALL (mm)=	42.500	
RUNOFF COEFFICIENT =	.196	

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0113)					
IN= 2--> OUT= 1	Routing time step (min)'= 5.00				
<---- DATA FOR SECTION ( 1.1 ) ----->					
Distance	Elevation	Manning			
.00	215.60	.0500			
1.80	215.00	.0500 / .0500 Main Channel			
2.56	215.00	.0500 / .0500 Main Channel			
4.36	215.60	.0500			
<---- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.541E+01	.0	.15	22.38
.06	215.06	.120E+02	.0	.25	13.54
.09	215.09	.198E+02	.0	.33	10.01
.13	215.13	.288E+02	.1	.41	8.05
.16	215.16	.390E+02	.1	.49	6.79
.19	215.19	.504E+02	.1	.56	5.91
.22	215.22	.630E+02	.2	.63	5.25

Page 25

Pre-Dev-Con-AES						
.25	215.25	.768E+02	.3	.70	4.74	
.28	215.28	.917E+02	.4	.77	4.33	
.32	215.32	.108E+03	.4	.83	4.00	
.35	215.35	.125E+03	.6	.90	3.72	
.38	215.38	.140E+03	.7	.96	3.48	
.41	215.41	.164E+03	.8	1.02	3.28	
.44	215.44	.185E+03	1.0	1.08	3.10	
.47	215.47	.207E+03	1.2	1.13	2.94	
.51	215.51	.230E+03	1.4	1.19	2.80	
.54	215.54	.255E+03	1.6	1.24	2.68	
.57	215.57	.280E+03	1.8	1.30	2.57	
.60	215.60	.307E+03	2.1	1.35	2.47	

<---- hydrograph ----> <-pipe / channel->						
AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL	
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)	
INFLOW : ID= 2 (0105)	4.82	.15	.67	8.33	.20	.58
OUTFLOW: ID= 1 (0113)	4.82	.15	.75	8.30	.19	.57

CALIB NASHYD (0112)						
ID= 1 DT=10.0 min	Area (ha)=	1.40	Curve Number (CN)= 75.0			
Ia (mm)=	5.00	# of Linear Res.(N)= 3.00				
U.H. Tp(hr)=	.24					

Unit Hyd Qpeak (cms)= .222  
 PEAK FLOW (cms)= .078 (i)  
 TIME TO PEAK (hrs)= .500  
 RUNOFF VOLUME (mm)= 11.357  
 TOTAL RAINFALL (mm)= 42.500  
 RUNOFF COEFFICIENT = .267

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0109)					
IN= 2--> OUT= 1	Routing time step (min)'= 5.00				
<---- DATA FOR SECTION ( 1.1 ) ----->					
Distance	Elevation	Manning			
.00	215.60	.0500			
1.80	215.00	.0500 / .0500 Main Channel			
2.56	215.00	.0500 / .0500 Main Channel			
4.36	215.60	.0500			
<---- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.170E+02	.0	.23	8.87
.09	215.09	.266E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.857E+02	.4	.62	3.30
.28	215.28	.997E+02	.5	.68	3.03
.32	215.32	.114E+03	.7	.73	2.80
.35	215.35	.130E+03	.8	.78	2.61

Page 26

Pre-Dev-Con-AES						
.38	215.38	.146E+03	1.0	.84	2.45	
.41	215.41	.163E+03	1.2	.89	2.31	
.44	215.44	.181E+03	1.4	.94	2.18	
.47	215.47	.199E+03	1.6	.99	2.08	
.51	215.51	.218E+03	1.8	1.04	1.98	
.54	215.54	.238E+03	2.1	1.08	1.89	
.57	215.57	.259E+03	2.4	1.13	1.81	
.60	215.60	.280E+03	2.7	1.18	1.74	
<---- hydrograph ----> <-pipe / channel->						
AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL	
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)	
ID1= 2 (0112)	1.40	.08	.50	11.36	.10	.32
OUTFLOW: ID= 1 (0109)	1.40	.07	.67	11.31	.10	.32

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0103)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
(ha)	(cms)	(hrs)	(mm)	
ID1= 1 (0113):	4.82	.147	.75	8.30
+ ID2= 2 (0109):	1.40	.075	.67	11.31
ID = 3 (0103):	6.22	.216	.75	8.98

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Pre-Dev-Con-AES						
STANDHYD (0115)	Area (ha)=	.83	Total Imp(%)= 33.00	Dir. Conn.(%)= 19.00		
IMPERVIOUS PERVIOUS (i)						
Surface Area (ha)=	.27	.55				
Dep. Storage (mm)=	1.00	2.00				
Average Slope (%)=	2.00	3.00				
Length (m)=	74.30	275.00				
Mannings n =	.013	.250				
Max.Eff.Inten.(mm/hr)=	147.32	75.84				
over (min)=	5.00	25.00				
Storage Coeff. (min)=	1.49 (ii)	23.68 (ii)				
Unit Hyd. Tpeak (min)=	5.00	25.00				
Unit Hyd. peak (cms)=	.33	.05				
*TOTALS*						
PEAK FLOW (cms)=	.06	.07				
TIME TO PEAK (hrs)=	.33	.75				
RUNOFF VOLUME (mm)=	46.40	28.13				
TOTAL RAINFALL (mm)=	47.40	47.40				
RUNOFF COEFFICIENT =	.98	.59				

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 88.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0116)					
IN= 2--> OUT= 1	Routing time step (min)'= 5.00				
<---- DATA FOR SECTION ( 1.1 ) ----->					
Distance	Elevation	Manning			
.00	215.60	.0500			
1.80	215.00	.0500 / .0500 Main Channel			
2.56	215.00	.0500 / .0500 Main Channel			
4.36	215.60	.0500			
<---- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.676E+01	.0	.13	33.24
.06	215.06	.150E+02	.0	.21	19.61
.09	215.09	.248E+02	.0	.29	14.23
.13	215.13	.360E+02	.1	.37	11.28
.16	215.16	.488E+02	.1	.44	9.41
.19	215.19	.630E+02	.1	.51	8.11
.22	215.22	.760E+02	.2	.58	7.15
.25	215.25	.960E+02	.2	.65	6.41
.28	215.28	.115E+03	.3	.72	5.83
.32	215.32	.135E+03	.4	.78	5.35
.35	215.35	.157E+03	.5	.84	4.95
.38	215.38	.180E+03	.6	.90	4.62
.41	215.41	.205E+03	.8	.96	4.33
.44	215.44	.231E+03	.9	1.02	4.09
.47	215.47	.258E+03	1.1	1.08	3.87
.51	215.51	.288E+03	1.3	1.13	3.68

Page 28

CALIB						
** SIMULATION NUMBER: 5 **						
MASS STORM Filename: C:\visual otthymo files\4456\AES 1-hr.mst						
Pttotal= 47.40 mm Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=						
Duration of storm = 1.00 hrs Mass curve time step = 5.00 min						
TIME RAIN TIME RAIN TIME RAIN TIME RAIN						
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs
.08	21.10	.33	147.32	.58	23.38	.83
.17	63.19	.42	135.43	.67	9.73	.92
.25	105.28	.50	56.94	.75	4.04	.06

Page 27

Pre-Dev-Con-AES

.54	215.54	.318E+03	1.5	1.19	3.51
.57	215.57	.350E+03	1.7	1.24	3.35
.60	215.60	.384E+03	2.0	1.30	3.22

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
.83	.08	.42	31.59	.16	.44

INFLOW : ID= 2 (0115) .83 .08 .42 31.59 .16 .44  
OUTFLOW: ID= 1 (0116) .83 .07 .75 31.37 .14 .40

CALIB STANDHYD (0107) | Area (ha)= 3.63  
ID= 1 DT= 5.0 min | Total Imp(%)= 29.40 dir. Conn.(%)= 19.00  
IMPERVIOUS PERVIOUS (i)  
Surface Area (ha)= 1.07 2.56  
Dep. Storage (mm)= 1.00 3.00  
Average Slope (%)= 2.00 3.00  
Length (m)= 155.50 440.00  
Mannings n = .013 .250  
Max.Eff.Inten.(mm/hr)= 147.32 42.43  
over (mm)= 5.00 40.00  
Storage Coeff. (min)= 2.32 (ii) 39.44 (ii)  
Unit Hyd. Peak (min)= 5.00 40.00  
Unit Hyd. peak (cms)= .30 .03  
\*TOTALS\*  
PEAK FLOW (cms)= .27 .18 .295 (iii)  
TIME TO PEAK (hrs)= .33 1.00 .42  
RUNOFF VOLUME (mm)= 46.40 24.82 28.91  
TOTAL RAINFALL (mm)= 47.40 47.40 47.40  
RUNOFF COEFFICIENT = .98 .52 .61

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN<sup>2</sup> = 86.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0110) | Routing time step (min)'= 5.00  
<---- DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500  
  
<---- TRAVEL TIME TABLE ----->  
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
(m) (m) (cu.m.) (cms) (m/s) (min)  
.03 215.03 .947E+01 .0 .15 38.53  
.06 215.06 .210E+02 .0 .25 23.36

Page 29

ADD HYD (0117) |  
1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0114): 4.45 .301 .50 29.34  
+ ID2= 2 (0111): 1.39 .129 .67 20.16  
ID = 3 (0117): 5.85 .393 .50 27.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .35

Page 31

Pre-Dev-Con-AES

.09	215.09	.347E+02	.0	.34	17.30
.13	215.13	.504E+02	.1	.42	13.94
.16	215.16	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.108E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23
.28	215.28	.161E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.252E+03	.7	.96	6.05
.41	215.41	.286E+03	.8	1.02	5.70
.44	215.44	.323E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.403E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
3.63	.29	.42	28.91	.26	.73

INFLOW : ID= 2 (0107) 3.63 .29 .42 28.91 .26 .73  
OUTFLOW: ID= 1 (0110) 3.63 .24 .42 28.88 .24 .67

ADD HYD (0114) |  
1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0116): .83 .070 .75 31.37  
+ ID2= 2 (0110): 3.63 .236 .42 28.88  
ID = 3 (0114): 4.45 .301 .50 29.34

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
ID= 1 DT=10.0 min | Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.167	42.15	.500	96.18	.833	2.87
.333	126.30	.667	16.55	1.000	.34

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .141 (i)  
TIME TO PEAK (hrs)= .500  
RUNOFF VOLUME (mm)= 20.244  
TOTAL RAINFALL (mm)= 47.400  
RUNOFF COEFFICIENT = .427

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.  
Page 30

Pre-Dev-Con-AES

Unit Hyd Qpeak (cms)= .522  
PEAK FLOW (cms)= .190 (i)  
TIME TO PEAK (hrs)= .667  
RUNOFF VOLUME (mm)= 10.345  
TOTAL RAINFALL (mm)= 47.400  
RUNOFF COEFFICIENT = .218

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0113) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

<---- TRAVEL TIME TABLE ----->  
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
(m) (m) (cu.m.) (cms) (m/s) (min)  
.03 215.03 .701E+01 .0 .18 22.93  
.06 215.06 .160E+02 .0 .29 14.14  
.09 215.09 .270E+02 .0 .39 10.61  
.12 215.12 .400E+02 .1 .48 8.65  
.16 215.16 .550E+02 .1 .56 7.38  
.19 215.19 .720E+02 .2 .64 6.48  
.22 215.22 .909E+02 .3 .72 5.80  
.25 215.25 .112E+03 .4 .79 5.27  
.28 215.28 .135E+03 .5 .86 4.85  
.32 215.32 .160E+03 .6 .93 4.50  
.35 215.35 .187E+03 .7 .99 4.21  
.38 215.38 .216E+03 .9 1.05 3.95  
.41 215.41 .247E+03 1.1 1.12 3.74  
.44 215.44 .280E+03 1.3 1.17 3.55  
.47 215.47 .314E+03 1.6 1.23 3.38  
.51 215.51 .353E+03 1.8 1.29 3.23  
.54 215.54 .390E+03 2.1 1.35 3.09  
.57 215.57 .431E+03 2.4 1.40 2.97  
.60 215.60 .474E+03 2.8 1.46 2.86

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
4.82	.19	.67	10.34	.22	.62

INFLOW : ID= 2 (0105) 4.82 .19 .67 10.34 .22 .62  
OUTFLOW: ID= 1 (0113) 4.82 .18 .75 10.32 .21 .61

CALIB NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222  
PEAK FLOW (cms)= .096 (i)  
TIME TO PEAK (hrs)= .500

Page 32

## Pre-Dev-Con-AES

RUNOFF VOLUME (mm)= 13.959  
 TOTAL RAINFALL (mm)= 47.400  
 RUNOFF COEFFICIENT = .294

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0109) | IN= 2--> OUT= 1 Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 3.80 215.00 .0500 Main Channel  
 5.60 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .813E+01 .0 .14 14.28  
 .06 215.06 .170E+02 .0 .23 8.87  
 .09 215.09 .266E+02 .1 .31 6.68  
 .13 215.13 .369E+02 .1 .38 5.45  
 .16 215.16 .480E+02 .2 .44 4.64  
 .19 215.19 .598E+02 .2 .50 4.07  
 .22 215.22 .717E+02 .3 .56 3.64  
 .25 215.25 .857E+02 .4 .62 3.30  
 .28 215.28 .997E+02 .5 .68 3.03  
 .32 215.32 .114E+03 .7 .73 2.80  
 .35 215.35 .130E+03 .8 .78 2.61  
 .38 215.38 .146E+03 1.0 .84 2.45  
 .41 215.41 .163E+03 1.2 .89 2.31  
 .44 215.44 .181E+03 1.4 .94 2.18  
 .47 215.47 .199E+03 1.6 .99 2.08  
 .51 215.51 .218E+03 1.8 1.04 1.98  
 .54 215.54 .238E+03 2.1 1.08 1.89  
 .57 215.57 .259E+03 2.4 1.13 1.81  
 .60 215.60 .280E+03 2.7 1.18 1.74

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0112) 1.40 .10 .50 13.96 .11 .35  
 OUTFLOW: ID= 1 (0109) 1.40 .09 .67 13.92 .11 .34

| ADD HYD (0103) |  
 1 + 2 = 3  
 AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0113): 4.82 .183 .75 10.32  
 + ID2= 2 (0109): 1.40 .091 .67 13.92  
 ID = 3 (0103): 6.22 .267 .75 11.13

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

## Pre-Dev-Con-AES

ADD HYD (0106)			AREA	QPEAK	TPEAK	R.V.	
1	+	2	= 3	(ha)	(cms)	(hrs)	(mm)
			ID1= 1 (0117):	5.85	.393	.50	27.16
			+ ID2= 2 (0103):	6.22	.267	.75	11.13
			ID = 3 (0106):	12.07	.616	.67	18.90

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
 \*\* SIMULATION NUMBER: 6 \*\*  
 \*\*\*\*\*

| MASS STORM Ptotal= 52.40 mm | Filename: C:\visual otthymo files\4456\AES 1-hr.mst  
 Comments: AES 1 HOUR STORM DISTRIBUTION a=21min k=

DURATION OF STORM = 1.00 hrs  
 MASS CURVE TIME STEP = 5.00 min  

TIME	RAIN	TIME	RAIN	TIME	RAIN	
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	
.08	23.33	.33	162.86	.58	25.84	.83
.17	69.86	.42	149.72	.67	10.75	.92
.25	116.39	.50	62.94	.75	4.46	1.00

| CALIB STANDHYD (0115) | Area (ha)= .83  
 ID= 1 DT= 5.0 min Total Imp(%)= 33.00 Dir. Conn.(%)= 19.00  
 IMPERVIOUS PERVIOUS (i)  
 Surface Area (ha)= .27 .55  
 Dep. Storage (mm)= 1.00 2.00  
 Average Slope (%)= 2.00 3.00  
 Length (m)= 74.30 275.00  
 Mannings n = .013 .250  
 Max.Eff.Inten.(mm/hr)= 162.86 102.33  
 over (min)= 5.00 25.00  
 Storage Coeff. (min)= 1.43 (ii) 21.12 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 25.00  
 Unit Hyd. peak (cms)= .33 .05

\*TOTALS\*  
 PEAK FLOW (cms)= .07 .09 .09 (iii)  
 TIME TO PEAK (hrs)= .33 .75 .42  
 RUNOFF VOLUME (mm)= 51.40 32.43 36.02  
 TOTAL RAINFALL (mm)= 52.40 52.40 52.40  
 RUNOFF COEFFICIENT = .98 .62 .69

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN<sup>n</sup> = 88.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 34

Page 33

## Pre-Dev-Con-AES

| ROUTE CHN (0116) | IN= 2--> OUT= 1 Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.00 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .676E+01 .0 .13 33.24  
 .06 215.06 .150E+02 .0 .21 19.61  
 .09 215.09 .248E+02 .0 .29 14.23  
 .13 215.13 .347E+02 .1 .37 11.28  
 .16 215.16 .448E+02 .1 .44 9.11  
 .19 215.19 .630E+02 .1 .51 8.11  
 .22 215.22 .787E+02 .2 .58 7.15  
 .25 215.25 .960E+02 .2 .65 6.41  
 .28 215.28 .115E+03 .3 .72 5.83  
 .32 215.32 .135E+03 .4 .78 5.35  
 .35 215.35 .157E+03 .5 .84 4.95  
 .38 215.38 .180E+03 .6 .90 4.62  
 .41 215.41 .205E+03 .8 .96 4.33  
 .44 215.44 .231E+03 .9 1.02 4.09  
 .47 215.47 .258E+03 1.1 1.08 3.87  
 .51 215.51 .285E+03 1.3 1.15 3.68  
 .54 215.54 .318E+03 1.5 1.19 3.51  
 .57 215.57 .350E+03 1.7 1.24 3.35  
 .60 215.60 .384E+03 2.0 1.30 3.22

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0115) .83 .10 .42 36.02 .17 .46  
 OUTFLOW: ID= 1 (0116) .83 .09 .75 35.82 .16 .44

| CALIB STANDHYD (0107) | Area (ha)= 3.63 Total Imp(%)= 29.40 Dir. Conn.(%)= 19.00  
 ID= 1 DT= 5.0 min

IMPERVIOUS PERVIOUS (i)  
 Surface Area (ha)= 1.07 2.56  
 Dep. Storage (mm)= 1.00 3.00  
 Average Slope (%)= 2.00 3.00  
 Length (m)= 155.50 440.00  
 Mannings n = .013 .230

Max.Eff.Inten.(mm/hr)= 162.86 55.84  
 over (min)= 5.00 40.00  
 Storage Coeff. (min)= 2.23 (ii) 35.48 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 40.00  
 Unit Hyd. peak (cms)= .30 .03

\*TOTALS\*

Page 35

Pre-Dev-Con-AES  
 TIME TO PEAK (hrs)= .33 1.00 .42  
 RUNOFF VOLUME (mm)= 51.40 28.88 33.15  
 TOTAL RAINFALL (mm)= 52.40 52.40 52.40  
 RUNOFF COEFFICIENT = .98 .55 .63

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN<sup>n</sup> = 86.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0110) | IN= 2--> OUT= 1 Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .947E+01 .0 .15 38.53  
 .06 215.06 .240E+02 .0 .24 23.36  
 .09 215.09 .447E+02 .0 .34 17.30  
 .13 215.13 .504E+02 .1 .42 13.94  
 .16 215.16 .683E+02 .1 .50 11.77  
 .19 215.19 .882E+02 .1 .57 10.25  
 .22 215.22 .110E+03 .2 .64 9.11  
 .25 215.25 .134E+03 .3 .71 8.23  
 .28 215.28 .161E+03 .4 .78 7.53  
 .32 215.32 .189E+03 .5 .84 6.95  
 .35 215.35 .219E+03 .6 .90 6.47  
 .38 215.38 .252E+03 .7 .96 6.05  
 .41 215.41 .289E+03 .8 1.02 5.70  
 .44 215.44 .329E+03 1.0 1.08 5.39  
 .47 215.47 .362E+03 1.2 1.14 5.12  
 .51 215.51 .403E+03 1.4 1.20 4.88  
 .54 215.54 .446E+03 1.6 1.25 4.66  
 .57 215.57 .491E+03 1.8 1.30 4.47  
 .60 215.60 .538E+03 2.1 1.36 4.30

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0107) 3.63 .33 .42 33.15 .28 .75  
 OUTFLOW: ID= 1 (0110) 3.63 .27 .42 33.11 .25 .71

| ADD HYD (0114) |  
 1 + 2 = 3  
 AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)

Page 36

Pre-Dev-Con-AES  
 ID1= 1 (0116): .83 .086 .75 35.82  
 + ID2= 2 (0110): 3.63 .270 .42 33.11  
 ID = 3 (0114): 4.45 .346 .50 33.62

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB  
 NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
 ID= 1 DT=10.0 min | Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TIME RAIN ---- TRANSFORMED HYETOGRAPH ----  
 hrs mm/hr | hrs mm hr | hrs mm/hr | hrs mm hr  
 .167 46.59 | .500 106.33 | .833 3.18  
 .333 139.63 | .667 18.30 | 1.000 .38

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .166 (1)  
 TIME TO PEAK (hrs)= .500  
 RUNOFF VOLUME (mm)= 23.876  
 TOTAL RAINFALL (mm)= 52.400  
 RUNOFF COEFFICIENT = .456

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0111) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1

<---- DATA FOR SECTION ( 1.1) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500 Main Channel  
 3.00 215.00 .0500  
 3.76 215.00 .0500  
 5.56 215.60 .0000

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .701E+01 .0 .18 22.93  
 .06 215.06 .160E+02 .0 .29 10.14  
 .09 215.09 .270E+02 .0 .39 10.61  
 .13 215.13 .400E+02 .1 .48 9.65  
 .16 215.16 .550E+02 .1 .56 9.38  
 .19 215.19 .720E+02 .2 .64 6.48  
 .22 215.22 .909E+02 .3 .72 5.80  
 .25 215.25 .112E+03 .4 .79 5.27  
 .28 215.28 .135E+03 .5 .86 4.85  
 .32 215.32 .160E+03 .6 .93 4.50  
 .35 215.35 .187E+03 .7 .99 4.21  
 .38 215.38 .216E+03 .9 1.05 3.95  
 .41 215.41 .247E+03 1.1 1.12 3.74  
 .44 215.44 .280E+03 1.3 1.17 3.55  
 .47 215.47 .314E+03 1.6 1.23 3.38

Page 37

Pre-Dev-Con-AES  
 .51 215.51 .351E+03 1.8 1.29 3.23  
 .54 215.54 .390E+03 2.1 1.35 3.09  
 .57 215.57 .431E+03 2.4 1.40 2.97  
 .60 215.60 .474E+03 2.8 1.46 2.86

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0102) 1.39 .17 .50 23.88 .18 .62  
 OUTFLOW: ID= 1 (0111) 1.39 .15 .67 23.79 .17 .60

<---- ADD HYD (0117) ---->  
 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 + ID1= 1 (0114): 4.45 .346 .50 33.62  
 + ID2= 2 (0111): 1.39 .153 .67 23.79  
 ID = 3 (0117): 5.85 .459 .50 31.27

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB  
 NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
 ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .231 (i)  
 TIME TO PEAK (hrs)= .667  
 RUNOFF VOLUME (mm)= 12.566  
 TOTAL RAINFALL (mm)= 52.400  
 RUNOFF COEFFICIENT = .240

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0113) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1

<---- DATA FOR SECTION ( 1.1) ---->  
 Distance Elevation Manning  
 .00 215.00 .0500 Main Channel  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.36 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .541E+01 .0 .15 22.38  
 .06 215.06 .120E+02 .0 .25 13.54  
 .09 215.09 .198E+02 .0 .33 10.01  
 .13 215.13 .288E+02 .1 .41 8.05  
 .16 215.16 .390E+02 .1 .49 6.79  
 .19 215.19 .504E+02 .1 .56 5.91

Page 38

Pre-Dev-Con-AES  
 .22 215.22 .630E+02 .2 .63 5.25  
 .25 215.25 .768E+02 .3 .70 4.74  
 .28 215.28 .917E+02 .4 .77 4.33  
 .32 215.32 .108E+03 .4 .83 4.00  
 .35 215.35 .125E+03 .6 .90 3.72  
 .38 215.38 .144E+03 .7 .96 3.48  
 .41 215.41 .164E+03 .8 1.02 3.28  
 .44 215.44 .185E+03 1.0 1.08 3.10  
 .47 215.47 .207E+03 1.2 1.13 2.94  
 .51 215.51 .230E+03 1.4 1.19 2.80  
 .54 215.54 .255E+03 1.6 1.24 2.68  
 .57 215.57 .280E+03 1.8 1.30 2.57  
 .60 215.60 .307E+03 2.1 1.35 2.47

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0105) 4.82 .23 .67 12.57 .24 .66  
 OUTFLOW: ID= 1 (0113) 4.82 .22 .75 12.54 .23 .66

Pre-Dev-Con-AES  
 .35 215.35 .130E+03 .8 .78 2.61  
 .38 215.38 .146E+03 1.0 .84 2.45  
 .41 215.41 .163E+03 1.2 .89 2.31  
 .44 215.44 .181E+03 1.4 .94 2.18  
 .47 215.47 .199E+03 1.6 .99 2.08  
 .51 215.51 .218E+03 1.8 1.04 1.98  
 .54 215.54 .238E+03 2.1 1.08 1.89  
 .57 215.57 .259E+03 2.4 1.13 1.81  
 .60 215.60 .280E+03 2.7 1.18 1.74

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0112) 1.40 .12 .50 16.78 .13 .38  
 OUTFLOW: ID= 1 (0109) 1.40 .11 .67 16.74 .12 .37

<---- ADD HYD (0103) ---->  
 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 + ID1= 1 (0113): 4.82 .223 .75 12.54  
 + ID2= 2 (0109): 1.40 .111 .67 16.74  
 ID = 3 (0103): 6.22 .323 .67 13.48

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

<---- ADD HYD (0106) ---->  
 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 + ID1= 1 (0117): 5.85 .459 .50 31.27  
 + ID2= 2 (0103): 6.22 .323 .67 13.48  
 ID = 3 (0106): 12.07 .741 .67 22.11

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

CALIB  
 NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
 ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .115 (i)  
 TIME TO PEAK (hrs)= .500  
 RUNOFF VOLUME (mm)= 16.785  
 TOTAL RAINFALL (mm)= 52.400  
 RUNOFF COEFFICIENT = .320

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0109) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1

<---- DATA FOR SECTION ( 1.1) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500 Main Channel  
 1.80 215.00 .0500 / .0500 Main Channel  
 3.80 215.00 .0500 Main Channel  
 5.60 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .813E+01 .0 .14 8.49  
 .06 215.06 .170E+02 .0 .23 8.67  
 .09 215.09 .266E+02 .1 .31 6.68  
 .13 215.13 .369E+02 .1 .38 5.45  
 .16 215.16 .480E+02 .2 .44 4.64  
 .19 215.19 .598E+02 .2 .50 4.07  
 .22 215.22 .724E+02 .3 .56 3.64  
 .25 215.25 .857E+02 .4 .62 3.30  
 .28 215.28 .997E+02 .5 .68 3.03  
 .32 215.32 .114E+03 .7 .73 2.80

Page 39

Page 40

## Post-Dev-Con-SCS

```

V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U A A L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLL

000 TTTT TTTT H H Y Y M M 000 TM, Version 2.0
0 0 T T H H Y Y M M 0 0 Licensed To: MJ Davenport
000 T T H H Y M M 000 vo2-0057

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files\visual otthymo v2.0\voin.dat  
output filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Controlled.out  
Summary filename: c:\visual otthymo files\3969\3969-all  
Scenarios\Post-Dev-Controlled.sum

DATE: 1/23/2019 TIME: 2:14:28 PM

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 1 \*\*  
\*\*\*\*\*

MASS STORM	Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst		
Ptotal= 38.40 mm	Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION		
Duration of storm = 6.00 hrs Mass curve time step = 10.00 min			
TIME RAIN	TIME RAIN	TIME RAIN	TIME RAIN
hrs mm/hr	hrs mm/hr	hrs mm/hr	hrs mm/hr
.17 1.61	1.67 3.92	3.17 8.52	4.67 2.30
.33 1.38	1.83 3.69	3.33 8.29	4.83 2.30
.50 1.61	2.00 3.92	3.50 8.52	5.00 2.30
.67 2.30	2.17 4.61	3.67 3.92	5.17 1.61
.83 2.30	2.33 4.61	3.83 3.69	5.33 1.38
1.00 2.30	2.50 4.61	4.00 3.92	5.50 1.61
1.17 2.30	2.67 23.04	4.17 3.00	5.67 1.61
1.33 2.30	2.83 41.47	4.33 3.23	5.83 1.38
1.50 2.30	3.00 59.90	4.50 3.00	6.00 1.61

Page 1

## Post-Dev-Con-SCS

CALIB STANDHYD (0115)	Area (ha)= .83
ID= 1 DT= 5.0 min	Total Imp(%)= 33.00
Dir. Conn.(%)= 19.00	
IMPERVIOUS PERVIOUS (i)	
Surface Area (ha)=	.27 .55
Dep. Storage (mm)=	1.00 2.00
Average Slope (%)=	2.00 3.00
Length (m)=	74.30 275.00
Mannings n =	.013 .250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	1.61	1.583	3.92	3.083	8.53	4.58	2.30
.167	1.61	1.667	3.92	3.167	8.52	4.67	2.30
.250	1.38	1.750	3.69	3.250	8.29	4.75	2.30
.333	1.38	1.833	3.69	3.333	8.29	4.83	2.30
.417	1.61	1.917	3.92	3.417	8.52	4.92	2.30
.500	1.61	2.000	3.50	3.500	8.52	5.00	2.30
.583	2.30	2.083	4.61	3.583	3.92	5.08	1.61
.667	2.30	2.167	4.61	3.667	3.92	5.17	1.61
.750	2.30	2.250	4.61	3.750	3.69	5.25	1.38
.833	2.30	2.333	4.61	3.833	3.69	5.33	1.38
.917	2.30	2.417	4.61	3.917	3.92	5.42	1.61
1.000	2.30	2.500	4.61	4.000	3.92	5.50	1.61
1.083	2.30	2.583	23.04	4.083	3.00	5.58	1.61
1.167	2.30	2.667	23.04	4.167	3.00	5.67	1.61
1.250	2.30	2.750	41.47	4.250	3.23	5.75	1.38
1.333	2.30	2.833	41.47	4.333	3.23	5.83	1.38
1.417	2.30	2.917	59.90	4.417	3.00	5.92	1.61
1.500	2.30	3.000	59.90	4.500	3.00	6.00	1.61

Max.Eff.Inten.(mm/hr)= 59.90 25.36  
over (min)= 5.00 40.00  
Storage Coeff. (min)= 2.13 (ii) 36.53 (ii)  
Unit Hyd. Tpeak (min)= 5.00 40.00  
Unit Hyd. peak (cms)= .31 .03

\*TOTALS\*  
PEAK FLOW (cms)= .03 .02 .035 (iii)  
TIME TO PEAK (hrs)= 3.00 3.50 3.00  
RUNOFF VOLUME (mm)= 37.40 20.65 23.80  
TOTAL RAINFALL (mm)= 38.40 38.40 38.40  
RUNOFF COEFFICIENT = .97 .54 .62

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 88.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 2

Post-Dev-Con-SCS  
ROUTE CHN (0116) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.676E+01	.0	.13	33.24
.06	215.06	.150E+02	.0	.21	19.61
.09	215.09	.248E+02	.0	.29	14.23
.13	215.13	.360E+02	.1	.37	11.28
.16	215.16	.488E+02	.1	.44	9.41
.19	215.19	.630E+02	.1	.51	8.11
.22	215.22	.780E+02	.2	.58	7.15
.25	215.25	.980E+02	.2	.65	6.41
.28	215.28	.115E+03	.3	.72	5.83
.32	215.32	.135E+03	.4	.78	5.35
.35	215.35	.157E+03	.5	.84	4.95
.38	215.38	.180E+03	.6	.90	4.62
.41	215.41	.205E+03	.8	.96	4.33
.44	215.44	.231E+03	.9	1.02	4.09
.47	215.47	.258E+03	1.1	1.08	3.87
.51	215.51	.288E+03	1.3	1.13	3.68
.54	215.54	.328E+03	1.5	1.19	3.51
.57	215.57	.350E+03	1.7	1.24	3.35
.60	215.60	.384E+03	2.0	1.30	3.22

<---- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
.83	.03	3.00	23.80	.10	.31
INFLOW: ID= 2 (0115)					
OUTFLOW: ID= 1 (0116)	.83	.03	3.58	23.70	.09 .27

Post-Dev-Con-SCS  
RUNOFF COEFFICIENT = .97 .46 .56

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 86.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0110) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance	Elevation	Manning
.00	215.00	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.947E+01	.0	.15	38.53
.06	215.06	.210E+02	.0	.25	23.36
.09	215.09	.347E+02	.0	.34	17.30
.13	215.13	.504E+02	.1	.42	13.94
.16	215.16	.660E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23
.28	215.28	.161E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.252E+03	.7	.96	6.05
.41	215.41	.286E+03	.8	1.02	5.70
.44	215.44	.323E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.404E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL

INFLOW: ID= 2 (0107)	3.63	.13	3.00	21.54	.18 .54
OUTFLOW: ID= 1 (0110)	3.63	.10	3.00	21.52	.16 .50

==== ADD HYD (0114) | AREA QPEAK TPEAK R.V.

| ID1= 1 (0116): .83 .025 3.58 23.70

+ ID2= 2 (0110): 3.63 .097 3.00 21.52

====

Page 3

Page 4

ID = 3 (0114): 4.45 .120 3.00 21.93

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB  
NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
ID= 1 DT=10.0 min Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr
.167	1.61	1.667	3.92	3.167	8.52	4.07	2.30
.333	1.38	1.833	3.69	3.333	8.29	4.83	2.30
.500	1.61	2.000	3.92	3.500	8.52	5.00	2.30
.667	2.30	2.167	4.61	3.667	3.92	5.17	1.61
.833	2.30	2.333	4.61	3.833	3.69	5.33	1.38
1.000	2.30	2.500	4.61	4.000	3.92	5.50	1.61
1.167	2.30	2.667	23.04	4.167	3.00	5.67	1.61
1.333	2.30	2.833	41.47	4.333	3.23	5.83	1.38
1.500	2.30	3.000	59.90	4.500	3.00	6.00	1.61

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .058 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 14.101  
TOTAL RAINFALL (mm)= 38.400  
RUNOFF COEFFICIENT = .367

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0111) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
3.00 215.00 .0500 Main Channel  
3.76 215.00 .0500  
5.56 215.60 .0000

TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.701E+01	.0	.18	22.93
.06	215.06	.160E+02	.0	.29	14.14
.09	215.09	.270E+02	.0	.39	10.61
.13	215.13	.400E+02	.1	.48	8.65
.16	215.16	.550E+02	.1	.56	7.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21

Page 5

Post-Dev-Con-SCS  
.38 215.38 .216E+03 .9 1.05 3.95  
.41 215.41 .247E+03 1.1 1.12 3.74  
.44 215.44 .280E+03 1.3 1.17 3.55  
.47 215.47 .314E+03 1.6 1.23 3.38  
.51 215.51 .351E+03 1.8 1.29 3.23  
.54 215.54 .380E+03 2.1 1.35 3.09  
.57 215.57 .431E+03 2.4 1.40 2.97  
.60 215.60 .474E+03 2.8 1.46 2.86

<---- hydrograph ----> <-pipe / channel->  
INFLOW : ID= 2 (0102) AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm) MAX DEPTH (m) MAX VEL (m/s)  
OUTFLOW: ID= 1 (0111) 1.39 .06 3.00 14.10 .11 .43

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB  
NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hr)= .35

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .071 (i)  
TIME TO PEAK (hrs)= 3.167  
RUNOFF VOLUME (mm)= 6.771  
TOTAL RAINFALL (mm)= 38.400  
RUNOFF COEFFICIENT = .176

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0113) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
2.56 215.00 .0500 / .0500 Main Channel  
4.36 215.60 .0500

TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.541E+01	.0	.15	22.38
.06	215.06	.120E+02	.0	.25	13.54

Page 6

Post-Dev-Con-SCS  
.09 215.09 .198E+02 .0 .33 10.01  
.13 215.13 .288E+02 .1 .41 8.05  
.16 215.16 .390E+02 .1 .49 6.79  
.19 215.19 .504E+02 .1 .56 5.91  
.22 215.22 .630E+02 .2 .63 5.25  
.25 215.25 .768E+02 .3 .70 4.74  
.28 215.28 .917E+02 .4 .77 4.33  
.32 215.32 .115E+03 .4 .83 4.00  
.35 215.35 .128E+03 .6 .90 3.72  
.38 215.38 .144E+03 .7 .96 3.48  
.41 215.41 .155E+03 .8 1.02 3.28  
.44 215.44 .185E+03 1.0 1.08 3.10  
.47 215.47 .207E+03 1.2 1.13 2.94  
.51 215.51 .230E+03 1.4 1.19 2.80  
.54 215.54 .255E+03 1.6 1.24 2.68  
.57 215.57 .280E+03 1.8 1.30 2.57  
.60 215.60 .307E+03 2.1 1.35 2.47

<---- hydrograph ----> <-pipe / channel->  
AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm) MAX DEPTH (m) MAX VEL (m/s)  
INFLOW : ID= 2 (0105) 4.82 .07 3.17 6.77 .14 .44  
OUTFLOW: ID= 1 (0113) 4.82 .07 3.33 6.75 .13 .43

Post-Dev-Con-SCS  
.22 215.22 .724E+02 .3 .56 3.64  
.25 215.25 .857E+02 .4 .62 3.30  
.28 215.28 .997E+02 .5 .68 3.03  
.32 215.32 .114E+03 .7 .73 2.80  
.35 215.35 .130E+03 .8 .78 2.61  
.38 215.38 .146E+03 1.0 .84 2.45  
.41 215.41 .163E+03 1.2 .89 2.31  
.44 215.44 .181E+03 1.4 .94 2.18  
.47 215.47 .198E+03 1.6 .99 2.08  
.51 215.51 .218E+03 1.8 1.04 1.98  
.54 215.54 .238E+03 2.1 1.08 1.89  
.57 215.57 .259E+03 2.4 1.13 1.81  
.60 215.60 .280E+03 2.7 1.18 1.74

<---- hydrograph ----> <-pipe / channel->  
AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm) MAX DEPTH (m) MAX VEL (m/s)  
INFLOW : ID= 2 (0112) 1.40 .04 3.00 9.32 .07 .24  
OUTFLOW: ID= 1 (0109) 1.40 .03 3.17 9.28 .06 .23

ADD HYD (0103) | AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
1 + 2 = 3 | ID1= 1 (0113): 4.82 .068 3.33 6.75  
+ ID2= 2 (0109): 1.40 .033 3.17 9.28  
ID = 3 (0103): 6.22 .100 3.25 7.31

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106) | AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
1 + 2 = 3 | ID1= 1 (0117): 5.85 .159 3.08 20.04  
+ ID2= 2 (0103): 6.22 .100 3.25 7.31  
ID = 3 (0106): 12.07 .232 3.08 13.48

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 2 \*\*  
\*\*\*\*\*

MASS STORM Ptotal= 50.50 mm | Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst  
Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION  
Duration of storm = 6.00 hrs  
Mass curve time step = 10.00 min

TIME RAIN TIME RAIN TIME RAIN  
hrs mm/hr hrs mm/hr hrs mm/hr  
.17 2.12 1.67 5.15 3.17 11.21 4.67 3.03  
.33 1.82 1.83 4.85 3.33 10.91 4.83 3.03

Page 8

ROUTE CHN (0109) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->  
Distance Elevation Manning  
.00 215.60 .0500  
1.80 215.00 .0500 / .0500 Main Channel  
3.80 215.00 .0500 Main Channel  
5.60 215.60 .0500

TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.170E+02	.0	.23	8.87
.09	215.09	.266E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07

Page 7

Post-Dev-Con-SCS						
.50	2.12	2.00	5.15	3.50	11.21	5.00
.67	3.03	2.17	6.06	3.67	5.15	5.17
.83	3.03	2.33	6.06	3.83	4.85	5.33
1.00	3.03	2.50	6.06	4.00	5.15	5.50
1.17	3.03	2.67	30.30	4.17	3.94	5.67
1.33	3.03	2.83	54.54	4.33	4.24	5.83
1.50	3.03	3.00	78.78	4.50	3.94	6.00

Post-Dev-Con-SCS  
 CN\* = 88.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		ROUTE CHN (0115)		
STANDHYD (0115)		Area (ha)= .83		
ID= 1	DT= 5.0 min	Total Imp(%)= 33.00	Dir. Conn.(%)= 19.00	
Surface Area (ha)= .83		IMPERVIOUS (i)		
Dep. Storage (mm)= 1.00		PERVIOUS (i)		
Average Slope (%)= 3.00				
Length (m)= 74.30				
Mannings n = .013				

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TRANSFORMED HYETOGRAPH						
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs
.083	1.1	1.383	5.15	3.083	11.21	4.58
.167	2.12	1.697	5.15	3.167	11.21	4.75
.250	1.82	1.750	4.85	3.250	10.91	4.75
.333	1.82	1.833	4.85	3.333	10.91	4.83
.417	2.12	1.917	5.15	3.417	11.21	4.92
.500	2.12	2.000	5.15	3.500	11.21	5.00
.583	3.03	2.083	6.06	3.583	5.15	5.08
.667	3.03	2.167	6.06	3.667	5.15	5.17
.750	3.03	2.250	6.06	3.750	4.85	5.25
.833	3.03	2.333	6.06	3.833	4.85	5.33
.917	3.03	2.417	6.06	3.917	5.15	5.42
1.000	3.03	2.500	6.06	4.000	5.15	5.50
1.083	3.03	2.583	30.30	4.183	3.94	5.58
1.167	3.03	667	30.30	4.167	3.94	5.67
1.250	3.03	750	54.54	4.250	4.24	5.75
1.333	3.03	833	54.54	4.333	4.24	5.83
1.417	3.03	917	78.78	4.417	3.94	5.92
1.500	3.03	3.000	78.78	4.500	3.94	6.00

Max.Eff.Inten.(mm/hr)= 78.78  
 over (min) 5.00 30.00  
 Storage Coeff. (min)= 1.91 (ii) 29.82 (ii)  
 Unit Hyd. Tpeak (min)= 5.00 30.00  
 Unit Hyd. peak (cms)= .32 .04

\*TOTALS\*

PEAK FLOW (cms)= .03 .04 .055 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.33 3.00  
 RUNOFF VOLUME (mm)= 49.50 30.79 34.32  
 TOTAL RAINFALL (mm)= 50.50 50.50 50.50  
 RUNOFF COEFFICIENT = .98 .61 .68

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 Page 9

ROUTE CHN (0116)		Routing time step (min)'= 5.00	
<---- DATA FOR SECTION ( 1.1 ) ----->			
Distance	Elevation	Manning	
.00	215.60	.0500	Main Channel
1.80	215.00	.0500 / .0500	Main Channel
2.56	215.00	.0500 / .0500	Main Channel
4.36	215.60	.0500	

<---- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.676E+01	.0	.13	33.24
.06	215.06	.150E+02	.0	.21	19.61
.09	215.09	.248E+02	.0	.29	14.23
.13	215.13	.360E+02	.1	.37	11.28
.16	215.16	.488E+02	.1	.44	9.41
.19	215.19	.630E+02	.1	.51	8.11
.22	215.22	.787E+02	.2	.58	7.15
.25	215.25	.960E+02	.2	.65	6.41
.28	215.28	1.138E+03	.3	.72	5.83
.32	215.32	1.353E+03	.4	.78	5.35
.35	215.35	1.575E+03	.5	.84	4.95
.38	215.38	1.800E+03	.6	.90	4.62
.41	215.41	2.025E+03	.8	.96	4.33
.44	215.44	2.313E+03	.9	1.02	4.09
.47	215.47	2.586E+03	1.1	1.08	3.87
.51	215.51	2.886E+03	1.3	1.13	3.68
.54	215.54	3.186E+03	1.5	1.19	3.51
.57	215.57	3.500E+03	1.7	1.24	3.35
.60	215.60	3.84E+03	2.0	1.30	3.22

<---- hydrograph -----> <-pipe / channel->  
 AREA (ha) OPEAK (cms) TPEAK (hrs) R.V. (mm) MAX DEPTH (m) MAX VEL (m/s)  
 INFLOW : ID= 2 (0115) .83 .06 3.00 34.32 .13 .37  
 OUTFLOW: ID= 1 (0116) .83 .04 3.42 34.18 .11 .33

CALIB		ROUTE CHN (0107)		
ID= 1	DT= 5.0 min	Area (ha)= 3.63	Total Imp(%)= 29.40	Dir. Conn.(%)= 19.00
Surface Area (ha)= 1.07		IMPERVIOUS (i)		
Dep. Storage (mm)= 1.00		PERVIOUS (i)		
Average Slope (%)= 2.00				
Length (m)= 155.50				
Mannings n = .013				

Max.Eff.Inten.(mm/hr)= 78.78  
 over (min) 5.00 50.00  
 Storage Coeff. (min)= 2.98 (ii) 47.47 (ii)  
 Page 10

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0114)		Post-Dev-Con-SCS			
1 + 2 = 3		AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1	(0116):	.83	.043	3.42	34.18
+ ID2= 2	(0110):	3.63	.143	3.00	31.50

ID = 3 (0114): 4.45 .183 3.00 32.00

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

Post-Dev-Con-SCS						
<---- DATA FOR SECTION ( 1.1 ) ----->						
Distance	Elevation	Manning				
.00	215.60	.0500	Main Channel			
1.80	215.00	.0500 / .0500	Main Channel			
2.56	215.00	.0500 / .0500	Main Channel			
4.36	215.60	.0500				

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .095 (i)

TIME TO PEAK (hrs)= 3.000

RUNOFF VOLUME (mm)= 22.480

TOTAL RAINFALL (mm)= 50.500

RUNOFF COEFFICIENT = .445

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0111)		Post-Dev-Con-SCS			
<---- DATA FOR SECTION ( 1.1 ) ----->					
Distance	Elevation	Manning			
.00	215.60	.0500	Main Channel		
3.00	215.00	.0500	Main Channel		
3.76	215.00	.0500	Main Channel		
5.56	215.60	.0500			

<---- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
.03	215.03	.701E+01	.0	.18	22.93
.06	215.06	.160E+02	.0	.29	14.14
.09	215.09	.270E+02	.0	.39	10.61
.13	215.13	.400E+02	.1	.48	8.65

Page 12

Post-Dev-Con-SCS

.16	215.16	.550E+02	.1	.56	7.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.130E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.216E+03	.9	1.05	3.95
.41	215.41	.247E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.314E+03	1.6	1.23	3.38
.51	215.51	.351E+03	1.8	1.29	3.23
.54	215.54	.390E+03	2.1	1.35	3.09
.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0102) 1.39 .09 3.00 22.48 .14 .51  
OUTFLOW: ID= 1 (0111) 1.39 .09 3.17 22.40 .13 .49

Post-Dev-Con-SCS

4.36	215.60	.0500			
TRAVEL TIME TABLE					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	5.10E+01	.001	.15	22.38
.06	215.06	1.20E+02	.00	.25	13.34
.09	215.09	1.98E+02	.00	.33	10.01
.13	215.13	2.88E+02	.1	.41	8.05
.16	215.16	3.90E+02	.1	.49	6.79
.19	215.19	5.04E+02	.1	.56	5.91
.22	215.22	.630E+02	.2	.63	5.25
.25	215.25	.768E+02	.3	.70	4.74
.28	215.28	.917E+02	.4	.77	4.33
.32	215.32	.108E+03	.4	.83	4.00
.35	215.35	.125E+03	.6	.90	3.72
.39	215.39	.142E+03	.7	.96	3.48
.43	215.41	.164E+03	.8	1.02	3.28
.44	215.44	.185E+03	1.0	1.08	3.10
.47	215.47	.207E+03	1.2	1.13	2.94
.51	215.51	.230E+03	1.4	1.19	2.80
.54	215.54	.255E+03	1.6	1.24	2.68
.57	215.57	.280E+03	1.8	1.30	2.57
.60	215.60	.307E+03	2.1	1.35	2.47

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0105) 4.82 .13 3.17 11.70 .18 .54  
OUTFLOW: ID= 1 (0113) 4.82 .12 3.25 11.68 .17 .53

ADD HYD (0117)  
| 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0114): 4.45 .183 3.00 32.00  
+ ID2= 2 (0111): 1.39 .086 3.17 22.40  
ID = 3 (0117): 5.85 .256 3.08 29.71

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0105) Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .126 (i)

TIME TO PEAK (hrs)= 3.167

RUNOFF VOLUME (mm)= 11.703

TOTAL RAINFALL (mm)= 50.500

RUNOFF COEFFICIENT = .232

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0113) IN= 2 --> OUT= 1 Routing time step (min)'= 5.00

<-- DATA FOR SECTION ( 1.1) ----->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel

Page 13

Post-Dev-Con-SCS

(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.170E+02	.0	.23	8.87
.09	215.09	.266E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.852E+02	.4	.62	3.10
.28	215.28	.997E+02	.5	.68	2.03
.32	215.32	.114E+03	.7	.73	2.80
.35	215.35	.130E+03	.8	.78	2.61
.38	215.38	.146E+03	1.0	.84	2.45
.41	215.41	.163E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18
.47	215.47	.199E+03	1.6	.99	2.08
.51	215.51	.218E+03	1.8	1.04	1.98
.54	215.54	.238E+03	2.1	1.08	1.89
.57	215.57	.259E+03	2.4	1.13	1.81
.60	215.60	.280E+03	2.7	1.18	1.74

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
(ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0112) 1.40 .06 3.00 15.69 .09 .30  
OUTFLOW: ID= 1 (0109) 1.40 .06 3.17 15.64 .09 .29

ADD HYD (0103)  
| 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0113): 4.82 .121 3.25 11.68  
+ ID2= 2 (0109): 1.40 .060 3.17 15.64  
ID = 3 (0103): 6.22 .177 3.25 12.57

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)  
| 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
(ha) (cms) (hrs) (mm)  
ID1= 1 (0117): 5.85 .256 3.08 29.71  
+ ID2= 2 (0103): 6.22 .177 3.25 12.57  
ID = 3 (0106): 12.07 .404 3.08 20.88

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\*  
\*\* SIMULATION NUMBER: 3 \*\*  
\*\*\*\*\*

MASS STORM Pttotal= 58.60 mm      Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst  
Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Post-Dev-Con-SCS  
Duration of storm = 6.00 hrs  
Mass curve time step = 10.00 min

TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	2.46	1.67	5.98	3.17	13.01
.33	2.11	1.83	5.63	3.33	12.66
.50	2.46	2.00	5.98	3.50	13.00
.67	2.72	2.27	5.98	3.67	5.00
.83	3.22	2.33	7.03	3.83	5.98
1.00	3.52	2.50	7.03	4.00	5.98
1.17	3.52	2.67	35.16	4.17	4.57
1.33	3.52	2.83	63.29	4.33	4.92
1.50	3.52	3.00	91.42	4.50	4.57

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TRANSFORMED HYETOGRAPH

TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	2.46	1.583	5.98	3.083	13.01
.167	2.46	1.667	5.98	3.167	13.01
.250	2.11	1.750	5.63	3.250	12.66
.333	2.11	1.833	5.63	3.333	12.66
.417	2.46	1.917	5.98	3.417	13.01
.500	2.46	2.000	5.98	3.500	13.01
.583	3.52	2.083	7.03	3.583	5.98
.667	3.52	2.167	7.03	3.667	5.98
.750	3.25	2.250	7.03	3.750	5.98
.833	3.25	2.333	7.03	3.833	5.98
.917	3.52	2.417	7.03	3.917	5.98
1.000	3.52	2.500	7.03	4.000	5.98
1.083	3.52	2.583	35.16	4.083	4.57
1.167	3.52	2.667	35.16	4.167	4.57
1.250	3.52	2.750	63.29	4.250	4.92
1.333	3.52	2.833	63.29	4.333	4.92
1.417	3.52	2.917	91.42	4.417	4.57
1.500	3.52	3.000	91.42	4.500	4.57

Max.Eff.Inten.(mm/hr)= 91.42 59.44  
over (min)= 5.00 30.00  
Storage Coeff. (min)= 1.80 (ii) 26.27 (ii)  
Unit Hyd. Tpeak (min)= 5.00 30.00  
Unit Hyd. peak (cms)= .32 .04  
\*TOTALS\*  
PEAK FLOW (cms)= .04 .05 .068 (iii)  
TIME TO PEAK (hrs)= 3.00 3.33 3.00  
RUNOFF VOLUME (mm)= 57.60 37.89 41.61  
TOTAL RAINFALL (mm)= 58.60 58.60 58.60

Page 15

Page 16

Post-Dev-Con-SCS  
 RUNOFF COEFFICIENT = .98 .65 .71

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 $CN^* = 88.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0116) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY (m/s) TRAV. TIME (min)  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .675E+01 .0 .13 33.24  
 .06 215.06 .150E+02 .0 .21 16.51  
 .09 215.09 .248E+02 .0 .29 14.23  
 .13 215.13 .360E+02 .1 .37 11.28  
 .16 215.16 .488E+02 .1 .44 9.41  
 .19 215.19 .630E+02 .1 .51 8.11  
 .22 215.22 .787E+02 .2 .58 7.15  
 .25 215.25 .960E+02 .2 .65 6.41  
 .28 215.28 .115E+03 .3 .72 5.83  
 .32 215.32 .135E+03 .4 .78 5.35  
 .35 215.35 .157E+03 .5 .84 4.95  
 .38 215.38 .180E+03 .6 .90 4.62  
 .41 215.41 .205E+03 .8 .96 4.33  
 .44 215.44 .231E+03 .9 .99 4.09  
 .47 215.47 .258E+03 1.1 1.08 3.87  
 .51 215.51 .288E+03 1.3 1.13 3.68  
 .54 215.54 .318E+03 1.5 1.19 3.51  
 .57 215.57 .350E+03 1.7 1.24 3.35  
 .60 215.60 .384E+03 2.0 1.30 3.22

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0115) .83 .07 3.00 41.61 .14 .40  
 OUTFLOW: ID= 1 (0116) .83 .06 3.42 41.44 .13 .38

CALIB STANDHYD (0107) | Area (ha)= 3.63  
 ID= 1 DT= 5.0 min | Total Imp% = 29.40 Dir. Conn.(%)= 19.00

IMPERVIOUS PERVERIOUS (i)  
 Surface Area (ha)= 1.07 2.56  
 Dep. Storage (mm)= 1.00 3.00

Page 17

Post-Dev-Con-SCS  
 Average Slope (%)= 2.00 3.00  
 Length (m)= 155.50 440.00  
 Manning's n = .013 .250

Max.Eff.Inten.(mm/hr)=	91.42	36.55
over (min)=	5.00	45.00
Storage Coeff. (min)=	2.80 (ii)	42.21 (ii)
Unit Hyd. Tpeak (min)=	5.00	45.00
Unit Hyd. peak (cms)=	.28	.03
PEAK FLOW (cms)=	.17	.15
TIME TO PEAK (hrs)=	3.00	3.58
RUNOFF VOLUME (mm)=	57.60	34.06
TOTAL RAINFALL (mm)=	58.60	58.60
RUNOFF COEFFICIENT =	.98	.58

\*TOTALS\* .225 (iii)

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 $CN^* = 86.0$  Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0110) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

<---- TRAVEL TIME TABLE ---->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY (m/s) TRAV. TIME (min)  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .947E+01 .0 .15 38.53  
 .06 215.06 .210E+02 .0 .25 23.36  
 .09 215.09 .347E+02 .0 .34 17.30  
 .13 215.13 .504E+02 .1 .42 13.94  
 .16 215.16 .683E+02 .1 .50 11.77  
 .19 215.19 .882E+02 .1 .57 10.25  
 .22 215.22 .110E+03 .2 .64 9.11  
 .25 215.25 .134E+03 .3 .71 8.23  
 .28 215.28 .161E+03 .4 .78 7.53  
 .32 215.32 .189E+03 .5 .84 6.95  
 .35 215.35 .219E+03 .6 .90 6.47  
 .38 215.38 .252E+03 .7 .96 6.05  
 .41 215.41 .286E+03 .8 1.02 5.70  
 .44 215.44 .323E+03 1.0 1.08 5.39  
 .47 215.47 .362E+03 1.2 1.14 5.12  
 .51 215.51 .403E+03 1.4 1.20 4.88  
 .54 215.54 .446E+03 1.6 1.25 4.66  
 .57 215.57 .491E+03 1.8 1.30 4.47  
 .60 215.60 .538E+03 2.1 1.36 4.30

<---- hydrograph ----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 Page 18

INFLOW : ID= 2 (0115) .83 .07 3.00 41.61 .14 .40  
 OUTFLOW: ID= 1 (0116) .83 .06 3.42 41.44 .13 .38

CALIB STANDHYD (0107) | Area (ha)= 3.63  
 ID= 1 DT= 5.0 min | Total Imp% = 29.40 Dir. Conn.(%)= 19.00

IMPERVIOUS PERVERIOUS (i)  
 Surface Area (ha)= 1.07 2.56  
 Dep. Storage (mm)= 1.00 3.00

Page 17

Post-Dev-Con-SCS  
 INFLOW : ID= 2 (0107) 3.63 .22 3.00 38.53 .23 .66  
 OUTFLOW: ID= 1 (0110) 3.63 .18 3.00 38.50 .21 .61

ADD HYD (0114) |  
 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0116): .83 .057 3.42 41.44  
 + ID2= 2 (0110): 3.63 .179 3.00 38.50  
 ======  
 ID = 3 (0114): 4.45 .229 3.00 39.04

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
 ID= 1 DT=10.0 min | Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TIME RAIN TRANSFORMED HYETOGRAPH  
 hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr  
 .367 2.46 1.295 5.98 3.137 13.91 12.66 4.83 3.52  
 .333 2.11 1.833 5.63 3.333 12.66 4.83 3.52  
 .500 2.46 2.000 5.98 3.500 13.01 5.00 3.52  
 .667 3.52 2.167 7.03 3.667 5.98 5.17 2.46  
 .833 3.52 2.333 7.03 3.833 5.63 5.33 2.11  
 1.000 3.52 2.500 7.03 4.000 5.98 5.50 2.46  
 1.167 3.52 2.667 35.16 4.167 4.57 5.67 2.46  
 1.333 3.52 2.833 63.29 4.333 4.92 5.83 2.11  
 1.500 3.52 3.000 91.42 4.500 4.57 6.00 2.46

Unit Hyd Ppeak (cms)= .223

PEAK FLOW (cms)= .122 (i)

TIME TO PEAK (hrs)= 3.0000

RUNOFF VOLUME (mm)= 28.556

TOTAL RAINFALL (mm)= 58.600

RUNOFF COEFFICIENT = .487

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0111) | Routing time step (min)'= 5.00  
 IN= 2--> OUT= 1 |  
 <---- DATA FOR SECTION ( 1.1 ) ---->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 3.00 215.00 .0500 Main Channel  
 3.76 215.00 .0500  
 5.56 215.60 .0000

Page 19

Post-Dev-Con-SCS  
 INFLOW : ID= 2 (0102) 1.39 .12 3.00 28.56 .16 .56  
 OUTFLOW: ID= 1 (0111) 1.39 .11 3.17 28.48 .15 .54

<---- hydrograph ----> <-pipe / channel->

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL

INFLOW : ID= 2 (0102) 1.39 .12 3.00 28.56 .16 .56

OUTFLOW: ID= 1 (0111) 1.39 .11 3.17 28.48 .15 .54

ADD HYD (0117) |  
 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0114): 4.45 .229 3.00 39.04  
 + ID2= 2 (0111): 1.39 .111 3.17 28.48  
 ======  
 ID = 3 (0117): 5.85 .329 3.08 36.53

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
 ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .35

Unit Hyd Ppeak (cms)= .522

PEAK FLOW (cms)= .169 (i)

TIME TO PEAK (hrs)= 3.167

RUNOFF VOLUME (mm)= 15.528

TOTAL RAINFALL (mm)= 58.600

RUNOFF COEFFICIENT = .265

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0113) |

Page 20

| IN= 2--> OUT= 1 | Routing time step (min)'= 5.00  
 -----  
 <---- DATA FOR SECTION ( 1.1 ) ----->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.60 .0500 / .0500 Main Channel  
 2.56 215.60 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

<---- TRAVEL TIME TABLE ----->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)  
 .03 215.03 .541E+01 .0 .15 22.38  
 .06 215.06 .120E+02 .0 .25 13.54  
 .09 215.09 .198E+02 .0 .33 10.01  
 .13 215.13 .288E+02 .1 .41 8.05  
 .17 215.16 .386E+02 .1 .49 6.79  
 .19 215.19 .504E+02 .1 .56 5.91  
 .22 215.22 .630E+02 .2 .63 5.25  
 .25 215.25 .768E+02 .3 .70 4.74  
 .28 215.28 .917E+02 .4 .77 4.33  
 .32 215.32 .108E+03 .4 .83 4.00  
 .35 215.35 .125E+03 .6 .90 3.72  
 .38 215.38 .144E+03 .7 .96 3.48  
 .41 215.41 .164E+03 .8 1.02 3.28  
 .44 215.44 .185E+03 1.0 1.08 3.10  
 .47 215.47 .207E+03 1.2 1.13 2.94  
 .51 215.51 .230E+03 1.4 1.19 2.80  
 .54 215.54 .255E+03 1.6 1.24 2.68  
 .57 215.57 .280E+03 1.8 1.30 2.57  
 .60 215.60 .307E+03 2.1 1.35 2.47

<---- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0105) 4.82 .17 3.17 15.53 .20 .59  
 OUTFLOW: ID= 1 (0113) 4.82 .16 3.25 15.50 .20 .59

CALIB NASHYD (0112) Area (ha)= 1.40 Curve Number (CN)= 75.0  
 ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .084 (i)  
 TIME TO PEAK (hrs)= 3.0000  
 RUNOFF VOLUME (mm)= 20.501  
 TOTAL RAINFALL (mm)= 58.600  
 RUNOFF COEFFICIENT = .350

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0109) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00  
 -----  
 <---- DATA FOR SECTION ( 1.1 ) ----->  
 Distance Elevation Manning  
 Page 21

Post-Dev-Con-SCS  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 3.80 215.00 .0500 Main Channel  
 5.60 215.60 .0500

<---- TRAVEL TIME TABLE ----->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.170E+02	.0	.23	8.87
.09	215.09	.266E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.857E+02	.4	.62	3.30
.28	215.28	.990E+02	.5	.68	3.03
.32	215.32	.114E+03	.7	.73	2.80
.35	215.35	.130E+03	.8	.78	2.61
.38	215.38	.146E+03	1.0	.84	2.45
.41	215.41	.163E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18
.47	215.47	.199E+03	1.6	.99	2.08
.51	215.51	.218E+03	1.8	1.04	1.98
.54	215.54	.238E+03	2.1	1.08	1.89
.57	215.57	.259E+03	2.4	1.13	1.81
.60	215.60	.280E+03	2.7	1.18	1.74

<---- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0112) 1.40 .08 3.00 20.50 .11 .33  
 OUTFLOW: ID= 1 (0109) 1.40 .08 3.17 20.45 .10 .32

ADD HYD (0103)		
1 + 2	3	4
AREA	QPEAK	TPEAK
(ha)	(cms)	(hrs)
+ ID1= 1 (0113):	4.82	.163
+ ID2= 2 (0109):	1.40	.080
ID = 3 (0103):	6.22	.238
	3.25	16.62

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106)		
1 + 2	3	4
AREA	QPEAK	TPEAK
(ha)	(cms)	(hrs)
+ ID1= 1 (0117):	5.85	.329
+ ID2= 2 (0103):	6.22	.238
ID = 3 (0106):	12.07	.534
	3.08	26.27

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

Post-Dev-Con-SCS  
 Unit Hyd. Tpeak (min)= 5.00 25.00  
 Unit Hyd. peak (cms)= .32 .05  
 \*TOTALS\*  
 PEAK FLOW (cms)= .05 .07 .092 (iii)  
 TIME TO PEAK (hrs)= 3.00 3.25 3.00  
 RUNOFF VOLUME (mm)= 67.70 46.97 50.90  
 TOTAL RAINFALL (mm)= 68.70 68.70 68.70  
 RUNOFF COEFFICIENT = .99 .68 .74

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%

YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0116) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->  
 Distance Elevation Manning  
 .00 215.60 .0500  
 1.80 215.00 .0500 / .0500 Main Channel  
 2.56 215.00 .0500 / .0500 Main Channel  
 4.36 215.60 .0500

<---- TRAVEL TIME TABLE ----->  
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME  
 (m) (m) (cu.m.) (cms) (m/s) (min)

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.676E+01	.0	.13	33.24
.06	215.06	.150E+02	.0	.21	19.61
.09	215.09	.248E+02	.0	.29	14.23
.13	215.13	.360E+02	.1	.37	11.28
.16	215.16	.488E+02	.1	.44	9.41
.19	215.19	.630E+02	.1	.51	8.11
.22	215.22	.787E+02	.2	.58	7.15
.25	215.25	.960E+02	.2	.65	6.41
.28	215.28	.115E+03	.3	.72	5.83
.32	215.32	.135E+03	.4	.78	5.35
.35	215.35	.157E+03	.5	.84	4.95
.38	215.38	.180E+03	.6	.90	4.62
.41	215.41	.205E+03	.8	.96	4.33
.44	215.44	.231E+03	.9	1.02	4.09
.47	215.47	.258E+03	1.1	1.08	3.87
.51	215.51	.288E+03	1.3	1.13	3.68
.54	215.54	.318E+03	1.5	1.19	3.51
.57	215.57	.350E+03	1.7	1.24	3.35
.60	215.60	.384E+03	2.0	1.30	3.22

<---- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)

INFLOW : ID= 2 (0115) .83 .09 3.00 50.90 .16 .45  
 OUTFLOW: ID= 1 (0116) .83 .08 3.33 50.70 .15 .41

Max.Eff.Inten.(mm/hr)= 107.17 73.77  
 over (min) 5.00 25.00  
 Storage Coeff. (min)= 1.69 (ii) 24.13 (ii)

Page 23

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Page 24

Post-Dev-Con-SCS

CALIB	STANDHYD (0107)	Area (ha)= 3.63	Curve Number (CN)= 19.00
ID= 1 DT= 5.0 min	Total Imp(%)= 29.40	Dir. Conn.(%)= 19.00	

IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	1.07 2.56
Dep. Storage (mm)=	1.00 3.00
Average Slope (%)=	2.00 3.00
Length (m)=	155.50 440.00
Mannings n =	.013 .250
Max.Eff.Inten.(mm/hr)=	107.17 50.61
over (min)	5.00 40.00
Storage Coeff. (min)=	2.63 (ii) 37.22 (ii)
Unit Hyd. Peak (min)=	5.00 40.00
Unit Hyd. peak (cms)=	.29 .03
PEAK FLOW (cms)=	.20 .21 .286 (iii)
TIME TO PEAK (hrs)=	3.00 3.50 3.00
RUNOFF VOLUME (mm)=	67.70 42.76 47.50
TOTAL RAINFALL (mm)=	68.70 68.70 68.70
RUNOFF COEFFICIENT =	.99 .62 .69

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN<sup>x</sup> = 86.0 Ia = Dep. Storage (Above)  
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.  
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0110) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ---->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.947E+01	.0	.15	38.53
.06	215.06	.240E+02	.0	.25	23.36
.09	215.09	.347E+02	.0	.34	16.30
.13	215.13	.504E+02	.1	.42	12.94
.16	215.16	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23
.28	215.28	.161E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.252E+03	.7	.96	6.05
.41	215.41	.286E+03	.8	1.02	5.70
.44	215.44	.323E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12

Page 25

Post-Dev-Con-SCS

.51	215.51	.403E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
3.63	.29	3.00	47.50	.26	.72
3.63	.23	3.00	47.46	.23	.67

INFLOW : ID= 2 (0107) 3.63 .29 3.00 47.50 .26 .72  
OUTFLOW: ID= 1 (0110) 3.63 .23 3.00 47.46 .23 .67

<---- ADD HYD (0114) ---->

1 + 2 = 3	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
	83	.075	3.33	50.70		
+ ID2= 2 (0110):	3.63	.231	3.00	47.46		
ID = 3 (0114):	4.45	.299	3.00	48.06		

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
ID= 1 DT=10.0 min | Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

<---- TRANSFORMED HYETOGRAPH ---->

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm hr	TIME hrs	RAIN mm hr
.167	2.89	1.667	6.00	1.367	15.84
.333	2.47	1.333	6.00	3.333	15.84
.500	2.89	2.000	7.01	3.500	15.25
.667	4.12	2.167	8.24	3.667	7.01
.833	4.12	2.333	8.24	3.833	6.60
1.000	4.12	2.500	8.24	4.000	7.01
1.167	4.12	2.667	41.22	4.167	5.36
1.333	4.12	2.833	74.20	4.333	5.77
1.500	4.12	3.000	107.17	4.500	5.83

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .157 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 36.516  
TOTAL RAINFALL (mm)= 68.700  
RUNOFF COEFFICIENT = .532

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0111) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

Page 26

Post-Dev-Con-SCS

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
.00	215.60	.0500
3.00	215.00	.0500 Main Channel
3.76	215.00	.0500
5.56	215.60	.0000

<---- TRAVEL TIME TABLE ---->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.701E+01	.0	.18	22.93
.06	215.06	.160E+02	.0	.29	14.14
.09	215.09	.270E+02	.0	.39	10.61
.13	215.13	.400E+02	.1	.48	8.65
.16	215.16	.550E+02	.1	.56	7.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.30
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.216E+03	.9	1.05	3.95
.41	215.41	.247E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.314E+03	1.6	1.23	3.38
.51	215.51	.351E+03	1.8	1.29	3.23
.54	215.54	.390E+03	2.1	1.35	3.09
.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
1.39	.16	3.00	36.52	.17	.60
1.39	.14	3.17	36.43	.17	.59

Post-Dev-Con-SCS  
RUNOFF COEFFICIENT = .303

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0113) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ---->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.541E+01	.0	.15	22.38
.06	215.06	.120E+02	.0	.25	13.54
.09	215.09	.198E+02	.0	.33	10.01
.13	215.13	.288E+02	.1	.41	8.05
.16	215.16	.390E+02	.1	.49	6.79
.19	215.19	.504E+02	.1	.56	5.91
.22	215.22	.630E+02	.2	.63	5.25
.25	215.25	.768E+02	.3	.70	4.74
.28	215.28	.917E+02	.4	.77	4.33
.32	215.32	.108E+03	.4	.83	4.00
.35	215.35	.125E+03	.6	.90	3.72
.38	215.38	.144E+03	.7	.96	3.48
.41	215.41	.163E+03	.8	1.02	3.18
.44	215.44	.185E+03	1.0	1.08	3.10
.47	215.47	.207E+03	1.2	1.13	2.94
.51	215.51	.230E+03	1.4	1.19	2.80
.54	215.54	.255E+03	1.6	1.24	2.68
.57	215.57	.280E+03	1.8	1.30	2.57
.60	215.60	.307E+03	2.1	1.35	2.47

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
4.82	.23	3.17	20.79	.23	.66
4.82	.22	3.25	20.77	.23	.65

CALIB NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222  
PEAK FLOW (cms)= .112 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 26.984  
TOTAL RAINFALL (mm)= 68.700  
RUNOFF COEFFICIENT = .393

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Page 28

CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .35

Unit Hyd Qpeak (cms)= .522  
PEAK FLOW (cms)= .3228 (i)  
TIME TO PEAK (hrs)= 3.167  
RUNOFF VOLUME (mm)= 20.792  
TOTAL RAINFALL (mm)= 68.700

Page 27

## Post-Dev-Con-SCS

ROUTE CHN (0109) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

TRAVEL TIME TABLE					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME
(m)	(m.)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.178E+02	.0	.23	8.87
.09	215.09	.266E+02	.1	.31	5.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.857E+02	.4	.62	3.30
.28	215.28	.997E+02	.5	.68	3.03
.32	215.32	.114E+03	.7	.73	2.80
.35	215.35	.130E+03	.8	.78	2.61
.38	215.38	.146E+03	1.0	.84	2.45
.41	215.41	.163E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18
.47	215.47	.199E+03	1.6	.99	2.08
.51	215.51	.218E+03	1.8	1.04	1.98
.54	215.54	.238E+03	2.1	1.08	1.89
.57	215.57	.259E+03	2.4	1.13	1.81
.60	215.60	.280E+03	2.7	1.18	1.74

<---- hydrograph ----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)

INFLOW : ID= 2 (0112)

OUTFLOW: ID= 1 (0109)

1.40

.11

3.00

26.98

.13

.37

1.40

.11

3.17

26.94

.12

.37

ADD HYD (0103) | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0113): 4.82 .222 3.25 20.77  
 + ID2= 2 (0109): 1.40 .107 3.17 26.94  
 ID = 3 (0103): 6.22 .320 3.25 22.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0106) | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 (0117): 5.85 .436 3.08 45.29  
 + ID2= 2 (0103): 6.22 .320 3.25 22.16

Page 29

## Post-Dev-Con-SCS

ID = 3 (0106): 12.07 .723 3.08 33.37

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

=====  
 \*\* SIMULATION NUMBER: 5 \*\*  
 =====

MASS STORM | Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst  
 Ptotal= 76.30 mm | Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Duration of storm = 6.00 hrs

Mass curve time step = 10.00 min

TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	3.20	1.67	7.78	3.17	16.94
.33	2.75	1.83	7.32	3.33	16.48
.50	3.20	2.00	7.78	3.50	16.94
.67	4.58	2.17	9.16	3.67	7.78
.83	4.58	2.33	9.16	3.83	7.32
1.00	4.58	2.50	9.16	4.00	7.78
1.17	4.58	2.67	45.78	4.17	5.95
1.33	4.58	2.83	82.40	4.33	6.41
1.50	4.58	3.00	119.03	4.50	5.95

CALIB | STANDHYD (0115) | Area (ha)= .83  
 ID= 1 DT= 5.0 min | Total Imp(%)= 33.00 Dir. Conn.(%)= 19.00

Surface Area	Impervious	Pervious (i)
(ha)	.27	.55
Dep. Storage (mm)=	1.00	2.00
Average Slope (%)=	2.00	3.00
Length (m)=	74.30	275.00
Mannings n =	.013	.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.083	3.20	1.583	7.78	3.083	16.94
.167	3.20	1.667	7.78	3.167	16.48
.250	2.75	1.150	7.32	3.250	16.48
.333	2.75	1.83	7.32	3.33	16.48
.417	3.20	1.917	7.78	3.417	16.94
.500	3.20	2.000	7.78	3.500	16.94
.667	4.58	2.167	9.16	3.667	7.78
.750	4.58	2.250	9.16	3.750	7.32
.833	4.58	2.333	9.16	3.833	7.32
.917	4.58	2.417	9.16	3.917	7.78
1.000	4.58	2.500	9.16	4.000	7.78
1.083	4.58	2.583	45.78	4.083	5.95
1.167	4.58	2.667	45.78	4.167	5.95
1.250	4.58	2.750	82.40	4.250	6.41

Page 30

Post-Dev-Con-SCS | (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 2 (0115) .83 .11 3.00 57.98 .17 .47  
 OUTFLOW: ID= 1 (0116) .83 .09 3.33 57.79 .16 .45

CALIB | STANDHYD (0107) | Area (ha)= 3.63  
 ID= 1 DT= 5.0 min | Total Imp(%)= 29.40 Dir. Conn.(%)= 19.00

Surface Area	Impervious	Pervious (i)
(ha)	1.07	2.56
Dep. Storage (mm)=	1.00	3.00
Average Slope (%)=	2.00	3.00
Length (m)=	155.50	440.00
Mannings n =	.013	.250

Max.Eff.Inten.(mm/hr)=	58.72
over (min)	5.00
Storage Coeff. (min)=	2.52 (ii) 33.12 (ii)
Unit Hyd. Tpeak (min)=	5.00 40.00
Unit Hyd. peak (cms)=	.29 .03

\*TOTALS\*

PEAK FLOW (cms)=	.23
TIME TO PEAK (hrs)=	3.00
RUNOFF VOLUME (mm)=	75.30
TOTAL RAINFALL (mm)=	76.30
RUNOFF COEFFICIENT =	.99 .65

.71 .71 .45 .45

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
 \*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%  
 YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:  
 CN<sup>x</sup> = 88.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

ROUTE CHN (0116) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME
(m)	(m.)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.947E+01	.0	.15	38.53
.06	215.06	.210E+02	.0	.25	23.36
.09	215.09	.347E+02	.0	.34	17.30
.13	215.13	.504E+02	.1	.42	13.94
.16	215.16	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23

Page 32

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME
(m)	(m.)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.947E+01	.0	.15	38.53
.06	215.06	.210E+02	.0	.25	23.36
.09	215.09	.347E+02	.0	.34	17.30
.13	215.13	.504E+02	.1	.42	13.94
.16	215.16	.683E+02	.1	.50	11.77
.19	215.19	.882E+02	.1	.57	10.25
.22	215.22	.110E+03	.2	.64	9.11
.25	215.25	.134E+03	.3	.71	8.23

Area Qpeak Tpeak R.V. MAX DEPTH MAX VEL

Page 31

Post-Dev-Con-SCS

.28	215.28	.161E+03	.4	.78	7.53
.32	215.32	.189E+03	.5	.84	6.95
.35	215.35	.219E+03	.6	.90	6.47
.38	215.38	.252E+03	.7	.96	6.05
.41	215.41	.280E+03	.8	1.02	5.70
.44	215.44	.303E+03	1.0	1.08	5.39
.47	215.47	.362E+03	1.2	1.14	5.12
.51	215.51	.403E+03	1.4	1.20	4.88
.54	215.54	.446E+03	1.6	1.25	4.66
.57	215.57	.491E+03	1.8	1.30	4.47
.60	215.60	.538E+03	2.1	1.36	4.30

<---- hydrograph ----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0107)	3.63	.33	3.00	54.38	.27
OUTFLOW: ID= 1 (0110)	3.63	.27	3.58	54.34	.25
					.71

Post-Dev-Con-SCS  
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0111)| IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance	Elevation	Manning
.00	215.60	.0500
3.00	215.00	.0500
3.76	215.00	.0500
5.56	215.60	.0500

Main Channel

<---- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.701E+01	.0	.18	22.93
.06	215.06	.160E+02	.0	.29	14.14
.09	215.09	.270E+02	.0	.39	10.61
.13	215.13	.400E+02	.1	.48	8.65
.16	215.16	.550E+02	.1	.56	7.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.215E+03	.9	1.05	3.95
.41	215.41	.247E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.314E+03	1.6	1.23	3.38
.51	215.51	.351E+03	1.8	1.29	3.23
.54	215.54	.390E+03	2.1	1.35	3.09
.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

<---- hydrograph ----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0102)	1.39	.18	3.00	42.73	.19
OUTFLOW: ID= 1 (0111)	1.39	.17	3.17	42.65	.18
					.62

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0  
ID= 1 DT=10.0 min Ia (mm)= 4.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

TIME RAIN | TIME RAIN | TIME RAIN

TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.167	3.20	1.667	7.78	3.167	16.94
.333	2.75	1.833	7.32	3.333	16.48
.500	3.20	2.000	7.78	3.500	16.98
.667	4.58	2.167	9.16	3.667	7.78
.833	4.58	2.333	9.16	3.833	7.32
1.000	4.58	2.500	9.16	4.000	7.78
1.167	4.58	2.667	45.28	4.167	5.95
1.333	4.58	2.833	82.40	4.333	6.41
1.500	4.58	3.000	119.03	4.500	5.95

---- TRANSFORMED HYETOGRAPH ----

Unit Hyd Qpeak (cms)= .223

PEAK FLOW (cms)= .184 (i)  
TIME TO PEAK (hrs)= 3.167  
RUNOFF VOLUME (mm)= 42.727  
TOTAL RAINFALL (mm)= 76.300  
RUNOFF COEFFICIENT = .560

Page 33

| ADD HYD (0117) | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
-----  
+ ID1= 1 (0114): 4.45 .347 3.00 54.98  
+ ID2= 2 (0111): 1.39 .169 3.17 42.65  
-----  
ID = 3 (0117): 5.85 .511 3.08 52.04

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB NASHYD (0105) | Area (ha)= 4.82 Curve Number (CN)= 66.0  
ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .35

Page 34

#### Post-Dev-Con-SCS

Unit Hyd Qpeak (cms)= .522  
PEAK FLOW (cms)= .277 (i)  
TIME TO PEAK (hrs)= 3.167  
RUNOFF VOLUME (mm)= 25.070  
TOTAL RAINFALL (mm)= 76.300  
RUNOFF COEFFICIENT = .329

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Post-Dev-Con-SCS  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 32.159  
TOTAL RAINFALL (mm)= 76.300  
RUNOFF COEFFICIENT = .421

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0109) | IN= 2--> OUT= 1 | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ----->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
2.56	215.00	.0500 / .0500 Main Channel
4.36	215.60	.0500

<---- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.03	215.03	.541E+01	.0	.15	22.38
.06	215.06	.120E+02	.0	.25	13.54
.09	215.09	.198E+02	.0	.33	10.01
.13	215.13	.288E+02	.1	.41	8.05
.16	215.16	.380E+02	.1	.49	6.79
.19	215.19	.504E+02	.1	.56	5.91
.22	215.22	.630E+02	.2	.63	5.25
.25	215.25	.768E+02	.3	.70	4.74
.28	215.28	.917E+02	.4	.77	4.33
.32	215.32	.108E+03	.4	.83	4.00
.35	215.35	.125E+03	.6	.90	3.72
.38	215.38	.144E+03	.7	.96	3.48
.41	215.41	.164E+03	.8	1.02	3.28
.44	215.44	.185E+03	1.0	1.08	3.10
.47	215.47	.207E+03	1.2	1.13	2.94
.51	215.51	.230E+03	1.4	1.19	2.80
.54	215.54	.255E+03	1.6	1.24	2.68
.57	215.57	.280E+03	1.8	1.30	2.57
.60	215.60	.307E+03	2.1	1.35	2.47

<---- hydrograph ----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0112)	1.40	.13	3.00	32.16	.14
OUTFLOW: ID= 1 (0109)	1.40	.13	3.08	32.11	.13
					.39

| ADD HYD (0103) | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
-----  
+ ID1= 1 (0113): 4.82 .271 3.25 25.05  
+ ID2= 2 (0109): 1.40 .129 3.08 32.11  
-----  
ID = 3 (0103): 6.22 .387 3.25 26.63

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Page 36

CALIB NASHYD (0112) Area (ha)= 1.40 Curve Number (CN)= 75.0  
ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .134 (i)

Page 35

Post-Dev-Con-SCS

ADD HYD (0106)		1 + 2 = 3	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)
+ ID1= 1 (0117);		.833	.511	3.08	52.04	
+ ID2= 2 (0103);		6.22	.387	3.23	26.63	
ID = 3 (0106):		12.07	.861	3.08	38.95	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

*****	
** SIMULATION NUMBER: 6 **	
*****	

MASS STORM	Filename: C:\visual otthymo files\4456\SCS II 6-hr.mst
Ptotal= 83.80 mm	Comments: SCS 6 HOUR TYPE II STORM DISTRIBUTION

Duration of storm = 6.00 hrs

Mass curve time step = 10.00 min

TIME hrs	RAIN mm/hr						
.15	3.52	1.67	8.55	3.17	18.60	4.67	5.03
.13	3.04	1.83	8.04	3.33	18.60	4.83	5.35
.50	2.52	2.00	8.55	3.50	18.60	5.00	5.03
.67	2.03	2.17	10.06	3.67	8.55	5.17	5.52
.83	5.03	2.33	10.06	3.83	8.04	5.33	5.02
1.00	5.03	2.50	10.06	4.00	8.55	5.50	5.52
1.17	5.03	2.67	50.28	4.17	6.54	5.67	5.52
1.33	5.03	2.83	90.50	4.33	7.04	5.83	5.02
1.50	5.03	3.00	130.73	4.50	6.54	6.00	3.52

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

IMPERVIOUS		PERVIOUS (i)	
Surface Area (ha)=	.27	Impervious (%)=	.55
Dep. Storage (mm)=	1.00		2.00
Average Slope (%)=	2.00		3.00
Length (m)=	74.30		275.00
Mannings n =	.013		.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

Page 37

Post-Dev-Con-SCS						
.750	5.03	2.250	10.06	3.750	8.04	5.25
.833	5.03	2.333	10.06	3.833	8.04	5.33
.917	5.03	2.417	10.06	3.917	8.55	5.42
1.000	5.03	2.500	10.06	4.000	8.55	5.50
1.083	5.03	2.583	10.25	4.183	6.00	5.58
1.167	5.03	2.667	10.17	4.367	6.54	5.67
1.250	5.03	2.750	90.50	4.250	7.04	5.75
1.333	5.03	2.833	90.50	4.333	7.04	5.83
1.417	5.03	2.917	130.73	4.417	6.54	5.92
1.500	5.03	3.000	130.73	4.500	6.54	5.52

Max.Eff.Inten.(mm/hr)=	130.73	109.46
over (min)	5.00	25.00
Storage Coeff. (min)=	1.56	(ii) 20.72 (ii)
Unit Hyd. Tpeak (min)=	5.00	25.00
Unit Hyd. peak (cms)=	.33	.05
		*TOTALS*
PEAK FLOW (cms)=	.06	.10
TIME TO PEAK (hrs)=	3.00	3.25
RUNOFF VOLUME (mm)=	82.80	60.90
TOTAL RAINFALL (mm)=	83.80	83.80
RUNOFF COEFFICIENT =	.99	.73

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!  
\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20% YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
- CN= 88.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----| ROUTE CHN (0116) | Routing time step (min)'= 5.00

DATA FOR SECTION ( 1.1 ) ----->			
Distance .00	Elevation 215.60	Manning .0500	
1.80	215.00	.0500 / .0500 Main Channel	
2.56	215.00	.0500 / .0500 Main Channel	
4.36	215.60	.0500	

<---- TRAVEL TIME TABLE ----->						
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	
.03	215.03	.676E+01	.0	.13	33.24	
.06	215.06	.150E+02	.0	.21	19.61	
.09	215.09	.240E+02	.0	.29	14.23	
.13	215.13	.360E+02	.1	.37	11.72	
.16	215.16	.488E+02	.1	.44	9.41	
.19	215.19	.630E+02	.1	.51	8.11	
.22	215.22	.787E+02	.2	.58	7.15	
.25	215.25	.960E+02	.2	.65	6.41	
.28	215.28	.115E+03	.3	.72	5.83	
.32	215.32	.136E+03	.4	.78	5.35	
.35	215.35	.157E+03	.5	.84	4.95	
.38	215.38	.180E+03	.6	.90	4.62	
.41	215.41	.205E+03	.8	.96	4.33	
.44	215.44	.231E+03	.9	1.02	4.09	
.47	215.47	.258E+03	1.1	1.08	3.87	

Page 38

Post-Dev-Con-SCS	
.51	215.51
.54	215.54
.57	215.57
.60	215.60

<---- hydrograph ---->		<--pipe / channel-->	
AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm/s)
(ha)	(cms)	(hrs)	(mm/s)
.83	.12	3.00	65.05
OUTFLOW: ID= 2 (0115)	.83	.10	3.33
INFLOW: ID= 1 (0116)	.83	.17	.47

CALIB		STANHYD (0107)	
ID= 1	DT= 5.0 min	Area (ha)=	3.63
Total	Imp(%)=	Dir. Conn. (%)=	19.00

IMPERVIOUS		PERVIOUS (i)	
Surface Area (ha)=	.17	Impervious (%)=	.56
Dep. Storage (mm)=	1.00		3.00
Average Slope (%)=	2.00		3.00
Length (m)=	155.50		440.00
Mannings n =	.013		.250

Max.Eff.Inten.(mm/hr)=	130.73	74.94
over (min)	5.00	35.00
Storage Coeff. (min)=	2.43	(ii) 31.99 (ii)
Unit Hyd. Tpeak (min)=	5.00	35.00
Unit Hyd. peak (cms)=	.30	.03

\*TOTALS\*

PEAK FLOW (cms)=	.25	.31
TIME TO PEAK (hrs)=	3.00	3.42
RUNOFF VOLUME (mm)=	82.80	56.23
TOTAL RAINFALL (mm)=	83.80	83.80
RUNOFF COEFFICIENT =	.99	.67

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

\*\*\*\*\* WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%

YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
- CN= 86.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----| ADD HYD (0114) | Routing time step (min)'= 5.00

-----| DATA FOR SECTION ( 1.1 ) ----->

Distance .00

Elevation 215.60

Manning .0500

1.80 215.00 .0500 / .0500 Main Channel

2.56 215.00 .0500 / .0500 Main Channel

4.36 215.60 .0500

-----| ADD HYD (0114) | Routing time step (min)'= 5.00

-----| TRAVEL TIME TABLE ----->

DEPTH (m)

ELEV (m)

VOLUME (cu.m.)

FLOW RATE (cms)

VELOCITY (m/s)

TRAV. TIME (min)

.03 215.03 .947E+01 .0 .15 38.53

-----| CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0

ID= 1 DT=10.0 min Ia (mm)= 4.00 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .24

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

-----| CALIB NASHYD (0102) | Area (ha)= 1.39 Curve Number (CN)= 84.0

ID= 1 DT=10.0 min Ia (mm)= 4.00 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .24

-----| TRANSFORMED HYETOGRAPH ----->

TIME RAIN

hrs mm/hr

Post-Dev-Con-SCS

PEAK FLOW (cms)= .212 (i)

TIME TO PEAK (hrs)= 3.000

RUNOFF VOLUME (mm)= 49.006

TOTAL RAINFALL (mm)= 83.800

RUNOFF COEFFICIENT = .585

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0111) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
.00	215.00	.0500
3.00	215.00	.0500
3.76	215.00	.0500
5.56	215.60	.0000

<---- TRAVEL TIME TABLE ---->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.701E+01	.0	.18	22.93
.06	215.06	.160E+02	.0	.29	14.14
.09	215.09	.240E+02	.0	.39	10.61
.13	215.13	.400E+02	.1	.48	8.65
.15	215.15	.550E+02	.1	.56	7.38
.19	215.19	.720E+02	.2	.64	6.48
.22	215.22	.909E+02	.3	.72	5.80
.25	215.25	.112E+03	.4	.79	5.27
.28	215.28	.135E+03	.5	.86	4.85
.32	215.32	.160E+03	.6	.93	4.50
.35	215.35	.187E+03	.7	.99	4.21
.38	215.38	.216E+03	.9	1.05	3.95
.41	215.41	.247E+03	1.1	1.12	3.74
.44	215.44	.280E+03	1.3	1.17	3.55
.47	215.47	.313E+03	1.6	1.23	3.38
.51	215.51	.351E+03	1.8	1.29	3.23
.54	215.54	.390E+03	2.1	1.35	3.09
.57	215.57	.431E+03	2.4	1.40	2.97
.60	215.60	.474E+03	2.8	1.46	2.86

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0102)	1.39	.21	3.00	49.01	.20
OUTFLOW: ID= 1 (0111)	1.39	.20	3.17	48.92	.19

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.  
Page 41

Post-Dev-Con-SCS

CALIB NASHYD (0105)	Area (ha)= 4.82	Curve Number (CN)= 66.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .35		

Unit Hyd Qpeak (cms)= .522

PEAK FLOW (cms)= .327 (i)  
TIME TO PEAK (hrs)= 3.167  
RUNOFF VOLUME (mm)= 29.527  
TOTAL RAINFALL (mm)= 83.800  
RUNOFF COEFFICIENT = .352

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0113) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
3.80	215.00	.0500 Main Channel
5.60	215.60	.0500

<---- TRAVEL TIME TABLE ---->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.541E+01	.0	.15	22.38
.06	215.06	.120E+02	.0	.25	13.54
.09	215.09	.198E+02	.0	.33	10.01
.13	215.13	.288E+02	.1	.41	8.05
.16	215.16	.390E+02	.1	.49	6.79
.19	215.19	.502E+02	.1	.56	5.91
.22	215.22	.630E+02	.2	.63	5.25
.25	215.25	.768E+02	.3	.70	4.74
.28	215.28	.917E+02	.4	.77	4.33
.32	215.32	.108E+03	.4	.83	4.00
.35	215.35	.125E+03	.6	.90	3.72
.38	215.38	.144E+03	.7	.96	3.48
.41	215.41	.164E+03	.8	1.02	3.28
.44	215.44	.185E+03	1.0	1.08	3.10
.47	215.47	.207E+03	1.2	1.13	2.94
.51	215.51	.230E+03	1.4	1.19	2.80
.54	215.54	.255E+03	1.6	1.24	2.68
.57	215.57	.280E+03	1.8	1.30	2.57
.60	215.60	.307E+03	2.1	1.35	2.47

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0105)	4.82	.33	3.17	29.53	.27
OUTFLOW: ID= 1 (0113)	4.82	.32	3.25	29.50	.27

| CALIB |

Page 42

Post-Dev-Con-SCS  
| NASHYD (0112) | Area (ha)= 1.40 Curve Number (CN)= 75.00  
ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
U.H. Tp(hrs)= .24

Unit Hyd Qpeak (cms)= .222

PEAK FLOW (cms)= .157 (i)  
TIME TO PEAK (hrs)= 3.000  
RUNOFF VOLUME (mm)= 37.478  
TOTAL RAINFALL (mm)= 83.800  
RUNOFF COEFFICIENT = .447

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ROUTE CHN (0109) | Routing time step (min)'= 5.00

<---- DATA FOR SECTION ( 1.1 ) ---->

Distance	Elevation	Manning
.00	215.60	.0500
1.80	215.00	.0500 / .0500 Main Channel
3.80	215.00	.0500 Main Channel
5.60	215.60	.0500

<---- TRAVEL TIME TABLE ---->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.03	215.03	.813E+01	.0	.14	14.28
.06	215.06	.170E+02	.0	.23	8.87
.09	215.09	.260E+02	.1	.31	6.68
.13	215.13	.369E+02	.1	.38	5.45
.16	215.16	.480E+02	.2	.44	4.64
.19	215.19	.598E+02	.2	.50	4.07
.22	215.22	.724E+02	.3	.56	3.64
.25	215.25	.857E+02	.4	.62	3.30
.28	215.28	.997E+02	.5	.68	3.03
.32	215.32	.114E+03	.7	.73	2.80
.35	215.35	.130E+03	.8	.78	2.61
.38	215.38	.146E+03	1.0	.84	2.45
.41	215.41	.163E+03	1.2	.89	2.31
.44	215.44	.181E+03	1.4	.94	2.18
.47	215.47	.199E+03	1.6	.99	2.08
.51	215.51	.218E+03	1.8	1.04	1.98
.54	215.54	.238E+03	2.1	1.08	1.89
.57	215.57	.259E+03	2.4	1.13	1.81
.60	215.60	.280E+03	2.7	1.18	1.74

<---- hydrograph ----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0112)	1.40	.16	3.00	37.48	.15
OUTFLOW: ID= 1 (0109)	1.40	.15	3.08	37.44	.15

| ADD HYD (0103) | AREA (ha) QPEAK (cms) TPEAK (hrs) R.V. (mm)  
ID1= 1 (0113): 4.82 .320 3.25 29.50

Page 43

Post-Dev-Con-SCS  
+ ID2= 2 (0109): 1.40 .152 3.08 37.44  
ID = 3 (0103): 6.22 .456 3.17 31.29

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.  
FINISH

Page 44